

Similarity Assessment with TSUNAMI

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Outline

- BRIEF intro to sensitivity coefficients
- "Fundamental theorem of TSUNAMI"
- Uncertainty propagation and correlation coefficients
- Similarity assessment via integral index c_k
- Conclusion



Introduction to Sensitivity Coefficients

- Predict the expected change in a response (k) due to a change in some input parameter (Σ)
 - These responses can be k_{eff} (or ratios of reaction rates)
 - These input parameters are typically nuclear data
 - Cross sections, multiplicity (nubar: $\bar{\nu}$), fission spectrum (chi: χ)
- The coefficients are dimensionless ratios
 - What would happen to the system $k_{\rm eff}$ if some piece of data were changed by some amount?
 - The coefficient is calculated <u>without</u> making the change

$$S_{k,\Sigma} = \frac{\delta k/k}{\delta \Sigma/\Sigma}$$



TSUNAMI Sensitivity Methods

- 1. TSUNAMI-1D Deterministic, Multigroup
- 2. TSUNAMI-2D Deterministic, Multigroup
- 3. TSUNAMI-3D

tional Laborator

- Multigroup TSUNAMI-3D Monte Carlo, Multigroup
- Iterated Fission Probability (IFP) Method Monte Carlo, Continuous-Energy
- CLUTCH Method Monte Carlo, Continuous-Energy

• TSUNAMI offers several options for sensitivity calculations based on the transport code used for analysis. The accuracy and runtime of the approaches vary.

Sensitivities of k_{eff} for a Critical Experiment

Nuclide	Material	Sensitivity	Unc.
H-1	Moderator	0.2396	0.6%
U-235	Fuel	0.2415	0.1%
U-238	Fuel	-0.1395	0.1%
B-10	Absorber	-0.0097	0.2%
Fe-56	Reflector	0.0199	0.5%





Use of uncertainty information to assess system similarity

- "Fundamental theorem of TSUNAMI": bias is caused by errors in cross section data, which are bounded by cross-section uncertainties
- Systems will have similar computational biases if they have similar sensitivities
 - Uncertainties act like a weighting function
- Comparison must examine nuclide-, reaction-, and energy-dependent data



Code validation with TSUNAMI

- Some questions TSUNAMI analysis is intended to answer:
 - Which experiments should I use to validate my application?
 - Is there a quantitative basis for generating a reactivity allowance for a validation weakness or gap?
 - Is there a basis for extracting relevant information from existing experiments to largely dissimilar applications?
- TSUNAMI-IP performs
 - Uncertainty analysis
 - Benchmark experiment selection (Similarity assessment)



Propagation of Cross Section Uncertainties

•Chain rule allows for propagation of cross section uncertainty (i.e. covariance) to quantify the data-induced uncertainty in k_{eff} (σ_k^2)

$$\sigma_k^2 = S C_{aa} S^T$$

Where:

- •S is a matrix of all energy-dependent sensitivity data for all systems considered (S^T is transpose)
- •C_{aa} is a matrix containing energy-dependent covariance information evaluated for all nuclear data



Uncertainty Propagation

• Uncertainty in k_{eff} of a single system



 B
 B
 E
 E
 E

 InfTelastic

 1, h, gamma

 b-10 elastic

 -11 n, alpha

 n-14 elastic

C_{kk}

 Δk

k

2



Uncertainties for Criticality Benchmarks

- Results from SCALE 6.2.2 Validation Report
- ~96.5% of C/E
 values within 1σ
 of unity





Uncertainty Propagation

• Suppose we have sensitivity information for multiple systems:



S

 $C_{\alpha\alpha}$

ST



Uncertainty Propagation

• Suppose we have sensitivity information for multiple systems:



ariance between 1 systems

Correlation Coefficient c_k for System 1 and System 4

 $c_{kk} = \begin{bmatrix} \sigma_{11}^{2} & \sigma_{12}^{2} & \sigma_{13}^{2} & \sigma_{14}^{2} \\ \sigma_{21}^{2} & \sigma_{22}^{2} & \sigma_{23}^{2} & \sigma_{24}^{2} \\ \sigma_{31}^{2} & \sigma_{32}^{2} & \sigma_{33}^{2} & \sigma_{34}^{2} \\ \sigma_{41}^{2} & \sigma_{42}^{2} & \sigma_{43}^{2} & \sigma_{44}^{2} \end{bmatrix}$



