

Nuclide Inventories with ORIGAMI for Criticality Safety Models

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Practical application of ORIGAMI to generate nuclide inventory data for use in criticality safety models

- **Goal:** determine **bias and bias uncertainty for burnup credit criticality safety** that are associated with isotopic depletion validation.
- The nuclide compositions uncertainty is propagated to bias and uncertainty in k_{eff} of reference models.
- Cask criticality models served as reference models under NUREG-7108¹ (2012) and NUREG-7109² (2012).
- Each reference model has unique assembly-average burnup and enrichment.
- The cask consists of 32 W 17x17 fuel assemblies. Each fuel element is discretized into 18 axial zones with different burnups.
- Using TRITON to compute the nuclides inventory is computationally expensive.
- TRITON is used to generate **burnup-dependent** ORIGEN libraries for the **fuel** assembly and then ORIGAMI uses these libraries to rapidly generate nuclides inventory for any enrichment/burnup combination.
- This approach is more efficient since TRITON depletion calculation takes **hours** whereas ORIGAMI takes **seconds**.

[1] G. Radulescu , I. Gauld , G. Ilas, and J. Wagner, "An Approach for Validating Actinide and Fission Product Burnup Credit Criticality Safety Analyses—Isotopic Composition Predictions," NUREG/CR-7108, U.S. Nuclear Regulatory Commission, Office of Nuclear Regulatory Research (2012).

[2] J. M. Scaglione , D. E. Mueller , J. C. Wagner , W. J. Marshall , " An Approach for Validating Actinide and Fission Product Burnup Credit Criticality Safety Analyses—Criticality (k_{eff}) Predictions ", NUREG/CR-7109, U.S. Nuclear Regulatory Commission, Office of Nuclear Regulatory Research (2012).

Overview of the workflow

- Generate **ORIGEN** reactor libraries at different assembly enrichments.
- Each library includes cross sections at different burnups
- Rapidly calculate inventory at different burnups/enrichments
- Use the resulting nuclide inventory in CSAS model to calculate k_{eff}

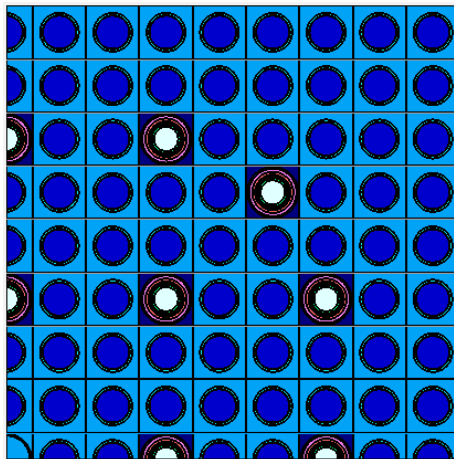
TRITON



ORIGAMI



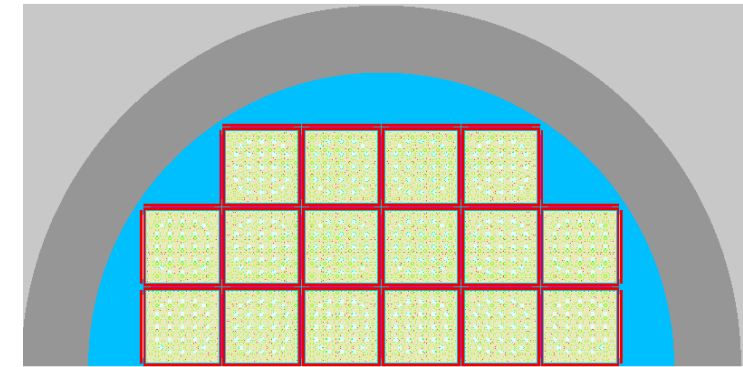
CSAS



TRITON assembly model

```
=origami
title='PWR cask'
options{ft71=all, stdcomp=yes,fdens=10.5216}
libs=[ "w17x17_waba" ]
fuelcomp{
  mix(1){ stdcomp(fuel){
    base=uo2 iso[92235=6.0 92238=94.0]
  }
}
}
hist[
  cycle{ power=60 burn=500 nlib=15}
  cycle{ down=100 }
  cycle{ down=100 }
]
end
```

