ORNL/HSSI (6953)/MLSR-2000/9

HEAVY-SECTION STEEL IRRADIATION (HSSI) PROGRAM (W6953)

Monthly Letter Status Report

June 2000

ORNL/HSSI (6953)/MLSR-2000/9

HEAVY-SECTION STEEL IRRADIATION PROGRAM

JCN W6953

MONTHLY LETTER STATUS REPORT FOR JUNE 2000

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PREFACE

This report is issued monthly by the staff of the Heavy-Section Steel Irradiation (HSSI) Program (JCN:W6953) to provide the Nuclear Regulatory Commission (NRC) staff with summaries of technical highlights, important issues, and financial and milestone status within the program.

This report gives information on several topics corresponding to events during the reporting month: (1) overall project objective, (2) technical activities, (3) meetings and trips, (4) publications and presentations, (5) property acquired, (6) problem areas, and (7) plans for the next reporting period. Next the report gives a breakdown of overall program costs as well as cost summaries and earned-value-based estimates for performance for the total program and for each of the eight program tasks. The six tasks correspond to the 189, dated March 23, 1998, and modified by the inclusion of the former "Embrittlement Data Base and Dosimetry Evaluation" Program, JCN 6164 in March, 1999. The final part of the report provides financial status for all tasks and status reports for selected milestones within each task. The task milestones address the period from April 1998 to December 2000, while the individual task budgets address the period from October 1999 to November 2000.

Beginning in October, 1992, the monthly business calendar of the Oak Ridge National Laboratory was changed and no longer coincides with the Gregorian/Julian calendar. The business month now ends earlier than the last day of the calendar month to allow adequate time for processing required financial reports to the Department of Energy. The precise reporting period for each month is indicated on the financial and milestone charts by including the exact start and finish dates for the current business month.

Thomas M. Rosseel, Manager
Heavy-Section Steel Irradiation

MONTHLY LETTER STATUS REPORT
June 2000

Job Code Number:	**W6953**
Project Title:	**Heavy-Section Steel Irradiation Program**
Period of Performance:	**4/1/98 to 11/30/00**
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1. PROJECT OBJECTIVE:

The primary goal of the Heavy-Section Steel Irradiation (HSSI) Program is to provide a thorough, quantitative assessment of the effects of neutron irradiation on the material behavior, and in particular the fracture toughness properties, of typical pressure vessel steels as they relate to light-water reactor pressure vessel (RPV) integrity. The program includes studies of the effects of irradiation on the degradation of mechanical and fracture properties of vessel materials augmented by enhanced examinations and modeling of the accompanying microstructural changes. Effects of specimen size; material chemistry; product form and microstructure; irradiation fluence, flux, temperature, and spectrum; and post-irradiation mitigation are being examined on a wide range of fracture properties. This program will also maintain and upgrade computerized data bases, calculational procedures, and standards relating to RPV fluence-spectra determinations and embrittlement assessments. Results from the HSSI studies will be incorporated into codes and standards directly applicable to resolving major regulatory issues that involve RPV irradiation embrittlement such as pressurized-thermal shock, operating pressure-temperature limits, low-temperature overpressurization, and the specialized problems associated with low upper-shelf welds. Six technical tasks and one for program management are now contained in the HSSI Program.

2. TECHNICAL ACTIVITIES:

TASK 1: Program Management (T. M. Rosseel)

This task is responsible for managing the program to ensure that the overall objectives are achieved. The management responsibilities include three major activities: (1) program planning and resource allocation; (2) program monitoring and control; and (3) documentation and technology transfer. Program planning and resource allocation includes: (a) developing and preparing annual budgetary proposals and (b) issuing and administrating subcontracts to other contractors and consultants for specialized talents not available at Oak Ridge National Laboratory (ORNL) or that supplement those at ORNL. Program monitoring and control includes: (a) monitoring and controlling the project through an earned-value, project-management system; (b) ensuring that quality assurance (QA) requirements are satisfied; and (c) issuing monthly management reports. Documentation and technology transfer includes: (a) participating in appropriate codes and standards committees; (b) preparing briefings for the NRC; (c) coordinating NRC and internal ORNL review activities; (d) coordinating domestic and foreign information exchanges approved by NRC; and (e) documenting the activities of the program through letter and NUREG reports.

(Milestone 1.2.B) The MTS 100-kip servo-hydraulic machine in the hot cell developed an oil leak necessitating that testing of the KS-01 compact specimens be stopped (subtask 2.2). The actuator of another machine will be reconditioned and used to replace the existing rig. Although the total cost and time of this effort is not yet known, it is anticipated that the repair will be completed in late July or early August, depending on other activities at the hot cell facility, primarily the crane replacement. The cost of the repair and replacement will be shared among the ORNL Fusion, APT, and HSSI programs. It is also anticipated that testing of the PSI specimens (subtask 3.3) may be delayed until the next fiscal year.

Hot cell charges have been increased by 25% due to higher than planned costs required to operate the Irradiated Materials Evaluation and Testing facility. Discussions are being held to determine the impact on the Program and options for next fiscal year with ORNL M&C Division senior management.

(Milestone 1.3.A) On June 4-9, 2000, the Program Manager traveled to Williamsburg, Virginia, to participate in the ASTM E-10.02 Committee meeting and the 20th Symposium on the Effects of Radiation on Materials. Discussions were held with HSSI collaborators including Professors O'dette, University of California, Santa Barbara, and Kumar, University of Misouri-Rolla, as well Dr. Lee of KAERI, Dr. Ortner of AEA Technology, UK, and Mr. Oniza of JAERI.

<u>Task 2: Fracture-Toughness Transition and Master-Curve Methodology</u> (M. A. Sokolov)

Fracture-toughness transition and master-curve (MC) methodology will be broadly explored for pressure-vessel applications through a series of experiments, analyses, and evaluations in eight Subtasks. For example, pertinent fracture-toughness data needed to assess the shift and potential change in shape of the fracture-toughness curves due to neutron irradiation will be collected and statistically analyzed. The effects of irradiation on fracture-toughness curve shape for highly embrittled RPV steels, dynamic effects, crack arrest, intergranular fracture, and subsized specimens will also be explored. Finally, guidelines for the application of "surrogate materials" to the assessment of fracture toughness of RPV steels will be evaluated.

<u>Subtask 2.1: Fracture-Toughness Transition-Temperature Shifts</u> (M. A. Sokolov)

The purpose of this subtask is to collect and statistically analyze pertinent fracture-toughness data to assess the shift and potential change in shape of the fracture-toughness curves due to neutron irradiation. The MC methodology will be applied to provide a statistical analysis of the fracture-toughness data and Charpy data will be fitted by hyperbolic tangent functions. The resulting reference fracture-toughness temperature, T_0, shifts will be compared with Charpy shifts determined by various indexing methods.

(Milestone 2.1.A) No activity during this reporting period.

The report by M. A. Sokolov and R. K. Nanstad, *Comparison of Irradiation-Induced Shifts of K_{Jc} and Charpy Impact Toughness for Reactor Pressure Vessel Steels* [NUREG/CR-6609 (ORNL/TM-13755)], was submitted to the NRC for publication in May 1999.

<u>Subtask 2.2: Irradiation Effects on Fracture-Toughness Curve Shape</u> (M. A. Sokolov)

The purpose of this subtask is to evaluate the assumption of constant shape for the MC even for highly embrittled RPV steels. The evaluation will be performed through irradiation of a pressure-vessel steel to a neutron fluence sufficient to produce a fracture-toughness transition-temperature shift (T_0) of about 150 ^{0}C (270 ^{0}F). Evaluation of the MC shape will be determined with sufficient numbers of 1T compact specimens, 1T C(T), to allow for testing at three temperatures in the transition-temperature region. Additionally, 0.5T C(T), and precracked Charpy V-notch (PCVN) specimens, for both quasi-static and dynamic tests, will be irradiated and tested to investigate the use of more practical surveillance-size specimens. Tensile specimens will also be included to determine the irradiation-induced hardening. A comprehensive test program with unirradiated material will be included to provide the necessary baseline data for comparison.

(Milestone 2.2.A) As reported in the previous progress report, all the irradiated specimens of the KS-01 weld were transported to ORNL from the Ford Nuclear Reactor. Charpy specimens have been tested, and testing of compact specimens was begun. The initial results indicate that the T_o of this material is about 150°C. Based on these data, 1T C(T) will be tested at this temperature first and then the entire transition curve will be determined. However, testing has been stopped because the servohydraulic machine began to leak oil. It was determined that the oil is coming from the actuator; most likely because of a faulty seal. The actuator of the machine must be removed to affect the repair. A replacement actuator has been obtained from a similar testing machine at ORNL and has been sent to a commercial company for reconditioning. The total cost and time of this effort is not yet known, but we anticipate completion of the repair during the month of July, dependening on other activities at the hot cell facility, primarily the crane replacement.

Irradiation of the Midland beltline weld and a high-nickel weld from the Palisades steam generator is under way and proceeding on schedule. John Kneeland (Palisades) indicated that some additional high-nickel weld material might become available for irradiation studies.

<u>Subtask 2.3: Dynamic Effects, Including Precracked Charpy V-Notch Testing</u> (S. K. Iskander)

As reactors age, the operating window between the startup or shutdown K_a curve, generated from the allowable pressures and temperatures, and the K_{Ia} curve becomes smaller, making it difficult for plants to startup and shut-down. Dynamic testing of relatively small specimens will be evaluated as an alternative method to determine a lower bound to fracture toughness. Results from Subtask 2.5 (crack-arrest), which measures dynamic properties, will also be used in this subtask.

(Milestone 2.3.A) No significant activity during this reporting period.

<u>Subtask 2.4: Irradiation Effects on Fracture Toughness of Midland RPV Weld</u> (R. K. Nanstad)

The purpose of this subtask is to determine the transition-temperature shift and to evaluate transition-toughness curve shape for a low Charpy upper-shelf weld metal at a relatively high neutron fluence that will produce greater embrittlement damage than previously obtained with irradiations at lower fluences. This subtask will evaluate the assumption of constant shape for the MC with highly embrittled low-upper-shelf RPV steels that exhibit onset of stable ductile tearing at relatively low-fracture toughness. The evaluation will be performed through irradiation of the beltline weld from the Midland Unit 1 RPV to a fluence of about 2.5 to 5 x 10^{19} n/cm^2 (>1 MeV) for which a substantial database of unirradiated and irradiated results to a fluence of 1 x 10^{19} n/cm^2 (>1 MeV) already exists. This research is needed to assess the fracture-toughness behavior of such a weld at high-embrittlement levels. Evaluation of the MC shape will be determined with sufficient numbers of 0.5T C(T) to allow for testing at three temperatures in the transition-temperature region. Additionally, PCVN specimens, for both quasi-static and dynamic tests, will also be irradiated and tested to investigate the use of more typical surveillance-size specimens, and tensile specimens will be included to determine the irradiation-induced hardening. A comprehensive-test program with unirradiated material was previously completed under the first HSSI Program (L1098) 10th Irradiation Series, except for dynamic testing of PCVN specimens, which will be included to provide the necessary baseline data for comparison.