Integral Index c_k

- c_k is an integral index used to assess similarity
 - Uncertainty weighted sensitivity profiles between two systems
 - Typically an application system and a critical experiment
 - What fraction of the data-induced uncertainty is shared by two systems?
 - Correlation coefficient, so normalized from -1.0 to +1.0
 - +1.0 is exactly the same system while 0 is completely uncorrelated
- Current guidance:
 - c_k of 0.9 or higher indicates a highly similar system
 - c_k between 0.8 and 0.9 are "marginally" similar



c_k calculation

- c_k calculated by TSUNAMI-IP
- Each application compared with each experiment

- Extended c_k edit from TSUNAMI-IP
- Contribution of each covariance matrix location (largely isotope-reaction) to c_k

Integral Indices for All Experiments in Relation to All Applications

Values colored Blue exceed cutoff value

Values colored Red are maximum for each application

Application #1 gbc-32 - buc w17x17, 1.0 - 6

NUMBER	EXPERIMENT	Туре	Format	Value	Xsec Uncert	¢ _k ↑
111	lct049, case 18, maracas, h/	keff	Relative	1.0015E+0 ± 4.9700E-4	5.53031E-1 ± 4.2903E-5 % dk/k	0.7455 ± 0.0009
97	lct049, case 4, maracas, h/u	keff	Relative	9.9928E-1 ± 4.9700E-4	5.72524E-1 ± 5.7411E-5 % dk/k	0.7363 ± 0.0008
96	lct049, case 3, maracas, h/u	keff	Relative	9.9866E-1 ± 4.2700E-4	5.74281E-1 ± 5.0922E-5 % dk/k	0.7354 ± 0.0008
94	lct049, case1, maracas, h/u=	keff	Relative	9.9783E-1 ± 4.9900E-4	5.78241E-1 ± 5.5989E-5 % dk/k	0.7328 ± 0.0009
95	1ct049, case 2, maracas, h/u	keff	Relative	9.9943E-1 ± 4.9600E-4	5.82083E-1 ± 6.5012E-5 % dk/k	0.7314 ± 0.0009
101	lct049, case 8, maracas, h/u	keff	Relative	9.9771E-1 ± 4.9800E-4	5.93696E-1 ± 6.1676E-5 % dk/k	0.7246 ± 0.0011
110	lct049, case 17, maracas, h/	keff	Relative	9.9902E-1 ± 4.9000E-4	5.94144E-1 ± 5.6457E-5 % dk/k	0.7237 ± 0.0011
148	mix-comp-therm-004-003	keff	Relative	9.9677E-1 ± 2.5800E-4	$6.34278E-1 \pm 1.6177E-4 \% dk/k$	0.7182 ± 0.0009

Application #1 gbc-32 - buc w17x17, 1.0 - 6 with Experiment #111 lct049, case 18, maracas, h/

The c_k value is: 0.7455 ± 0.0009

Contributions to c_k by individual energy covariance matrices:

The c_k value is the sum of the individual contributions.

Input covariance file: 56groupcov7.1

Working covariance file: tsunami-ip_sample.wrk

Covariance Matrix			c _k Contribution		Individual c _k	
Nuclide-Reaction	Nuclide-Reaction	Γ	Due to this Matrix		From this Matrix	
²³⁵ U nubar	²³⁵ U nubar		2.7967E-01 ± 8.8787E-06		9.9977E-01 ± 3.1739E-05	
²³⁸ U n,gamma	²³⁸ U n,gamma		2.3888E-01 ± 4.2904E-05		9.8109E-01 ± 1.7621E-04	
²³⁵ U n,gamma	²³⁵ U n,gamma		6.5028E-02 ± 1.2896E-05		9.4240E-01 ± 1.8689E-04	
²³⁸ U n,n'	²³⁸ U n,n'		6.2786E-02 ± 8.4151E-04		9.9993E-01 ± 1.3402E-02	
²³⁸ U nubar	²³⁸ U nubar		2.5906E-02 ± 2.3041E-06		9.9993E-01 ± 8.8932E-05	
²³⁵ U fission	²³⁵ U fission		2.3404E-02 ± 6.9609E-06		9.7662E-01 ± 2.9047E-04	
²³⁵ U fission	²³⁵ U n,gamma		2.0116E-02 ± 6.5511E-06			
¹ H elastic	¹ H elastic		1.4180E-02 ± 4.4734E-05		9.9896E-01 ± 3.1513E-03	
²³⁸ U elastic	²³⁸ U n,n'		-1.4143E-02 ± 1.2650E-04			
²³⁵ U n,gamma	²³⁵ U fission		1.0555E-02 ± 2.1524E-06			



Summary

- S/U-based parameters should be useful in identifying similar benchmark systems
 - Basis for similarity is both sensitivity information and nuclear data uncertainties
 - Use of c_k has been integrated into other validation approaches
- Similarity assessment can be used in trending analyses to determine subcritical limits
- \bullet ORNL recommends c_k values greater than 0.8 for inclusion in validation

