

## **AS-BUILT SIMULATION OF THE HIGH FLUX ISOTOPE REACTOR**

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### **ABSTRACT**

The Oak Ridge National Laboratory High Flux Isotope Reactor (HFIR) is an 85 MWt flux trap-type research reactor that supports key research missions, including isotope production, materials irradiation, and neutron scattering. The core consists of an inner and an outer fuel element containing 171 and 369 involute-shaped plates, respectively. The thin fuel plates consist of a U<sub>3</sub>O<sub>8</sub>-Al dispersion fuel (highly enriched), an aluminium-based filler, and aluminium cladding. The fuel meat thickness is varied across the width of the involute plate to reduce thermal flux peaks at the radial edges of the fuel elements. Some deviation from the designed fuel meat shaping is allowed during manufacturing. A homogeneity scan of each fuel plate checks for potential anomalies in the fuel distribution by scanning the surface of the plate and comparing the attenuation of the beam to calibration standards. While typical HFIR simulations use homogenized fuel regions, explicit models of the plates were developed under the Low-Enriched Uranium Conversion Program. These explicit models typically include one inner and one outer fuel plate with nominal fuel distributions, and then the plates are duplicated to fill the space of the corresponding fuel element. Therefore, data extracted from these simulations is limited to azimuthally averaged quantities. To determine the reactivity and physics impacts of an as-built outer fuel element and to generate azimuthally dependent data in the element, 369 unique fuel plate models are generated and positioned. This model generates the three-dimensional (i.e., radial-axial-azimuthal) plate power profile, where the azimuthal profile is impacted by features within the adjacent control element region and beryllium reflector. For an as-built model of the outer fuel element, plate-specific homogeneity data, <sup>235</sup>U loading, enrichment, and channel thickness measurements are translated into the model, yielding a much more varied azimuthal power profile encompassed by uncertainty factors in analyses. These models are run with the ORNL-TN and Shift Monte Carlo tools, and they contain upwards of 500,000 cells and 100,000 unique tallies.

**KEYWORDS:** High Flux Isotope Reactor, as-built, high-fidelity, Monte Carlo

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## 1. INTRODUCTION

The Oak Ridge National Laboratory High Flux Isotope Reactor (HFIR) is a very high power density research reactor supporting several scientific missions, including neutron scattering, isotope production, and materials irradiation. The water-cooled reactor consists of several concentric cylindrical regions (Fig. 1), including a central flux trap, core, control elements, and beryllium reflectors. The core consists of a 171-plate inner fuel element (IFE) and a 369-plate outer fuel element (OFE), each with 1.27 mm thick involute-shaped fuel plates and coolant channel gaps (Fig. 1). Each 1.27 mm thick plate consists of a 0.762 mm thick central volume filled with a  $\text{U}_3\text{O}_8$ -Al dispersion fuel and an Al filler, with additional boron in the IFE filler (Fig. 1) [1].

To reduce power peaking at the radial edges of the fuel elements, the thickness of the  $\text{U}_3\text{O}_8$ -Al fuel mixture is varied along the length of the involute (Fig. 2). The as-designed distribution of this fuel mixture is defined in flat-plate geometry (Fig. 2) before the plates are curved to final involute form. To accommodate the difficulties in manufacturing processes with such finely detailed geometries, tolerances are defined within the design specifications, and uncertainty factors are used in safety analyses to account for inhomogeneities or other manufacturing variances [2]. Data generated during the manufacturing process quantify this deviation from the designed IFE and OFE. Interpreting and incorporating this data within the highest fidelity models of the HFIR OFE and examining the impact demonstrates the capability of modern modeling and simulation tools and shows the value of as-built simulations.

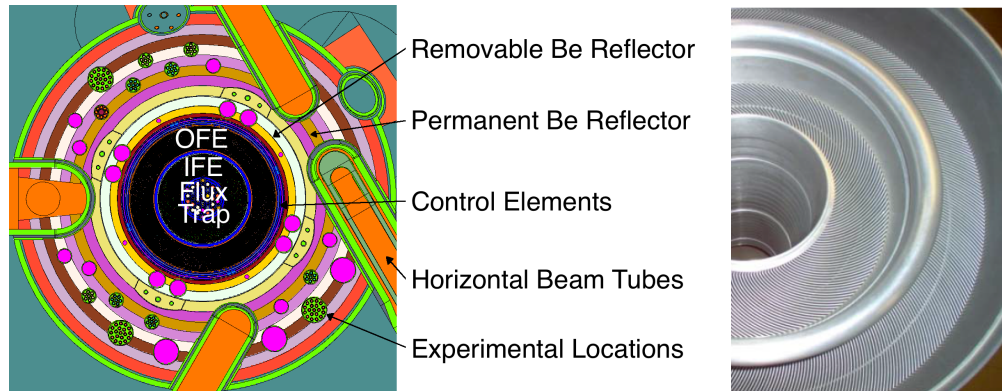


Figure 1. The HFIR core at the axial horizontal midplane (left) and a top-down view of the HFIR core showing the curved fuel plates (right).