Subtask 2.4: Irradiation Effects on Fracture Toughness of Midland RPV Weld (R. K. Nanstad)

(Milestone 2.4.D) The final report, *Evaluation of WF-70 Weld Metal from the Midland Unit 1 Reactor Vessel - Final Report*, by D. E. McCabe, R. K. Nanstad, S. K. Iskander, D. W. Heatherly, and R. L. Swain, NUREG/CR-5736 (ORNL/TM-13748), was submitted to the NRC for publication in February 1999.

Further evaluation of the Midland beltline weld will be performed under Subtask 2.2.

Subtask 2.5: Crack-Arrest Including Midland Weld (S. K. Iskander)

In this subtask, the low-temperature operating pressure regulatory concerns will be addressed through testing of the 15 irradiated, Midland crack-arrest specimens. This evaluation will provide an excellent opportunity to determine whether the lower bounds of crack initiation and arrest toughness coincide for this very important class of irradiated LUS welds. These specimens, which were produced and irradiated as part of the previous HSSI (L1098) program, will be used to evaluate the lower and transition arrest-toughness values.

(Milestone 2.5.A) The preparation of the draft NUREG report, *Detailed Results of Testing Unirradiated and Irradiated Crack-Arrest Toughness Specimens from the Low Upper-Shelf Energy, High Copper Weld, WF-70*, by S. K. Iskander, C. A. Baldwin, D. W. Heatherly, D. E. McCabe, I. Remec, and R. L. Swain, NUREG/CR-6621 (ORNL/TM-13764), has been completed and the manuscript is being prepared for technical review and transmission to the NRC.

S. K. Iskander attended the ASTM E08 Committee on Crack-Arrest in Philadelphia, June 6. Iskander is the First Co-chairperson of the Committee on Dynamic Fracture Toughness.

Subtask 2.6: Intergranular Fracture (R. K. Nanstad, and J. G. Merkle)

This subtask will address the issue of whether the MC technique can be applied to materials that experience brittle fracture by an intergranular mechanism. Specifically, it will be determined whether steels that experience intergranular fracture can be correctly characterized by the MC T_o temperature and whether the transition-curve shape can be changed by different fracture modes. Complete intergranular fracture from temper embrittlement occurs only at lower-shelf temperatures. As it is with transgranular cleavage, the transition to upper shelf is marked by an increased volume percentage of ductile rupture mixed with the lower-shelf, brittle-fracture mechanism. Since the onset of crack instability is most likely triggered in the brittle zones, the critical issue is understanding the influence of the triggering mechanism on the distribution of K_{Jc} values obtained. This information can be obtained on the lower shelf and, in part, into the transition range.

The proposed approach is to determine if there is an operational weakest-link effect when instability is triggered within an intergranular region. If an effect is observed, there should also be a measurable specimen-size effect on K_{Jc}. It will also be determined if the temper-embrittled materials exhibit a change in the J-R fracture toughness since such steels do not show a significant change in upper-shelf CVN energy.

(Milestone 2.6.B) As discussed in the last progress report, following review of the draft letter report, discussions were held to consider some amount of additional testing. This additional testing will be performed following machining of specimens from the remaining pieces of previously tested 2T C(T) specimens. The 2T specimens have been identified and obtained, a drawing has been prepared, and the specimens are ready for machining.

Subtask 2.7: Subsized Specimens (M. A. Sokolov)

The purpose of this subtask is to evaluate the applicability of the weakest-link theory-based size-adjustment procedure in the MC methodology to specimen sizes that are the most likely to be present in surveillance capsules. The MC methodology will be applied using precracked Charpy-size or smaller specimens to test the lower-size limit applicability. Testing will be performed at two or more temperatures with at least six specimens at each temperature. The exact number of temperatures and specimens will be determined following analysis of initial results. The testing of these subsize specimens will also satisfy the HSSI Program suggested testing matrix within the New Coordinated Research Program (CRP) of the International Atomic Energy Agency (IAEA). Subsized specimens will be fabricated from previously characterized materials within the HSSI Program, such as HSST Plate 02, HSSI Welds 68W through 73W, the Midland beltline weld and plate JRQ.

(Milestone 2.7.C) Abstracts are arriving for the ASTM Fourth International Symposium on Small Specimen Techniques. This symposium will be held in January of 2001 and M. A. Sokolov is serving as the Chairman of the Symposium.

Subtask 2.8: Quantification of Surrogate Materials for use in a Statistics-Based Fracture Toughness Assessment (R. K. Nanstad and J. G. Merkle)

The purpose of this subtask is to establish guidelines for the use of "surrogate materials" in the assessment of fracture toughness of RPV steels. A plan will be developed to describe the information acquired and the means of collecting it, the method of evaluating the information, and the methods for using the information. Analyses will be performed to provide a methodology for determining limits for predicting fracture toughness of one material, i.e., a surrogate material, with measured fracture toughness of similar materials.

(Milestone 2.8.B) A NUREG report, *Considerations for Use of Surrogate Materials Data for Reactor Pressure Vessels*, by R. K. Nanstad, J. G. Merkle, and J. Galt, has been prepared and sent to the NRC technical monitor for review. The abstract was included in the progress report for May of 2000. Further review of data, both unirradiated and irradiated, is continuing with a view towards eventual preparation of a table of uncertainties that could be utilized for evaluating the application of surrogate materials. Progress on this activity was slowed somewhat due to a request by the NRC for HSSI staff input to an HSST project.

Subtask 2.10: Dosimetry and Fluence Analysis of the IAR Irradiation Capsules from the First IAR Campaign (C. A. Baldwin, I. Remec, T. M. Rosseel)

The purpose of this task is measure and analyze the dosimeters used during the first IAR Campaign and to obtain accurate fluence determinations.

(Milestone 2.10.A) The remaining iron gradient wires from the first two IAR metallurgical capsules were transferred from the IMEF to the IFEL. Work is underway to segment, weigh, and count these wires.

Task 3: Irradiation Embrittlement of RPV Steel (S. K. Iskander)

The purpose of this task is to examine two important issues affecting the application of mitigation procedures to RPVs. The first addresses the effects of temper embrittlement on the coarse-grained HAZ in RPV steels. The second examines the effects of reirradiation on K_{Jc} and K_{Ia} in order to evaluate the relative changes in the recovery and reembrittlement between CVN and fracture-toughness properties and a detailed examination of reembrittlement rates. These questions will be addressed using the IAR facility designed, fabricated, and installed as part of the previous HSSI

(L1098) program and with a matrix of irradiated and tempered specimens supplied by the Swiss Paul Scherrer Institut (PSI). Further data on reirradiation embrittlement will be obtained through reconstitution and reirradiation of previously irradiated specimens at the RRC-KI.

Subtask 3.1: HAZ Embrittlement (M. A. Sokolov and R. K. Nanstad)

Research conducted to date on temper embrittlement of the coarse-grain materials in HAZs of RPV steel multi-pass welds has revealed the potential for such embrittlement under some conditions. AEA-Technology discovered that using high-temperature austenitization to produce very coarse grains, followed by thermal aging resulted in large transition-temperature shifts. Further, post-irradiation mitigation of such material resulted in an even greater increase of the transition temperature. Subsequent research at ORNL under the previous HSSI Program (L1098) used five commercial RPV steels to investigate potential temper embrittlement. The first phase simulated the AEA-Technology heat treatment and observed large transition-temperature shifts, although not as large as those from AEA-Technology. The second phase of the ORNL study used the same five RPV steels, but used the Gleeble system (an electrical-resistance heating device) to produce material deemed representative of the coarse-grain region in RPV welds. These materials revealed very high toughness in the initial condition (i.e., from the Gleeble). After thermal aging at about 454 ^{0}C for 168 hours the materials exhibited only modest transition temperature increases, however, after aging at the same temperature for 2000 hours, significant transition temperature increases were observed. Of course, 2000 hours is much in excess of the time that RPV steels would be exposed to mitigation cycles, but potential synergistic effects of irradiation and thermal aging are unknown. Moreover, questions also remain regarding other time-temperature effects, such as post-irradiation mitigation at somewhat lower or higher temperatures.

(Milestone 3.1.B) The irradiation of specimens has been completed. Three material conditions for evaluation are HAZ material before and after thermal anneal (at 460°C for 168 h) and base metal after irradiation. Base metal specimens were tested after irradiation and did not reveal any significant changes in transition temperature as result of irradiation. The simulated HAZ material has been tested in both the irradiated condition and the irradiated/annealed condition. Compared with the unirradiated case, the simulated HAZ material revealed transition temperature shifts of 22°C and 29°C, respectively.

Scanning electron fractography showed that the as-received base metal failed by cleavage with no evidence of intergranular fracture in the irradiated condition. The simulated HAZ material, however, revealed intergranular fracture estimated at about 10 to 20% in the irradiated condition, and more than 75% intergranular fracture following postirradiation thermal annealing. Such a significant exhibition of intergranular fracture was unexpected, especially since this particular material contains only a bulk phosphorus content of 0.007 wt %. Further analyses and discussions are underway, with particular attention to the cooling rate following postweld heat treatment of the simulated HAZ material. Consideration is also being given to reirradiation of some specimens.

R. K. Nanstad presented a paper by R. K. Nanstad, D. E. McCabe, M. A. Sokolov, C. A. English, and S. R. Ortner, “Investigation of Temper Embrittlement in Reactor Pressure Vessel Steels Following Thermal Aging, Irradiation, and Thermal Annealing,” at the 20th Symposium on the Effects of Radiation on Materials, Williamsburg, Virginia, June 6-8, 2000. A subsequent publication will appear in ASTM STP 1405.