Sample of ORIGAMI input

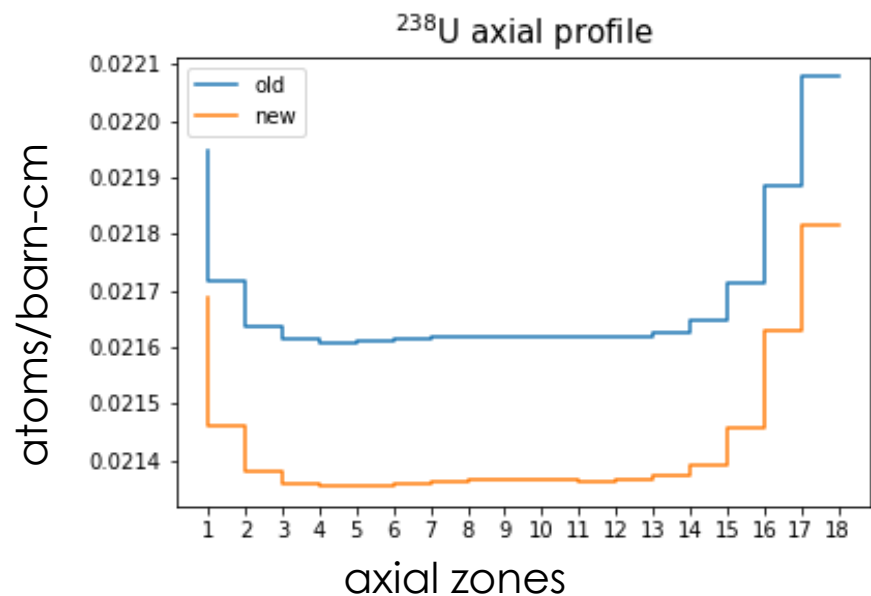


CSAS cask model

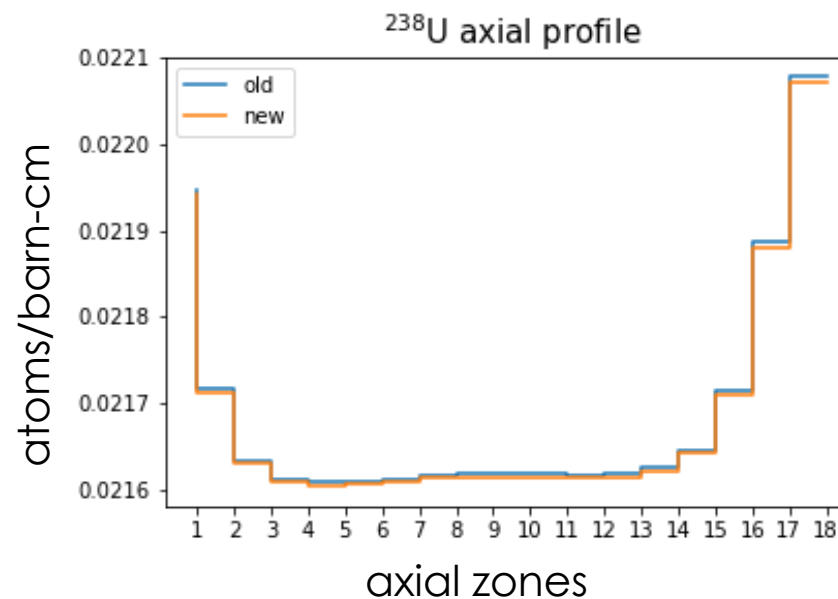
ORIGAMI tips 1/3

- **fdens** must be specified if **actual fuel density** is different from the default density value in ORIGAMI (**10.4 g/cm³**)
- Using wrong fuel density will result in an inaccurate isotopic composition and accordingly wrong k_{eff}

```
=origami  
  title='PWR cask'  
  options{ft71=all, stdcomp=yes, fdens=10.5216}
```



default fdens



correct fdens

ORIGAMI tips 2/3

***nlibs*: not too many, not too few**

- ***nlibs***: number of ORIGEN library burnup-interpolations during the cycle.
- Few interpolation points might cause inaccurate results because of the error introduced by interpolation.
- Too many interpolation points could add unnecessary computational cost.
- Burnup step is recommended to be ~ 2 GWd/MTU.

```
hist[
  cycle{ power=60 burn=500 nlib=15}
  cycle{ down=100 }
  cycle{ down=100 }
]
end
```

ORIGAMI tips 3/3

Format of output nuclides inventory in atom/barn-cm to be provided to CSAS

Option 1: use *stdcomp=yes*

- generates separate text file **myInput_compBlock.txt**
- concentrations are given at the last time step
- the resulting file can be used directly in CSAS input.

```
=origami
title='PWR cask'
options{ft71=all, stdcomp=yes, fdens=10.5216}
```

Option 2: use *OPUS*

- generates separate text file **myInput.plt**
- concentrations are given with lower precision

```
=opus
data="myInp.f71"
title="cask"
typarams=nuclides
nrank=22
symnuc=U234 U235 U236 U238 Np237 Pu238 Pu239 Pu240 Pu241
      Tc99 Ru101 Rh103 Ag109 Cs133 Nd143 Nd145 Sm147 Sm149 Sm150
      Sm151 Eu151 Sm152 Eu153 Gd155 o16 end
sort=no
units=ATOM
end
```

