

Non-LWR Analysis with SCALE 6.3

Horizontal Split Table Conceptual Design for Validation of Nuclear Data used in Advanced Reactors

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Outline

- 1. Motivation
- 2. Methods
 - Critical core experimental configuration
 - Evaluation of nuclear data tested by the experimental configuration
 - Assessment of horizontal split-table mechanical tolerances
- 3. Example concept: Pebble-bed High-Temperature Gas-cooled reactor -HTR-10 application case
- 4. Summary and next concepts



Motivation

- Advanced reactors designs use different material, energy spectrum, and/or temperature conditions than current commercial nuclear reactors
- Potential nuclear data gap or high uncertainties exist on some materials (e.g., graphite, sodium)
- To help judge the adequacy of available nuclear data, a design of benchmark critical experiments similar to those advanced reactors is proposed



Motivation

- Lawrence Livermore National Laboratory is leading the overall and mechanical design (Catherine Percher and Daniel Siefman), ORNL is leading the criticality/nuclear data need design
- LLNL proposed a horizontal-split-table design
- The choice of type of advanced reactor for the conceptual design is based on F. Bostelmann, G. Ilas, W. A. Wieselquist "Key Nuclear Data Impacting Reactivity in Advanced Reactors," ORNL/TM-2020/1557 (2020)



Motivation

 From LLNL, limitation on the geometry of the table, and on the mass and size of material on it



Example rendering of the Horizontal Split Table concept proposed by LLNL (Catherine Percher)

	Table Part	Dimension	Cm	Maximum	
Maximum Table dimensions	Both tables	Width	182.88	Surface Area	
				cm²	44593
	Fixed table	length	121.92		
				m²	4.46
	Moving table	length	121.92		
	Total	length	243.84		



For each Horizontal split table advanced reactor type concept studied, a similar process is followed:

- 1. Determination of a critical core experimental configuration
- 2. Evaluation of nuclear data tested by the experimental configuration
- 3. Assessment of horizontal split table mechanical tolerances



1. Determination of a critical core experimental configuration

- Search to find a publicly available and trustworthy advanced reactor benchmark model
- Conversion of the model to a SCALE KENO-VI format if needed
- Modification of the model to accommodate a rectangular shape and the maximal required dimensions of 182.88 x 243.84 cm
- Incremental SCALE 6.3 KENO-VI calculations with ENDF/B-VII.1 cross-section library to determine a critical core, adjusting reflector/moderator in priority, active core region if needed
- Separation of the model in half to correspond to the two sides of the split-table



2. Evaluation of nuclear data tested by the experimental configuration

- Creation of a TSUNAMI model of the critical core
- Calculation of the keff uncertainty due to the use of ENDF/B-VII.1 cross-section library
- Observation of the materials and/or nuclear isotopes responsible for the highest keff sensitivity
- Creation of sensitivity data file (.sdf)
- Assessment of the correlation between the HST .sdf file and the original application benchmark .sdf file with TSUNAMI-IP
- If ck, the correlation coefficient determine by TSUNAMI-IP is high, it means a useful critical experiment benchmark concept for nuclear data validation of advanced reactors materials



Assessment of horizontal split table mechanical tolerances 3.

- What is the influence on keff of mechanical uncertainties in the table design?
 - Horizontal gap •
 - Vertical gap •
 - Angular gap •
 - Torsion gap •
- Quadratic fit to determine a keff uncertainty Horizontal gap per mechanical uncertainty





Angular gap

- Described in IRPhEP, Evaluation of the Initial Critical Configuration of the HTR-10 Pebble-Bed Reactor, HTR10-GCR-RESR-00 (2007)
- Previously modeled in SCALE KENO-VI by G. Ilas et al., "Validation of SCALE for High Temperature Gas-Cooled Reactor Analysis," NUREG/CR-7107, ORNL/TM-2011/161 (2012)
- Good candidate because of available information, model, and uncertainties on nuclear data used exist