Subtask 3.2: Embrittlement Rate of Reirradiated Steel (S. K. Iskander, I. Remec, E. D. Blakeman, and C. A. Baldwin)

This subtask will examine the effects of reirradiation on K_{Ic} and K_{Ia} toughness of RPV steel so as to evaluate the relative changes in recovery and reembrittlement between CVN and fracture-toughness properties and to provide a detailed examination of reembrittlement rates. This will be accomplished using the HSSI IAR and the University of California Santa Barbara (UCSB) irradiation facilities at the University of Michigan, Ford Nuclear Reactor (FNR), and through the reirradiation of previously irradiated specimens at RRC-KI, if funding is available. Emphasis will also be placed on completing dosimetry calculations for the new IAR facility.

(Milestone 3.2.B) Neutronics Analysis of the IAR/UCSB Irradiation Capsules (I. Remec, E. D. Blakeman, C. A. Baldwin) The report entitled: *Characterization of the Neutron Field in the HSSI/UCSB Irradiation Facility at the Ford Nuclear Reactor*, by I. Remec, E. D. Blakeman, and C. A. Baldwin, NUREG/CR-6646 (ORNL/TM-1999/140) was submitted to the NRC in September.

(Milestone 3.2.C) S. K. Iskander presented a paper by S. K. Iskander, R. K. Nanstad, C. A. Baldwin, D. W. Heatherly, and I. Remec, "Reirradiation Response Rate of a High-Copper Reactor Pressure Vessel Weld," at the 20th Symposium on the Effects of Radiation on Materials, Williamsburg, Virginia, June 6-8, 2000. A subsequent publication will appear in ASTM STP 1405.

Subtask 3.3: Evaluation of Reirradiated JRQ Specimens (R. K. Nanstad, and T. M. Rosseel)

The purpose of this subtask is to examine the fracture-toughness behavior of a model steel that has been irradiated, tempered, and re-irradiated. The specimens, identified as JRQ, will supplied by the Swiss PSI from a terminated research program.

(Milestone 3.3.A) Six drums with two lead pigs each were received at ORNL in January from the Paul Scherrer Institute (PSI) in Switzerland. The total complement is 87 each CVN, 36 each PCVN, 6 each tensile, and 6 each 1T three-point bend specimens. The specimens have been removed from the pigs, placed in individually numbered containers, and are ready for testing. However, the repair of the servohydraulic machine, which is located in the same hot cell as the Charpy impact machine, and the replacement of the overhead crane in the hot cell building will delay the schedule for testing of the JRQ samples. Furthermore, recently announced increases in hot cell costs may cause additional uncertainty in the schedule. Schedules for testing will be prepared as soon as the work activities are scheduled and budget uncertainties are resolved.

Task 4: Validation of Irradiated and Aged Materials (R. K. Nanstad)

The purpose of this task is to validate the assessment of the effects of neutron irradiation on the fracture-toughness properties of typical RPV materials obtained in the previous HSSI (L1098) Program, tasks 2 and 3 of this program, and retired RPVs. This will be accomplished through the examination of the effects of neutron irradiation on the fracture toughness (ductile and brittle) of the HAZ of welds and of typical plate materials used in RPVs. The irradiated materials from retired RPVs will be machined and tested in the Irradiated Materials Examination and Testing (IMET) hot cells. The feasibility of reconstitution for CVN and 0.5T C(T) and aging of stainless steel welds will also be explored in this task. Other issues to be address include foreign interactions and technical assistance to the NRC.

Subtask 4.1: Examination of Materials from Retired RPVs (S. K. Iskander and J. T. Hutton)

This subtask will examine the issue of neutron-irradiation-induced damage attenuation through the RPV wall. The damage will be related to measurements of received dose, such as displacements per atom (dpa) through the wall. The HSSI program will obtain suitable-size trepans of materials from previously decommissioned RPVs, because these materials would incorporate conditions from actual operating reactors such as the effects of irradiation on stressed material. A sufficient number and size of trepans will be obtained to permit use of the MC approach to relate measures of damage to the fracture toughness. Specimens will be machined on the CNC milling machine located in Cell

6 of the IMET facility. Depending upon availability and appropriateness, trepans from the Japan Power Demonstration Reactor (JPDR) project, Trojan, and Maine Yankee RPVs may be examined.

(Milestone 4.1.2.B). An extended abstract and viewgraphs have been prepared on the results of testing the Charpy specimens from the JPDR trepans, for the upcoming PTS meeting in July. These will form the nucleus of a NUREG on the results from testing the JPDR weld metal. The attenuation of damage as measured by Charpy impact testing will be compared to the dpa-based attenuation of fluence that is given in RG 1.99 Rev.2.

Preparations have been completed to mount early next month the auxiliary control unit above the floor level of cell 6 containing the computer controlled milling machine. At the present time, the auxiliary control unit is temporarily placed on a table in the rear of the cell as close as possible to the mill inside the machine, because of limits dictated by the electronics of the milling machine on length of cabling.

Subtask 4.2: Reconstitution of Irradiated Toughness Specimens (S. K. Iskander)

Feasibility studies for reconstitution of CVN, PCVN, and 0.5T bend bar specimens will be prepared. To adequately survey the state-of-the-art capabilities, on-site evaluations of US and international facilities will be required. A letter report that includes the estimated costs of either using existing and available facilities or implementing a reconstitution facility at ORNL will be prepared at the completion of this task.

No work is currently funded in this subtask.

Subtask 4.3: Toughness Changes in Aged Stainless Steel Welds (R. K. Nanstad)

The purpose of this subtask is to evaluate the effects of irradiation and thermal aging on stainless-steel weld metals. Two projects are incorporated in this subtask. The first involves completion of fracture-toughness testing on irradiated stainless-steel weld-overlay cladding specimens at 288ºC to complete the testing of the matrix from the HSSI (L1089) 7th Irradiation Series. The PCVN specimens were irradiated in HSSI Capsule 10.06. The second project involves completion of a NUREG report on thermal aging of stainless-steel welds for nuclear piping, a project that began before the inception of the HSSI (L1098) Program and involved thermal aging at 343ºC for up to 50,000 hours.

(Milestone 4.3.B) - The report, *The Effect of Aging at 343°C on the Microstructure and Mechanical Properties of Type 308 Stainless Steel Weldments*, by D. J. Alexander, K. B. Alexander, M. K. Miller and R. K. Nanstad, NUREG/CR-6628 (ORNL/TM-13767), was submitted to the NRC for publication in July 1999.

Subtask 4.4: Foreign Interactions (R. K. Nanstad)

The purpose of this subtask is to provide technical support and continued collaboration for a number of cooperative relationships with foreign institutions in the area of radiation effects on RPV steels. Collaborative relationships may be developed during the course of this program and will be developed with the cognizance of NRC. Current relationships are:

1. U.S.-Russia Joint Coordinating Committee for Civilian Nuclear Reactor Safety (JCCCNRS) Working Group on Radiation Embrittlement and Aging of Components.

2. Cooperation with SCK-CEN in Belgium regarding the supply of well-characterized materials and comparison of test results, including dynamic PCVN testing for development of RPV testing standards.

3. Collaboration with AEA-Technology in the United Kingdom regarding fracture toughness testing of intergranular embrittlement of RPV HAZs.

4. Collaborative studies on fracture properties of high-copper RPV materials with Korean institutes such as KAERI.

5. Collaboration with institutes in the Czech Republic, Germany, and Finland on fracture toughness with small specimens in support of MC evaluations.

6. Collaboration with PSI in Switzerland on reirradiation.

7. Information and data exchange with all of the above and other countries, especially regarding RPV surveillance data and comparisons of fracture toughness and Charpy impact data.

8. Participation, including membership on the Executive Committee, in the International Group on Radiation Damage Mechanisms (IGRDM).

9. Participation in two coordinated research programs (CRPs) sponsored by the International Atomic Energy Agency (IAEA), informally designated CRP-5 and CRP-6. These CRPs will investigate: the use of PCVN specimens to determine fracture toughness of RPV steels, and effects of nickel on irradiation-induced embrittlement of RPV steels, respectively.

10. Collaboration with NRI, Rez (Czech Republic) in the area of microstructural evolution in RPV steels as a consequence of irradiation, annealing, and reirradiation.

11. Collaboration with the University of Lille (France) in the area of primary radiation damage simulation.

(Milestone 4.4.C) - Planning for the next meeting of the IGRDM in Pressure Vessel Steels, IGRDM-9, continues. The meeting will be held in Leuven, Belgium, September 18-23, 2000, and will be hosted by SCK-CEN and Tractebel. R. K. Nanstad is the Secretary of the IGRDM and is assisting in the planning and scheduling of the technical program, as well as revisions to the IGRDM Charter and Membership list. Information has been sent to the members regarding offering of presentations, lodging arrangements, etc. Four of the six technical area coordinators have sent preliminary lists of presentations to the Secretary and the Chairman, Jean-Claude Van duysen. Seven presentations have been offered from the HSSI Program. The program on Friday, September 23, will be an open seminar, open to members of industrial, academic, and research organizations. The topic of the open seminar will be lifetime management of RPVs and invitations are being extended to organizations in all countries with IGRDM members.

<u>Subtask 4.5: Technical Assistance</u> (R. K. Nanstad, S. K. Iskander, and M. A. Sokolov)

The purpose of this subtask is to provide special analytical, experimental, and administrative support to the NRC in resolving various regulatory issues related to irradiation effects. Specific identified activities are incorporated in this subtask, while other activities may be included through modification to the task by the NRC. The currently identified activities involve evaluation of the irradiated specimens contained in capsules previously irradiated at the University of Michigan FNR by Materials Engineering Associates (MEA), evaluation of highly irradiated high-nickel weld surveillance specimens from the Palisades Reactor, evaluation of the effects of post-weld heat treatment (PWHT) on the copper solubility and fracture toughness of unirradiated RPV steels, and compilation of available materials at ORNL and elsewhere for studies of irradiation effects on RPV steels.

A revision of the ASTM Standard E1921 was completed, based on recommendations of the ASTM Task Group meeting held in November 1999. The revised version of the standard was sent to the ASTM Committee E8 for E08.08 subcommittee ballot. The ballot resulted in four negative votes which were discussed at the E08.08 Task Group meeting in June and resolved during the meeting, along with some other minor editorial changes. Other than re-organization of the standard, the primary change is the incorporation of the multi-temperature method as an option for determination of the reference transition temperature, T_o. M. A. Sokolov is co-chairman of the Task Group.

(Milestone 4.5.B) The letter report on RPV materials available for irradiation studies is in progress.

(Milestone 4.5.F) Testing of unirradiated specimens has continued with the high-copper weld given varying time/temperature postweld heat treatments. A Charpy impact energy vs temperature curve has been obtained for four of the conditions to evaluate toughness as a function of PWHT. Testing of the remaining groups will be completed later this year. If funding can be realized, atom probe tomography will be used to determine the matrix copper contribution as a function of PWHT.