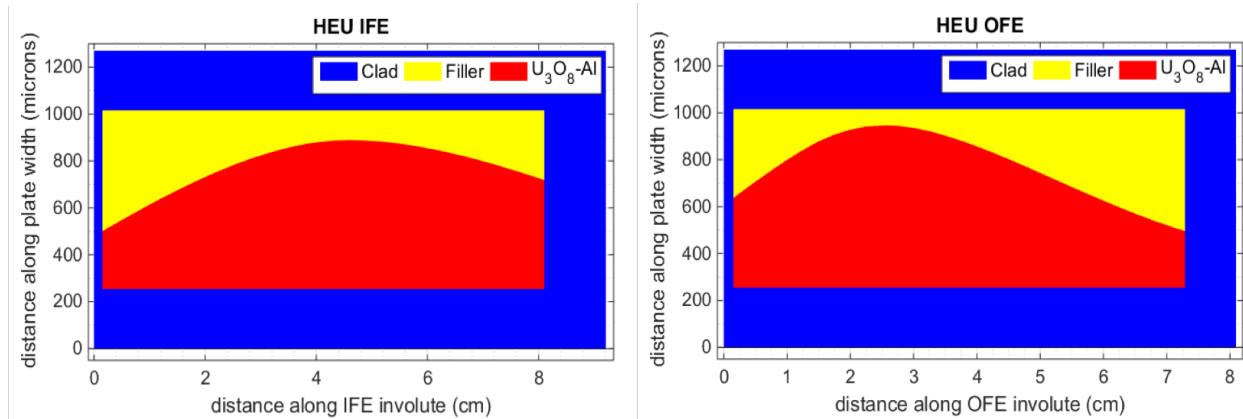


Figure 2. The HEU fuel meat profiles in the IFE (left) and the OFE (right).

## 2. MODELING TOOLS

Significant efforts through the Low-Enriched Uranium (LEU) Conversion Program have yielded high-fidelity reactor physics models of HFIR, including explicit models of the current highly enriched uranium (HEU) core [3]. These reactor physics models have been fully reviewed and checked, and they serve as the starting point for this analysis: HFIR with an HEU core and a representative target loading.

The Shift Monte Carlo tool [4–6] was leveraged by the LEU Conversion Program for design optimization studies due to its scalability and its ability to yield results equivalent to those obtained using software quality assurance tools [4]. Average run times reduced by orders of magnitude, yielding accurate results within hours [7]. In addition, the HFIRCON tool developed for high-fidelity multicycle target depletion calculations for HFIR is leveraged. HFIRCON uses the MCNP [8] transport solver with ORNL-TN upgrades [9] and the SCALE/ORIGEN [10] depletion solver to perform time-dependent depletion calculations with automatic detailed heating output.

In design studies for the LEU Conversion Program, fuel meshes, coupling methods, and data formats were generated and thoroughly exercised between reactor physics tools and thermal hydraulic solvers [2,11–14]. Of particular interest is the fission density and relative fission density distributions within the IFE and OFE fuel plates, which are typically azimuthally integrated quantities due to the transport model. This model explicitly defines one IFE and one OFE fuel plate and duplicates this plate throughout the IFE and OFE regions. The relative fission density  $F_d$  takes the fission density distribution and effectively renormalizes it over an overlaid mesh to account for the volumetric distribution of the fuel,

$$F_d = \frac{1}{\bar{F}_d V_{\text{mesh}}} \sum_i^M \int_0^\infty dE \int_{\partial V \in V_{\text{mesh}}} dV N_i(\mathbf{r}) \sigma_{i,f}(\mathbf{r}, E) \phi(\mathbf{r}, E), \quad (1)$$