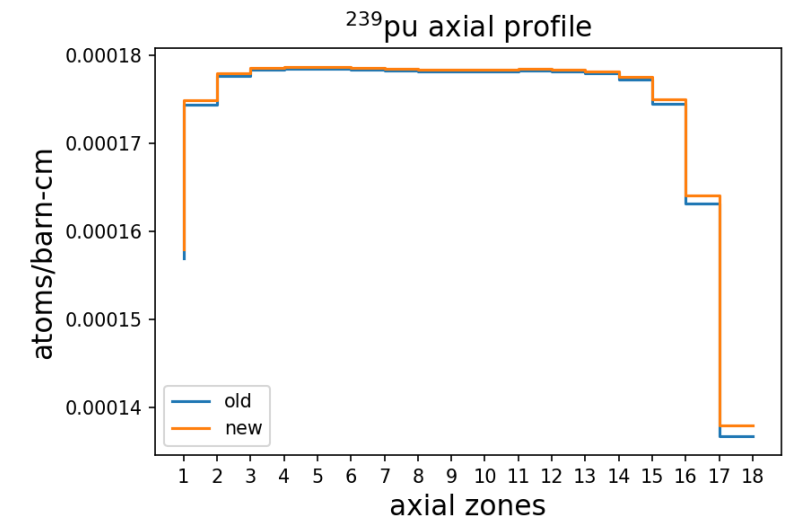
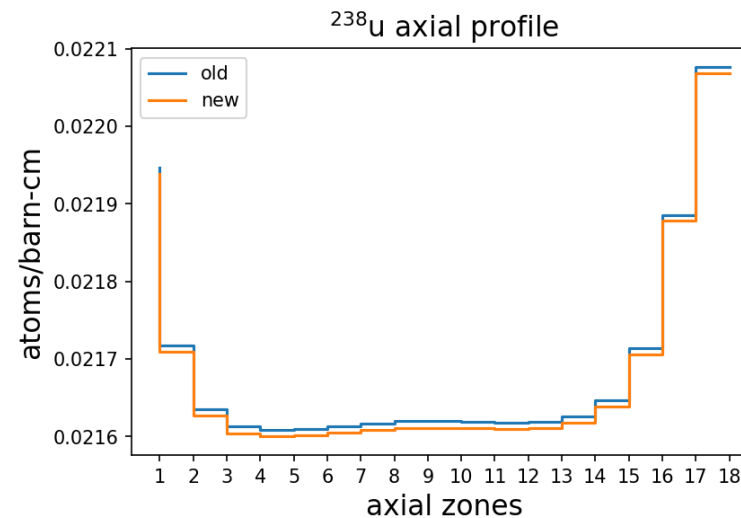
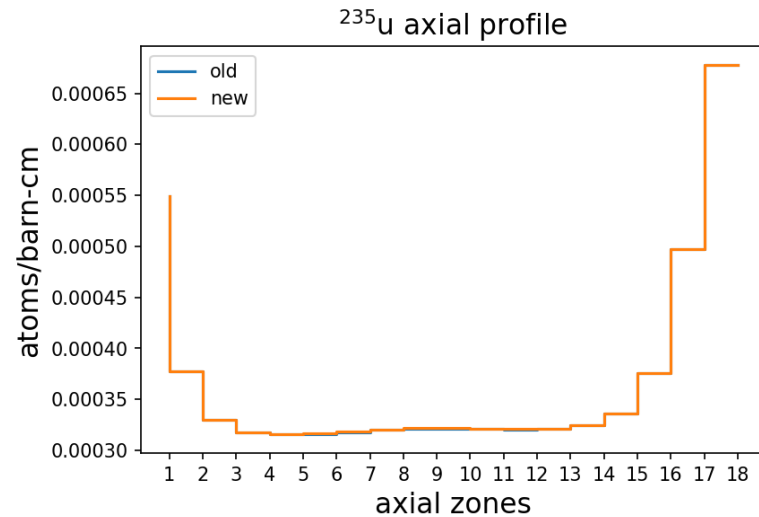
o-16	1001	0	4.6818E-02	293.0	end
u-234	1001	0	1.0369E-08	293.0	end
u-235	1001	0	3.8858E-04	293.0	end
u-236	1001	0	2.1565E-05	293.0	end
u-238	1001	0	2.2841E-02	293.0	end
np-237	1001	0	9.6119E-07	293.0	end
pu-238	1001	0	5.3095E-08	293.0	end

```
cask
time (d)
at/bcm
nuclide
49 31
      0.000e+00 3.262e+01 6.524e+01 9.785e+01
u234 0.000e+00 8.956e-04 1.751e-03 2.567e-03
u235 1.767e+02 1.704e+02 1.645e+02 1.587e+02
u236 0.000e+00 1.314e+00 2.570e+00 3.772e+00
u238 2.355e+03 2.353e+03 2.350e+03 2.347e+03
```

Verify consistency of ORIGAMI-based methodology for generating axial fuel composition to an old methodology

new – based on ORIGAMI with ORIGEN reactor libraries generated with SCALE 6.1.3/ 238 gr ENDF/B-VII.0

old – based on STARBUCS with ORIGEN reactor libraries generated with SCALE 6.1.3/238 gr ENDF/B-VII.0



Burnup=40 GWd/MTU, Enrichment=4.63506 %