Task 5: Modeling & Microstructural Analysis (R. E. Stoller)

This task shall determine the microstructural basis for radiation-induced property changes in RPV materials to aid in understanding and applying the experimental results obtained in Tasks 2 through 4. The subtasks comprise two major components: (1) theoretical modeling and data analysis, and (2) experimental investigations. The modeling work focuses on the development of an improved description of primary-damage formation in irradiated materials, and the further development and use of predictive models of radiation-induced microstructural evolution and its impact on the mechanical behavior of RPV materials. The experimental component consists of special-purpose irradiation experiments to isolate particular irradiation variables (neutron-flux level and energy spectrum), and detailed microstructural characterization of RPV materials in relevant conditions using atom probe and transmission electron microscopy techniques. These conditions include: long-term, thermally-aged, irradiated, post-irradiation mitigation (IA), and reirradiated (IAR). The information obtained from the experiments and microstructural characterization will be used to support validation of the theoretical models. Further model verification will be carried out through extensive use of the commercial-reactor surveillance data and test-reactor data contained in the NRC-funded Embrittlement Database (EDB), and data generated in other experiments coordinated by this task.

The major areas of inquiry will be: (a) the effects of chemical composition, (b) the role of displacement rate (neutron flux level), (c) the impact of differences in neutron-energy spectrum, (d) potential differences in hardening and embrittlement behavior at very high fluence, and (e) the response of materials that are reirradiated following a post-irradiation mitigation. Damage modeling will also address such questions as attenuation through the RPV wall. The overall goal of the task is to provide an embrittlement model that can be used in a predictive way to anticipate the response of RPV materials at high fluences near or slightly beyond their nominal end-of-life, and to provide support to the NRC for related safety or licensing questions. The tools developed in this task will also be used to support the analysis of experimental results obtained in other program tasks. Both the modeling and experimental research will be coordinated with complementary activities carried out by other NRC contractors.

Subtask 5.1: Modeling of Damage Evolution (R. E. Stoller)

The modeling and analysis work will include completion of the development required to incorporate alloying effects in the embrittlement model. Additional thermodynamic components are needed to account for chemical effects, particularly for the simulation of high-fluence effects and thermal mitigation. Enhancements to the code used for simulating displacement cascades will permit the investigation of the effects of alloying elements on primary damage formation.

(Milestone 5.1.A) Thermodynamic predictions indicate that the amount of copper is lower than the solubility limit at 650°C in the body-centered-cubic ferrite matrix and that no face centered ε-copper precipitates are formed. The ε-copper precipitates were also predicted to form at 626°C and lower temperatures for this alloy composition. As expected, the copper content of the ferrite matrix decreases with decreasing temperature, as shown in Fig. 1. The manganese, nickel, silicon, molybdenum, and chromium content of the matrix does not change significantly with temperature. The copper and iron contents of the ε-copper precipitates were also predicted to decrease and the manganese, nickel and molybdenum levels increase with decreasing temperature. No silicon or chromium were predicted to be present in the ε-copper precipitates.

The results of the copper solubilities in the matrix of this weld are shown in Fig. 1. For ease of representation, the temperatures used for the slow cooled materials are isothermal annealing temperatures. The copper content of the as-weld material was found to be slightly higher than the bulk composition. This increase is due to the presence of coarse carbides, which have little or no copper solubility. A small reduction from the bulk copper level was measured in the matrix of the material aged for 24 h at 650°C and water quenched. The copper content in the matrix of the fast cooled material aged for 24 h at 610°C was slightly lower than that of the similar 650°C annealed material and the level was in excellent agreement with the thermodynamic prediction. A comparison of the fast and slow cooled conditions at 650°C reveals that the copper level in the matrix is significantly lower in the slow cooled material. In addition, the copper levels in all three slow cooled materials were lower than the thermodynamic predictions for the isothermal annealing temperatures. These decreases are due to the additional time spent at elevated temperature during which significant amounts of diffusion can occur. A comparison of the material annealed for the typical post-irradiation treatment of 168 h at 454°C to the material annealed at 24 h at 610°C reveals a small decrease in the copper level in the matrix. However, the time at 454°C was insufficient to reach the equilibrium composition, as the measured copper content was significantly higher than the thermodynamic prediction.

R. E. Stoller presented a paper entitled, "An Evaluation of Through-Thickness Changes in Primary Damage Production in Commercial Reactor Pressure Vessels," at the 20th International Symposium on the Effects of Radiation on Materials, Williamsburg, Virginia, June 6-8, 2000. A subsequent publication will appear in ASTM STP 1405.

<u>Subtask 5.2: Microstructural Analysis</u> (R. E. Stoller and M. K. Miller)

Round-robin studies, using atom probe field-ion microscopy (APFIM), small angle neutron scattering (SANS), and field-emission scanning transmission electron microscopy (FEGSTEM), will be coordinated to resolve the inconsistencies between these techniques that have been used to determine the matrix copper content and the chemical composition of radiation-induced precipitates in RPV materials. Additionally, APFIM characterization will be used to determine whether additional radiation-induced phases are forming.

(Milestone 5.2.A). M. K. Miller presented a paper by M. K. Miller and K.F. Russell, Microscopy and Microanalytical Sciences Group, Metals and Ceramics Division, ORNL and J. Kocik and E. Keilova, Nuclear Research Institute, The Czech Republic, entitled, "Atom Probe Tomography of 15Kh2MFA Cr-Mo-V Steel Surveillance Specimens," at the 20th International Symposium on the Effects of Radiation on Materials, Williamsburg, Virginia, June 6-8, 2000.

The NUREG report entitled, *Atom Probe Tomography Characterization of the Solute Distributions in a Neutron-Irradiated and Annealed Pressure Vessel Steel Weld*, NUREG/ CR-6629, (ORNL/TM-13768), was submitted to the NRC in September.

Subtask 5.3: Experimental Verification of Neutron Flux and Energy Spectrum Effects (R. E. Stoller)

An experimental examination of neutron-flux level (displacement rate) and neutron energy spectrum effects (thermal-to-fast-flux ratio) will be conducted in collaboration with other NRC contractors.

No significant activity occurred in this subtask during this reporting period.

Task 6: Test Reactor Irradiation Coordination (K. R. Thoms)

This task provides the support required to supply and coordinate irradiation services needed by NRC contractors, such as the UCSB and the ORNL HSSI Program at the University of Michigan FNR. These services include the design and assembly of irradiation facilities (and/or capsules), as well as arranging for their exposure, periodic monitoring by remote computer access and interaction with the FNR staff, and return of specimens to the originating research organization.

Subtask 6.1: Operate the HSSI Irradiation (IAR) Facility (K. R. Thoms and D. W. Heatherly)

With the fabrication, installation, and initial testing of the HSSI IAR facility at the University of Michigan FNR completed as part of the previous (L1098) HSSI program, the activities associated with the new program include supervising the irradiation of the reusable irradiation capsules in the dual-capsule irradiation facility at FNR. A NUREG report on the design, assembly, installation, and operation of the HSSI IAR facility will be prepared.

(Milestone 6.1.A) Irradiation of the ORNL specimens in the HSSI-IAR 1 and 2 irradiation facilities continued during this reporting period.

During this reporting period, the reactor operated for eight days of half-cycle 446A, approximately 10 days during half-cycle 446B, and the first 2.5 days of half-cycle 447A. The IAR facilities were not operated during half-cycle 446B due to a faulty thermocouple in the UCSB facility, which shares the same trolley mechanism used to crank the facilities in and out of the face of the reactor. The problem with the UCSB facility was corrected during half-cycle 446B and operation of the facilities resumed at the beginning of half-cycle 447A.

During half-cycle 446A, the IAR irradiation facilities received a total of 189 EFPH (effective full power hours). After remaining shut down during half-cycle 446B, the facilities then received an additional 59 EFPH during the first 2.5 days of half-cycle 447A for a total of 248 EFPH during this reporting period.

At the beginning of this reporting period, the second group of specimens to be irradiated in the new IAR facilities had been irradiated for a total of 2048 EFPH. At the end of this reporting period, the second group of specimens had been irradiated for a total of 2296 EFPH. The facilities themselves had been in service for a total of 6624 EFPH.

Calibration activities have been delayed until at least the next reporting period.

(Milestone 6.1.B) The draft NUREG report on the reusable irradiation facilities will be delayed until September due to limited staff availability .

Subtask 6.2: Operate the HSSI/UCSB Irradiation Facility (K. R. Thoms and D. W. Heatherly)

This subtask includes supervising the overall operation and providing assistance to the reactor personnel in the routine operation and maintenance of the HSSI/UCSB irradiation facility. A

NUREG report on the design, assembly, installation, and operation of the UCSB facility will be prepared.

(Milestone 6.2.A) Irradiation of the UCSB specimens in the UCSB irradiation facility continued during this reporting period.

During this reporting period, the reactor operated for eight days of half-cycle 446A, approximately 10 days during half-cycle 446B, and the first 2.5 days of half-cycle 447A. The UCSB facility was not operated during half-cycle 446B due to a faulty thermocouple (#22) between zones 9 and 10 of the high flux portion of the facility. The faulty thermocouple indicated slightly higher than normal temperatures during initial heat up of the facility at the beginning of half-cycle 446B resulting in automatic shut down. All alarms and action from the faulty thermocouple were removed and operation of the facility resumed at the beginning of half-cycle 447A.

During half-cycle 446A, the UCSB irradiation facility received a total of 189 EFPH (effective full power hours). After remaining shut down during half-cycle 446B, the facility then received an additional 59 EFPH during the first 2.5 days of half-cycle 447A for a total of 248 EFPH during this reporting period.

At the beginning of this reporting period, the UCSB facility and original specimen compliment had been irradiated for a total of 13,861 EFPH. At the end of this reporting period the UCSB facility and original specimen compliment had been irradiated for a total of 14,109 EFPH. The latest irradiation plan received from the UCSB experimenters indicated that the final specimens would be removed from the UCSB facility after 13,500 EFPH. Additional specimen irradiations have been added to the original plan and at the end of this reporting period the UCSB irradiation program had obtained 104.5% of the original desired irradiation time.

Calibration activities have been delayed at least until the next reporting period.