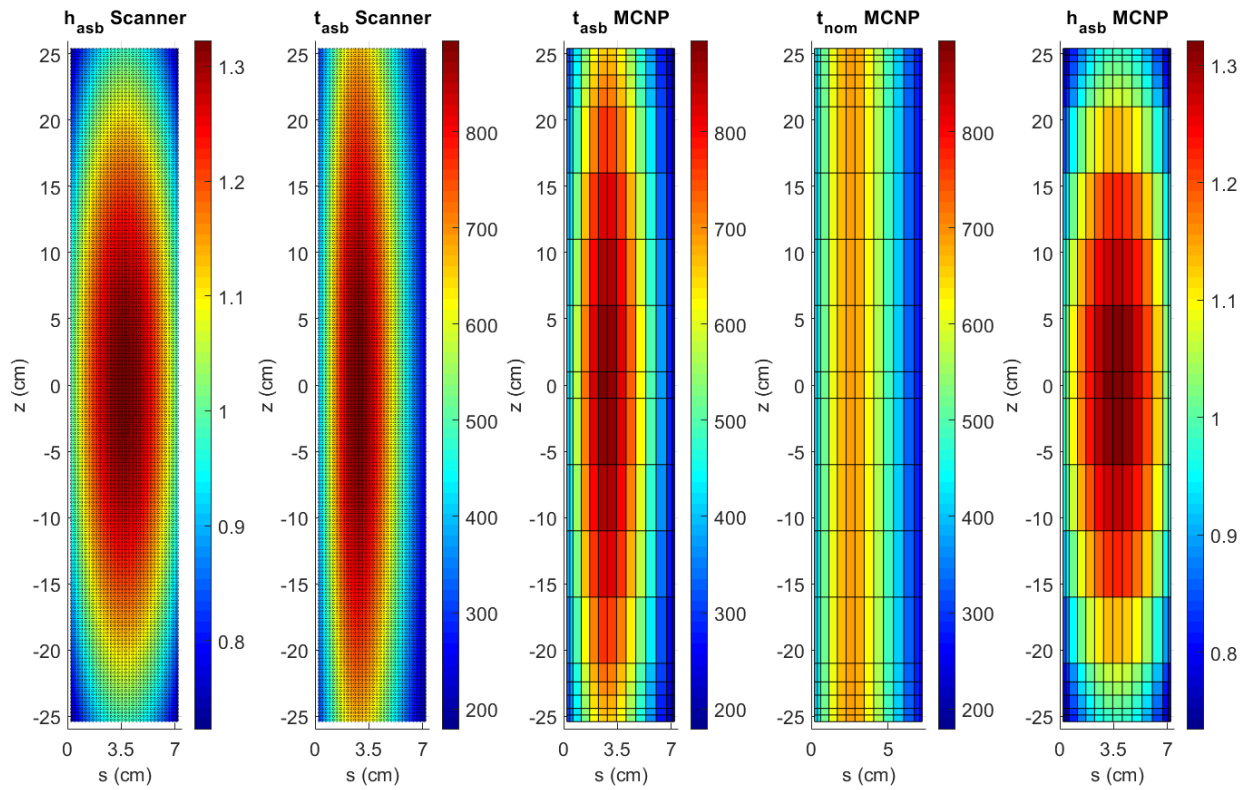
where  $V_{\text{mesh}}$  is the volume of the given mesh region,  $N_i$  is the number density of isotope  $i$ ,  $\sigma_{i,f}$  is the fission cross section of isotope  $i$ ,  $\phi$  is the scalar flux, the sum is over the  $M$  fissile isotopes within the fuel region, and  $\bar{F}_d$  is a normalization factor defined by the total fissions divided by the volume of the total mesh.

Monte Carlo source convergence is not an issue for small, tightly coupled cores like HFIR; calculated Shannon entropy of the Monte Carlo source tends to show source convergence within tens of cycles [7]. Typical HFIR Monte Carlo simulations for LEU and HEU core analysis use 50 inactive cycles, 300 active cycles, and  $10^5$  particles per cycle, for a total of  $30 \times 10^6$  active particles. This is sufficient for the 43,000-group flux tallies used for fuel region depletion, but it does not provide low-uncertainty results globally, particularly toward the outer edges of the reactor [2,15–18]. Therefore, more detailed metrics and heat deposition calculations requiring higher confidence in tallies in small cells far from the core use approximately  $500 \times 10^6$  active particles [19,20]. Though many quantities tallied for the following analysis are within the fuel, there is additional fidelity in these models, and there is a need to quantify the power distribution within individual fuel plates. Thus, results shown herein use at least  $3 \times 10^9$  active particles to adequately reduce tally uncertainties. In all cases, the calculated Monte Carlo uncertainty is less than 0.5% for single plate quantities and less than 0.1% for azimuthally integrated quantities.