- Active core region is 123 cm high and 180 cm diameter, not far from the splittable requirements
- Total of 16890 pebbles, 9627 fuel, 8263
 dummy
- Packing fraction 61%
- Pebble radius 3.0 cm, 2.5 cm fuel region and 0.5 cm radius graphite shell
- 8355 TRISO particles in each pebble
- TRISO: UO₂ kernel and layers of cladding





Layer of pebbles in active core region

From *G. Ilas et al., "Validation of SCALE for High Temperature Gas-Cooled Reactor Analysis," NUREG/CR-7107, ORNL/TM-2011/161 (2012)*



- 1. Determination of a critical core experimental configuration
- Critical configuration is obtained with SCALE
 6.3 KENO-VI calculations using ENDF/B-VII.1 cross-section library
- Modeled active core region is 120 x 140 x 123 cm high
- Modeled graphite reflector is 182 x 220 x 242.57 cm high



Center cut plane top view of SCALE KENO-VI model



- 2. Evaluation of nuclear data tested by the experimental configuration
- TSUNAMI is used to calculate keff sensitivities of the HST conceptual design
- Most significant contributors are Uranium and graphite

	Nuclide	Corresponding	TSUNAMI Results		
Material #		physical element in model	Sensitivity	Relative uncertainty (%)	
1	∪-235	Fuel kernel -UO ₂	0.25036	0.02%	
2	U-238	Fuel kernel -UO ₂	-0.03782	-0.12%	
3	c-graphite	Graphite matrix in pebble	0.42285	2.89%	
4	c-graphite	Pebble Shell	0.07597	3.35%	
5	c-graphite	Dummy Pebble	0.15208	3.59%	



- 2. Evaluation of nuclear data tested by the experimental configuration
- U-235 sensitivities profiles for the HST concept design and the original HTR-10 application are matching
- Correlation coefficient ck=0.9982, proof of a high correlation between both systems
- Goal is achieved: This design could help for cross-section validation of pebble-bed advanced reactor similar to the HTR-10



U²³⁵ total cross section sensitivity profiles for the HTR10 whole core and the Horizontal Split Table concept



- 2. Evaluation of nuclear data tested by the experimental configuration
- Additional study: Effects of changing the cross-section library
- About 1000 pcm difference between
 ENDF/B-VII.1 and ENDF/B-VII.0
- Difference mostly due to carbon crosssection updates in ENDF/B-VII.1

Model	Table size	Cross-section library	k _{eff}	Delta k _{eff} (pcm)
Critical core ENDF/B-VII.1	240x182x242.574	ENDF/B-VII.1	0.99963	-
		ENDF/B-VII.0	1.01225	+1262
Critical core ENDF/B-VII.0	240x182x220	ENDF/B-VII.0	1.00075	-
		ENDF/B-VII.1	0.99082	-993



- 3. Assessment of horizontal split table mechanical tolerances
- Parametric study performed with KENO-VI







- 3. Assessment of horizontal split table mechanical tolerances
- Most significant effects are from horizontal and angular gaps
- Logical result: in vertical and torsional gaps effects, the tables sides are still connected



Gap (°)

Gap (°)



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Interpolate d ∆k _{eff}	Horizontal Gap (cm)	Vertical Gap (cm)	Angular Gap (°)	Torsional Offset (°)
-0.00010	0.040	5.00	0.0235	2.10
-0.00020	0.055	6.00	0.033	2.60
-0.00050	0.099	8.10	0.061	3.68
-0.00100	0.170	10.70	0.106	4.95
-0.00200	0.308	14.45	0.191	6.78

Interpolated geometric uncertainties necessary to yield experimental uncertainties



Summary and next concepts in mind

- A methodology to create conceptual designs of benchmark critical experiments for advanced reactors nuclear data testing and validation was developed
- A first concept was explored, pebble-bed high-temperature gas cooled reactor, based on the HTR-10 reactor
- The very high correlation is a proof of concept that our design is similar to the application, and performing such critical experiments would help nuclear data testing and validation
- Next concepts being explored:
 - Molten-salt reactor
 - Sodium-cooled fast reactor
 - Heat pipe reactors/Microreactor





Questions?

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