Task 7: Embrittlement Data Base and Dosimetry Evaluation (T. M. Rosseel)

This task was until March 1, 1999, the Embrittlement Data Base (EDB) and Dosimetry Evaluation Program, JCN: 6164. The objectives of the two subtasks listed below have been reduced but the focus remains the same. Nuclear radiation embrittlement information from radiation embrittlement research on nuclear RPV steels and from power-reactor surveillance reports will be maintained in a data base to be published on a periodic basis. The information will assist the Office of Nuclear Reactor Regulation and the Office of Nuclear Regulatory Research to effectively monitor current procedures and data bases used by vendors, utilities , and service laboratories in the pressure vessel irradiation surveillance program. It will also provide technical expertise and analysis to the NRC regarding dosimetry and transport calculations and methodologies.

Subtask 7.1: Embrittlement Data Base (J.-A. Wang)

The purpose of the subtask is to maintain and update the EDB. This includes evaluating surveillance reports, entering the data into the EDB, and providing an update to the NRC by the end of the fiscal year.

(Milestone 7.1.A) The surveillance data from the following report were integrated into EDB format.

E. Terek, T. J. Hall, W. E. Pirl, "Analysis of Capsule W from Commonwealth Edison Company Braidwood Unit 1 Reactor Vessel Radiation Surveillance Program," WCAP-15316, October 1999.

(Milestone 7.1.B) Completed UPDATE-11 of PR-EDB. It includes the data from five surveillance reports containing a total of 252 Charpy impact test data, 30 tensile data, and 20 new transition-temperature shift data points from four welds, two plates, eight forgings, and five HAZ materials. Nine data files of the PR-EDB, which contain chemistry, irradiation environment, mechanical test results, and material history, were also updated.

Subtask 7.2: Dosimetry Evaluation (I. Remec)

Technical expertise and analysis regarding dosimetry and transport calculations and methodologies will be provided as needed to the US NRC. Specifically, work will be performed to complete the review of, and hold final discussions with the NRC concerning, the dosimetry guide, DG-1053.

This activity was eliminated as directed by SOEW 60-99-356.

3. MEETINGS AND TRIPS:

On June 4-9, 2000, S. K. Iskander, R. K. Nanstad, M. K. Miller, T. M. Rosseel, R. E. Stoller, and M. A. Sokolov traveled to Williamsburg, Virginia, to present papers, chair sessions, and participate in the ASTM E.10.02 Committee Meetings and the 20th Symposium on the Effects of Radiation on Materials.

On June 12-16, 2000, S. K. Iskander and M. A. Sokolov traveled to Philadelphia, Pennsylvania, to participate in the ASTM Committee E8 meetings and the 32nd National Symposium on Fatigue and Fracture.

On June 17-25, R. K. Nanstad traveled to Vienna, Austria, to participate in the International Atomic Energy Agency (IAEA) Coordinated Research Program meetings on Effects of Nickel in Reactor Pressure Vessel Steels.

4. PRESENTATIONS, REPORTS, PAPERS, AND PUBLICATIONS:

S. K. Iskander, R. K. Nanstad, C. A. Baldwin, D. W. Heatherly, and I. Remec, "Reirradiation Response Rate of a High-Copper Reactor Pressure Vessel Weld," presented by S. K. Iskander at the 20th Symposium on the Effects of Radiation on Materials, Williamsburg, Virginia, June 6-8, 2000. A subsequent publication will appear in ASTM STP 1405.

M. K. Miller, K.F. Russell, J. Kocik and E. Keilova, "Atom Probe Tomography of 15Kh2MFA Cr-Mo-V Steel Surveillance Specimens," presented by M. K. Miller at the 20th International Symposium on the Effects of Radiation on Materials, Williamsburg, Virginia, June 6-8, 2000. Note this was not submitted to the ASTM conference proceedings since it was already accepted for publication in the Journal of Nuclear Materials.

R. K. Nanstad, D. E. McCabe, M. A. Sokolov, C. A. English, and S. R. Ortner, "Investigation of Temper Embrittlement in Reactor Pressure Vessel Steels Following Thermal Aging, Irradiation, and Thermal Annealing," presented by R. K. Nanstad at the 20th Symposium on the Effects of Radiation on Materials, Williamsburg, Virginia, June 6-8, 2000. A subsequent publication will appear in ASTM STP 1405.

R. E. Stoller, "An Evaluation of Through-Thickness Changes in Primary Damage Production in Commercial Reactor Pressure Vessels," presented by R. E. Stoller at the 20th International Symposium on the Effects of Radiation on Materials, Williamsburg, Virginia, June 6-8, 2000. A subsequent publication will appear in ASTM STP 1405.

5. PROPERTY ACQUIRED:

Items listed in this section include all nonconsumable project purchases that were actually paid for during this reporting period. They do not include either accruals or accrual reversals and hence may not accurately reflect total material procurement charges within this period.

Item	Cost ($)
None	

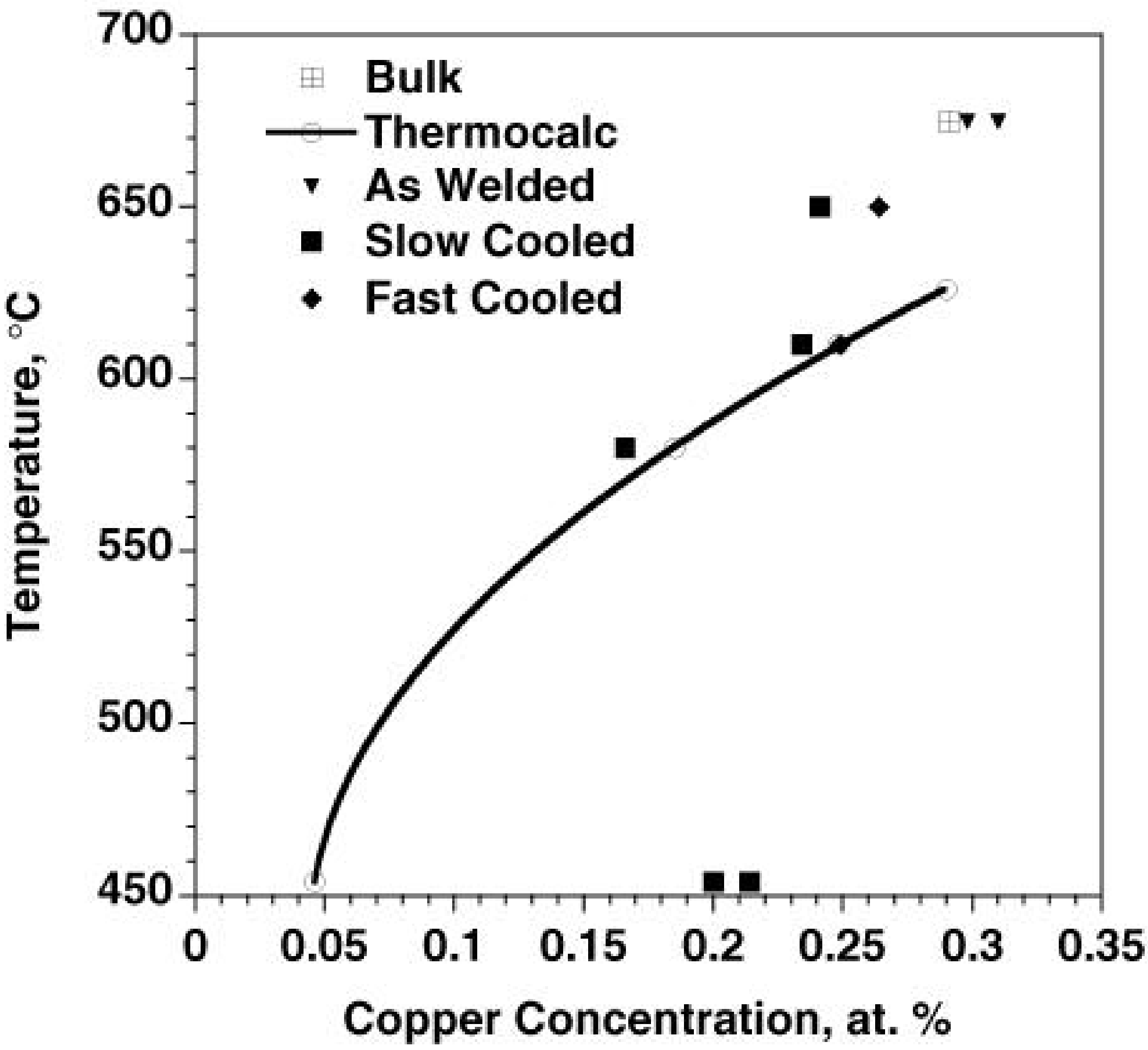
6. PROBLEM AREAS:

The MTS 100-kip servo-hydraulic machine in the hot cell developed an oil leak necessitating that testing of the KS-01 compact specimens be stopped (subtask 2.2). The actuator of another machine will be reconditioned and used to replace the existing rig. Although the total cost and time of this effort is not yet known, it is anticipated that the repair will be completed in late July or early August, depending on other activities at the hot cell facility, primarily the crane replacement. The cost of the repair and replacement will be shared among the ORNL Fusion, APT, and HSSI programs. It is also anticipated that testing of the PSI specimens (subtask 3.3) may be delayed until the next fiscal year.

Hot cell charges have been increased by 25% due to higher than planned costs required to operate the Irradiated Materials Evaluation and Testing facility. Discussions are being held to determine the impact on the Program and options for next fiscal year with ORNL M&C Division senior management.

7. PLANS FOR THE NEXT REPORTING PERIOD:

The plans for the next reporting period are described in Section 2.