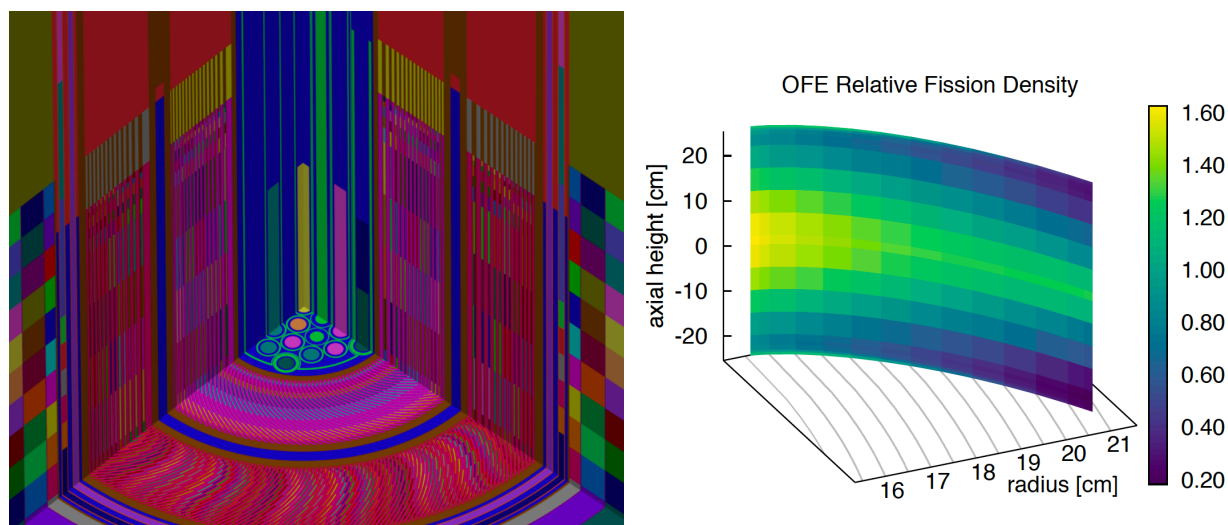
## 3. AS-BUILT DATA

Homogeneity, enrichment, and mass data are taken for each fuel plate that has been inserted into the fuel elements. A homogeneity scan effectively measures the fuel distribution within a given plate, which should reflect the as-designed radial distribution of the fuel meat. After the plates are inserted into the elements, the width distribution of each coolant channel between the plates is measured. The result is an indexed set of as-built fuel plate and coolant channel gap data.

Before this data can be incorporated into the explicit HFIR models, it must be remapped onto the existing fuel mesh. The HFIR HEU OFE  $14 \times 19$  fuel mesh (radial $\times$ axial) has been shown to adequately capture heat deposition and depletion physics [16,21]. The coolant channel gap is discretized in a similar manner, with additional mesh elements in the unfueled regions, resulting in a  $16 \times 21$  mesh. Conversely, homogeneity data are taken on a  $48 \times 333$  mesh, and coolant channel gap data are taken on a  $5 \times 461$  mesh. For the homogeneity data, the as-built integrated average fuel thickness is coarsened onto the MCNP mesh (Fig. 3). This generates an as-built fuel distribution within the plate, which is then adjusted to match the as-built plate mass and enrichment data. For the coolant channel gap data, a nearest neighbor extrapolation and linear interpolation approach in the radial dimension (to convert to a finer mesh) follows an axial integration onto the neutronics mesh. Previous preliminary analyses of as-built data determined that its inclusion would likely reduce conservatism, as the as-built plates are typically underloaded at the radial and axial edges of the active fuel region, where the fission power is typically higher.



**Figure 3.** From left to right displayed as a function of axial height and length along the involute (s): a sample homogeneity scan ( $h_{asb}$ ), a calculated thickness profile from the scan ( $t_{asb}$ ), a mapped thickness profile from the scan ( $t_{asb}$  MCNP), the nominal thickness profile ( $t_{nom}$ ), and homogeneity factors to apply to model the deviation from the nominal ( $h_{asb}$  MCNP). This is for a single plate.



**Figure 4.** The HFIR explicit fuel plate model with 369 unique OFE plates showing different materials and mixtures distributed throughout the OFE (left) and the relative fission density distribution within a given plate in the OFE (right).

#### 4. RESULTS AND DISCUSSION

The first step to incorporating this plate-specific data is to build a model that can accept this data: each OFE fuel plate must be explicitly defined. The resulting 369 individual explicit OFE plate model is comprised of 1.5 million lines of input and nearly 500 thousand cells (Fig. 4). Two models are generated: (1) with the as-designed fuel distribution repeated in all fuel plates, and (2) incorporating this as-built data. In all cases, the data are incorporated via density adjustments instead of physical changes to the geometry. This density adjustment approximation introduces negligible error [16]. The as-built OFE alone consists of 100,000 fuel and 125,000 coolant cells, with an individual reaction rate cell tally defined for each fuel cell to determine the fission density.