Temperature, °C
700
650
600
550
500
450
Bulk
Thermocalc
As Welded
Slow Cooled
Fast Cooled
0
0.05
0.1
0.15
0.2
0.25
0.3
0.35
Copper Concentration, at. %

FINANCIAL STATUS for W6953 — Reporting Period: 5/27/00-6/25/00

		Current Month (MM)	Fiscal Year to Date (MY)	Cumulative Project to date (MY)
I.	Direct Staff Effort	10	7.8	27.7
II.	A. Direct Lab Staff Effort ($)			
	Direct Salaries	81,713	748,737	2,801,976
	Materials and Services	3,847	24,886	346,050
	ADP Support	61	601	1,602
	Subcontracts	6,942	79,307	276,611
	Travel	9,409	16,442	106,950
	Indirect Labor Costs	0	0	0
	Other: NRC PO Tax	4,000	37,000	130,500
	General and Administrative	37,488	330,841	1,277,691
	Total LMER Costs	143,460	1,237,814	4,941,380
	B. DOE Added Factor Costs	0	0	0
	TOTAL PROJECT COSTS	143,460	1,237,814	4,941,380

Percentage of available cumulative funds costed	88
Percentage of available current FY funds costed	65
Funds Remaining	668,620

III. Funding Status

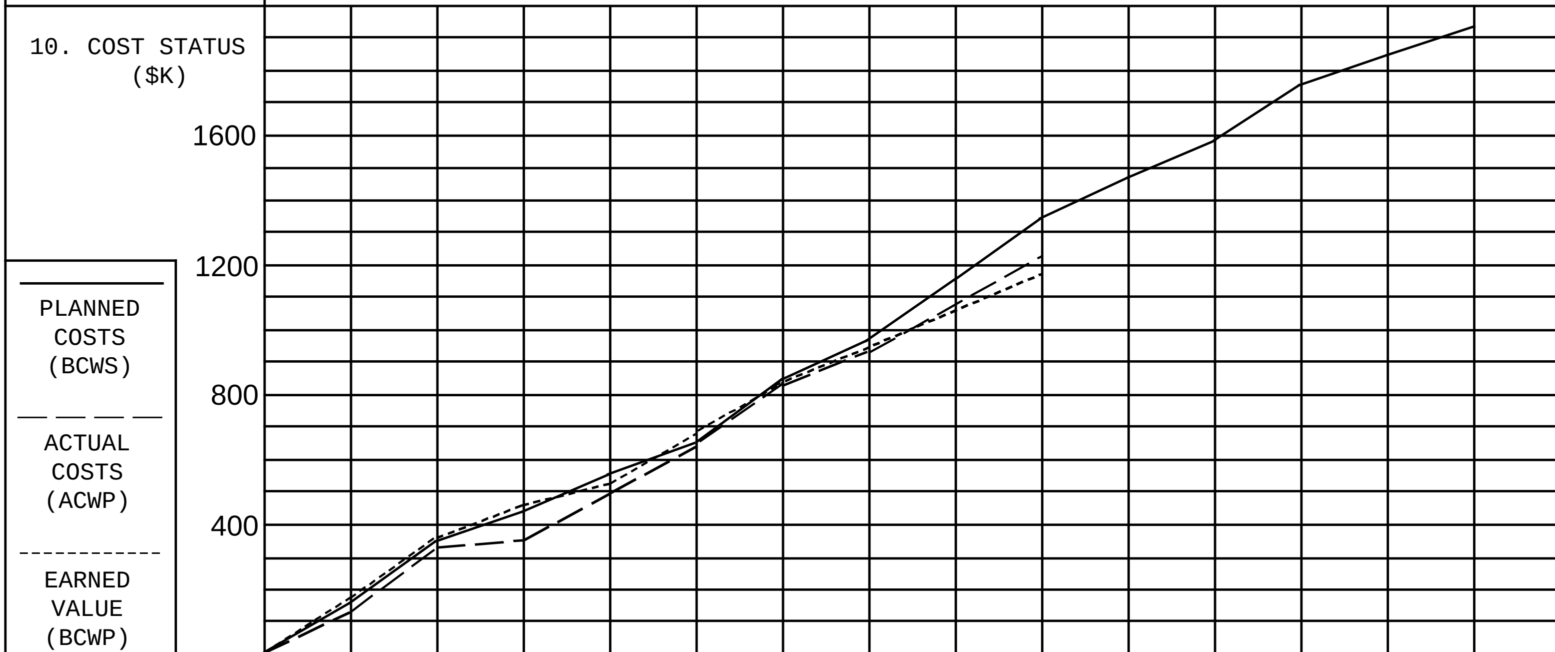
Prior FY Carryover	FY 00 Projected Funding Level	FY 00 Funds Received to Date	FY 00 Funding Balance Needed	Cumulative Amt. Obligated	Cumulative Amt. Costed
306,434	1,625,000	1,600,000	25,000	5,610,000	4,941,380

Comments:

1. CONTRACT REPORTING ELEMENT **HSSI - Heavy-Section Steel Irradiation Program**	2. REPORTING PERIOD **5/29/00 - 6/25/00**	3. JCN NO. **W6953**
4. CONTRACTOR (NAME AND ADDRESS) **OAK RIDGE NATIONAL LABORATORY** **P.O. BOX 2008** **OAK RIDGE, TN 37831**	5. CONTRACT PERIOD **FY 1999-2000** 7. NRC B&R NO. **860 15 21 20 05**	6. ACTIVITY NUMBER **41 W6 95 3W 1** 8. DOE B&R NO. **40 10 01 06**

9. MONTHS: O N D J F M A M J J A S O N D

10. COST STATUS ($K)



COST PLAN DATES: 1/31/00

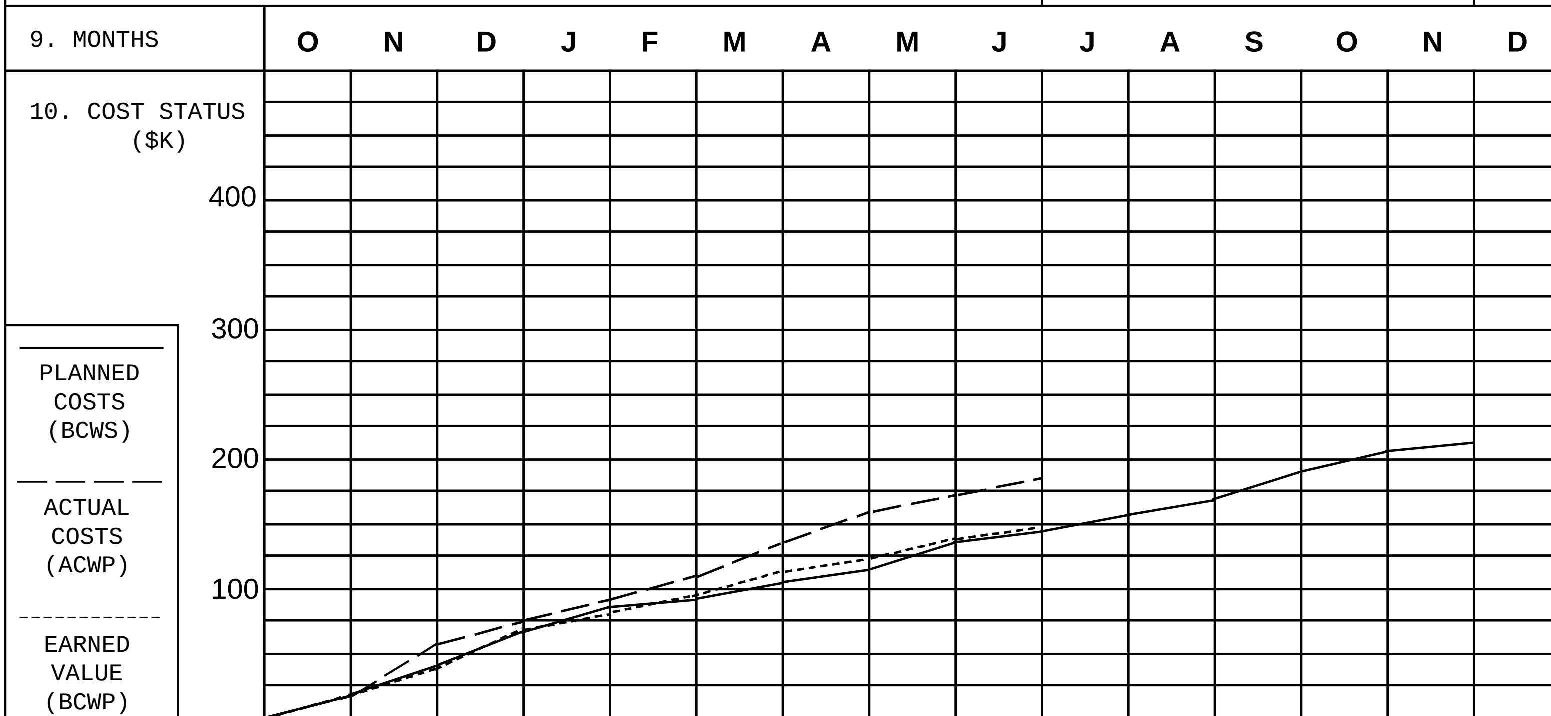
PLANNED COSTS FOR ELEMENT ($K): 1,906

ELEMENT COSTS FOR PRIOR FYS ($K): 306

ACCRUED COSTS ($K)	O	N	D	J	F	M	A	M	J	J	A	S	O	N	D
PLANNED	168	156	99	115	118	166	163	166	172	142	132	140	100	69	
ACTUAL	113	207	29	149	153	159	137	147	144						
EARNED	140	157	104	107	172	139	137	112	122						
CUM. PLAN.	168	324	423	538	656	822	985	1151	1323	1465	1597	1737	1837	1906	
CUM. ACT.	113	320	349	498	651	810	947	1094	1238						
CUM. EARN.	177	334	434	508	680	819	956	1068	1190						

11. REMARKS:

1. CONTRACT REPORTING ELEMENT **HSSI - 1. Program Management**	2. REPORTING PERIOD **5/29/00 - 6/25/00**	3. JCN NO. **W6953**
4. CONTRACTOR (NAME AND ADDRESS) **OAK RIDGE NATIONAL LABORATORY** **P.O. BOX 2008** **OAK RIDGE, TN 37831**	5. CONTRACT PERIOD **FY 1999-2000** 7. NRC B&R NO. **860 15 21 20 05**	6. ACTIVITY NUMBER **41 W6 95 3W 1** 8. DOE B&R NO. **40 10 01 06**



COST PLAN DATES

1/4/00

PLANNED COSTS FOR ELEMENT ($K)

219

ELEMENT COSTS FOR PRIOR FYS ($K)

29

ACCRUED COSTS ($K)

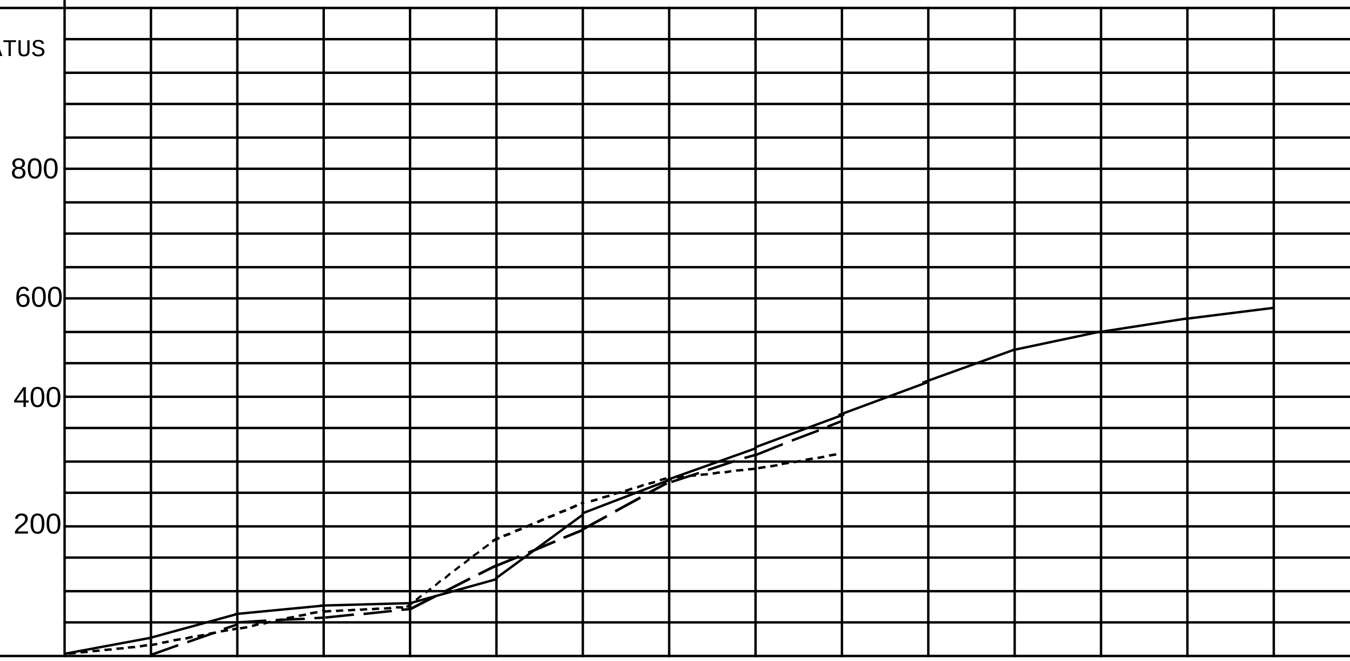
	O	N	D	J	F	M	A	M	J	J	A	S	O	N	D
PLANNED	18	25	21	17	13	11	12	13	15	12	14	20	13	15	
ACTUAL	18	37	20	17	21	19	25	15	16						
EARNED	18	24	23	14	18	13	14	12	15						
CUM. PLAN.	18	43	64	81	94	105	117	130	145	157	171	191	204	219	
CUM. ACT.	18	55	75	92	113	132	157	172	188						
CUM. EARN.	18	42	65	79	97	110	124	136	151						

11. REMARKS:

1. CONTRACT REPORTING ELEMENT **HSSI - 2. Fracture Toughness Transition and MC Methodology**	2. REPORTING PERIOD **5/29/00 - 6/25/00**	3. JCN NO. **W6953**
4. CONTRACTOR (NAME AND ADDRESS) **OAK RIDGE NATIONAL LABORATORY** **P.O. BOX 2008** **OAK RIDGE, TN 37831**	5. CONTRACT PERIOD **FY 1999-2000** 7. NRC B&R NO. **860 15 21 20 05**	6. ACTIVITY NUMBER **41 W6 95 3W 1** 8. DOE B&R NO. **40 10 01 06**

9. MONTHS: O N D J F M A M J J A S O N D

10. COST STATUS ($K)



PLANNED COSTS (BCWS) ———

ACTUAL COSTS (ACWP) — — —

EARNED VALUE (BCWP) - - - - -

COST PLAN DATES: 1/31/00

PLANNED COSTS FOR ELEMENT ($K): 539

ELEMENT COSTS FOR PRIOR FYS ($K): 21

ACCRUED COSTS ($K)	O	N	D	J	F	M	A	M	J	J	A	S	O	N	D
PLANNED	29	25	14	20	36	80	57	55	47	52	45	39	25	15	
ACTUAL	-18	43	14	50	53	53	63	51	44						
EARNED	24	24	11	26	89	59	36	20	18						
CUM. PLAN.	29	54	68	88	124	204	261	316	363	415	460	499	524	539	
CUM. ACT.	-18	25	39	89	142	195	258	309	353						
CUM. EARN.	24	48	59	87	174	233	269	289	307						

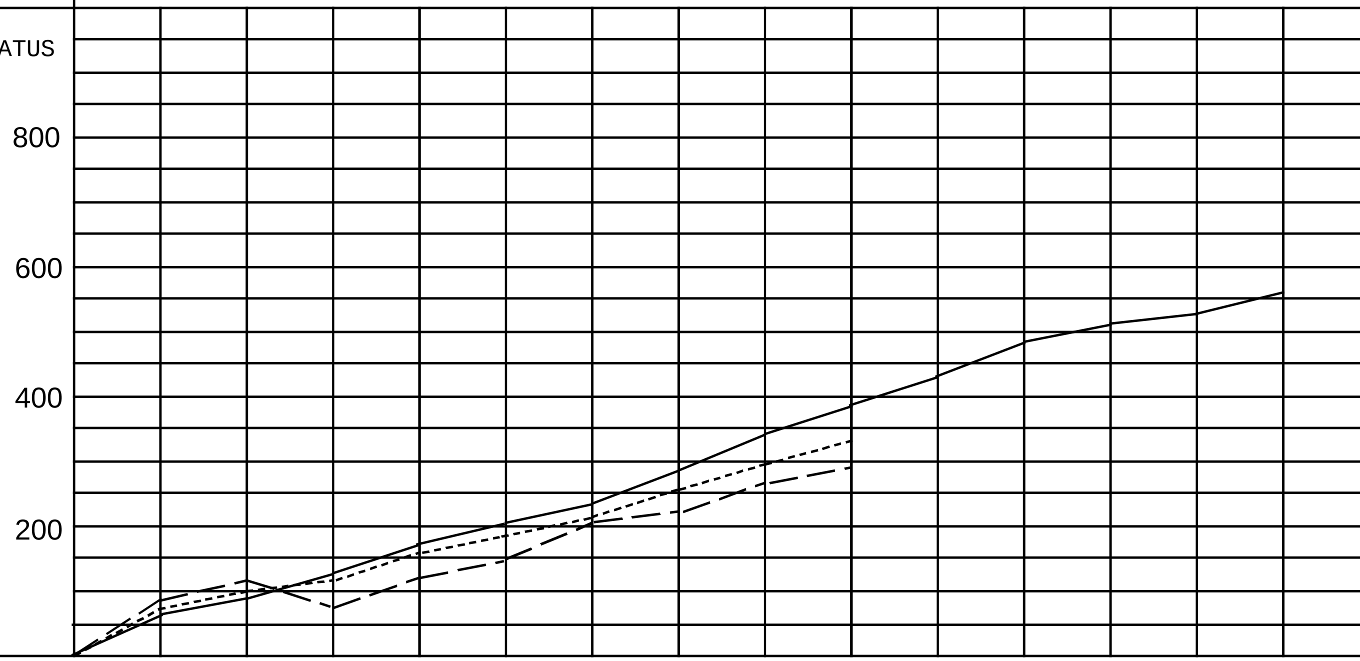
11. REMARKS:

1. CONTRACT REPORTING ELEMENT	2. REPORTING PERIOD	3. JCN NO.
HSSI - 3. Irradiation Embrittlement of RPV Steel	**5/29/00 - 6/25/00**	**W6953**

4. CONTRACTOR (NAME AND ADDRESS)	5. CONTRACT PERIOD	6. ACTIVITY NUMBER
OAK RIDGE NATIONAL LABORATORY **P.O. BOX 2008** **OAK RIDGE, TN 37831**	**FY 1999-2000**	**41 W6 95 3W 1**
	7. NRC B&R NO. **860 15 21 20 05**	8. DOE B&R NO. **40 10 01 06**

9. MONTHS: O N D J F M A M J J A S O N D

10. COST STATUS ($K)



Legend:
——— PLANNED COSTS (BCWS)
— — — — ACTUAL COSTS (ACWP)
------------ EARNED VALUE (BCWP)

COST PLAN DATES: 1/31/00

PLANNED COSTS FOR ELEMENT ($K): 552

ELEMENT COSTS FOR PRIOR FYS ($K): 167

ACCRUED COSTS ($K)

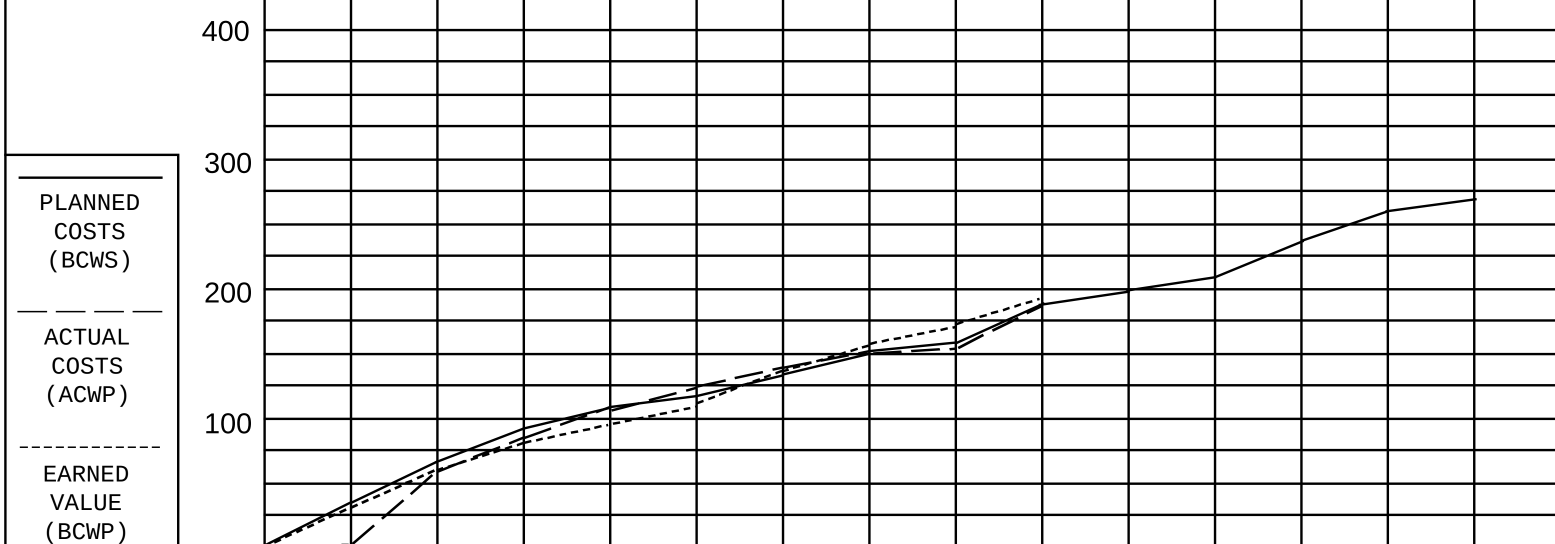
	O	N	D	J	F	M	A	M	J	J	A	S	O	N	D
PLANNED	52	43	30	41	35	42	46	52	51	41	41	32	24	22	
ACTUAL	92	31	-50	48	28	62	17	32	35						
EARNED	48	42	29	33	28	33	38	40	41						
CUM. PLAN.	52	95	125	166	201	243	289	341	392	433	474	506	530	552	
CUM. ACT.	92	123	73	121	149	211	228	260	295						
CUM. EARN.	48	90	119	152	180	213	251	291	332						