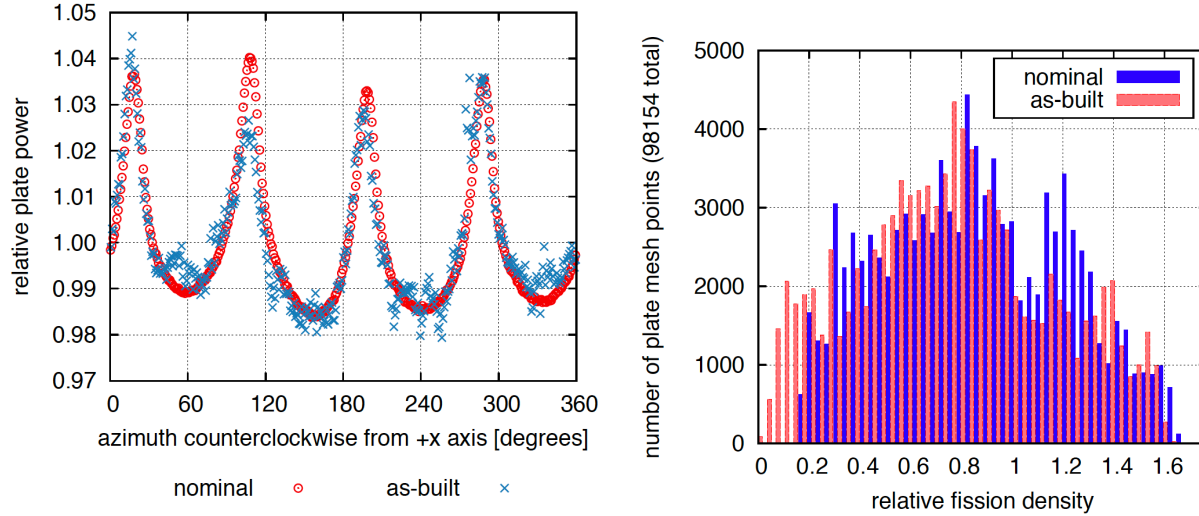
All computations were performed on the Oak Ridge Leadership Computing Facility machine, Titan [22]. Each calculation was run using 350 total cycles with 50 inactive cycles and  $10 \times 10^6$  particle histories per cycle. Regardless of the complexity of the simulation, Shift was able to return results within hours of real time (Table I). Modeling 369 individual fuel plates results in Shift Monte Carlo run times that are over eight times longer than previous models.

**Table I. Shift calculation times.**

Model	Nodes (processors per node)	Real time (hours)
One-plate as-designed	1280 (16)	1.17
369-plate as-designed	5120 (16)	2.67
369-plate as-built	5120 (16)	3.53

The change in the reactivity is relatively small (500 pcm) and as expected due to the underloading (relative to as-designed) of fuel plates toward the radial and axial edges of the plates. Replicating the as-designed fuel plates throughout the OFE yields a smooth, well-behaved plate power distribution that is impacted by the features in the control element and reflector regions (Fig. 5): the plate power recovers in

azimuthal locations adjacent to the four gaps between the absorbers within the control elements. Incorporating as-built data shows significant deviations from this smooth shape, although the peak powers are nearly bounded by those of the as-designed model (Fig. 5). Localized impacts of incorporating the as-built data show reduced peak relative power densities (Fig. 5), again due to the underloading at the radial edges of the core.



**Figure 5. Plate power distribution for the 369 fuel plates (left) and relative fission density distribution for all fuel mesh regions (right).**

## 5. DISCUSSION

The programmatic generation of the explicit fuel plate models developed under the LEU Conversion Program streamlined generation of these models and incorporation of the as-built data. The capability of ORNL-TN in generating the geometry for a very lengthy MCNP model and the scalability of Shift were also critical in generating tightly converged results within tens of hours of real time. The resulting as-built fission density distributions were bounded by current safety factors incorporated into safety analyses, supporting the current approach for reactor operations. Local impacts from incorporating the as-built data would have little impact relative to using the as-designed fuel plates. While this level of fidelity has less use for normal operations, the capability to incorporate as-built data in models provides for analysis of manufacturing anomalies or nonconforming components.

The MCNP model described herein is the largest and most detailed model of HFIR. To the author's knowledge, this is the largest Shift simulation (i.e., in terms of number of cells in the model and number of cell tallies) ever performed.

## ACKNOWLEDGMENTS

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