11. REMARKS:

1. CONTRACT REPORTING ELEMENT **HSSI - 4. Validation of Irradiated and Aged Materials**	2. REPORTING PERIOD **5/29/00 - 6/25/00**	3. JCN NO. **W6953**
4. CONTRACTOR (NAME AND ADDRESS) **OAK RIDGE NATIONAL LABORATORY** **P.O. BOX 2008** **OAK RIDGE, TN 37831**	5. CONTRACT PERIOD **FY 1999-2000** 7. NRC B&R NO. **860 15 21 20 05**	6. ACTIVITY NUMBER **41 W6 95 3W 1** 8. DOE B&R NO. **40 10 01 06**

9. MONTHS: O N D J F M A M J J A S O N D

10. COST STATUS ($K)



COST PLAN DATES: 1/31/00

PLANNED COSTS FOR ELEMENT ($K): 272

ELEMENT COSTS FOR PRIOR FYS ($K): 30

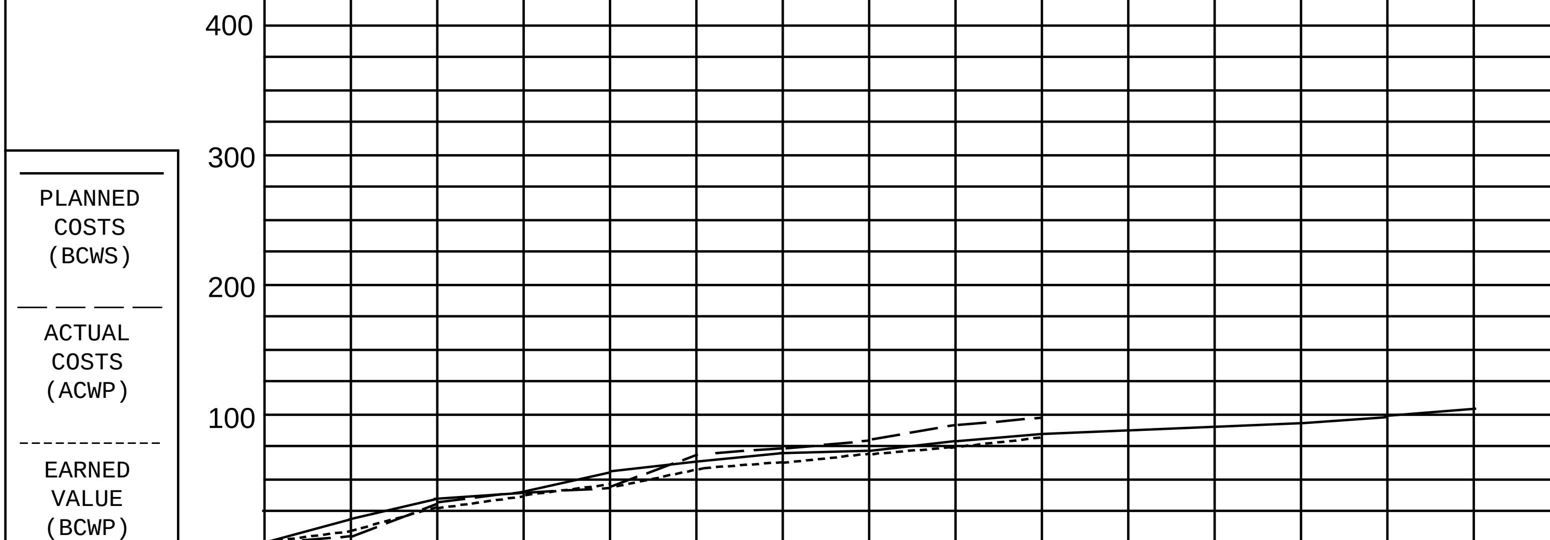
ACCRUED COSTS ($K)	O	N	D	J	F	M	A	M	J	J	A	S	O	N	D
PLANNED	35	37	20	15	11	12	20	15	18	17	13	23	22	14	
ACTUAL	1	57	29	20	17	13	14	11	26						
EARNED	30	31	23	14	15	18	23	14	18						
CUM. PLAN.	35	72	92	107	118	130	150	165	183	200	213	236	258	272	
CUM. ACT.	1	58	87	107	124	137	151	162	188						
CUM. EARN.	30	61	84	98	113	131	154	168	186						

11. REMARKS:

1. CONTRACT REPORTING ELEMENT	2. REPORTING PERIOD	3. JCN NO.
HSSI - 5. Modeling and Microstructural Analysis	**5/29/00 - 6/25/00**	**W6953**
4. CONTRACTOR (NAME AND ADDRESS)	5. CONTRACT PERIOD	6. ACTIVITY NUMBER
OAK RIDGE NATIONAL LABORATORY	**FY 1999-2000**	**41 W6 95 3W 1**
P.O. BOX 2008	7. NRC B&R NO.	8. DOE B&R NO.
OAK RIDGE, TN 37831	**860 15 21 20 05**	**40 10 01 06**

9. MONTHS: O N D J F M A M J J A S O N D

10. COST STATUS ($K)



COST PLAN DATES: 1/4/00

PLANNED COSTS FOR ELEMENT ($K): 102

ELEMENT COSTS FOR PRIOR FYS ($K): 42

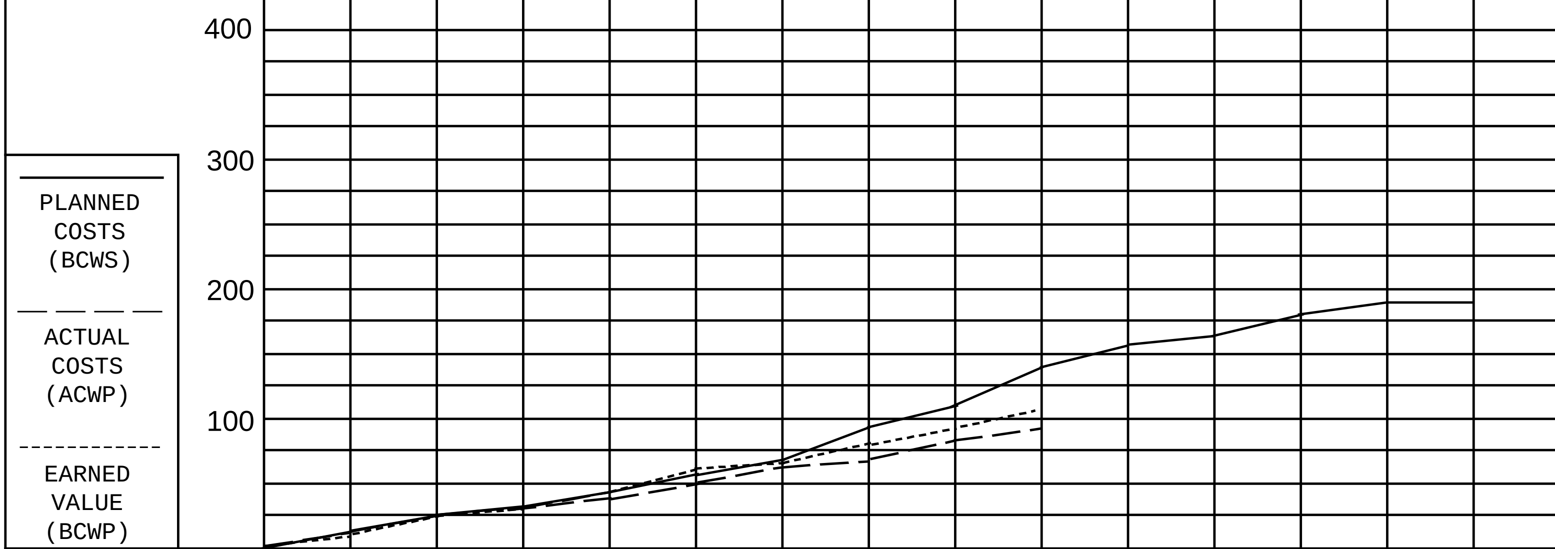
ACCRUED COSTS ($K)	O	N	D	J	F	M	A	M	J	J	A	S	O	N	D
PLANNED	20	15	5	12	13	5	3	3	6	4	3	5	5	3	
ACTUAL	4	29	7	5	24	5	6	10	8						
EARNED	5	25	9	9	10	4	7	7	8						
CUM. PLAN.	20	35	40	52	65	70	73	76	82	86	89	94	99	102	
CUM. ACT.	4	33	40	45	69	74	80	90	98						
CUM. EARN.	5	30	39	48	58	62	69	75	84				6		

11. REMARKS:

1. CONTRACT REPORTING ELEMENT **HSSI - 6. Irradiation Coordination**	2. REPORTING PERIOD **5/29/00 - 6/25/00**	3. JCN NO. **W6953**
4. CONTRACTOR (NAME AND ADDRESS) **OAK RIDGE NATIONAL LABORATORY** **P.O. BOX 2008** **OAK RIDGE, TN 37831**	5. CONTRACT PERIOD **FY 1999-2000** 7. NRC B&R NO. **860 15 21 20 05**	6. ACTIVITY NUMBER **41 W6 95 3W 1** 8. DOE B&R NO. **40 10 01 06**

9. MONTHS: O N D J F M A M J J A S O N D

10. COST STATUS ($K)



COST PLAN DATES: 1/4/00

PLANNED COSTS FOR ELEMENT ($K): 187

ELEMENT COSTS FOR PRIOR FYS ($K): 17

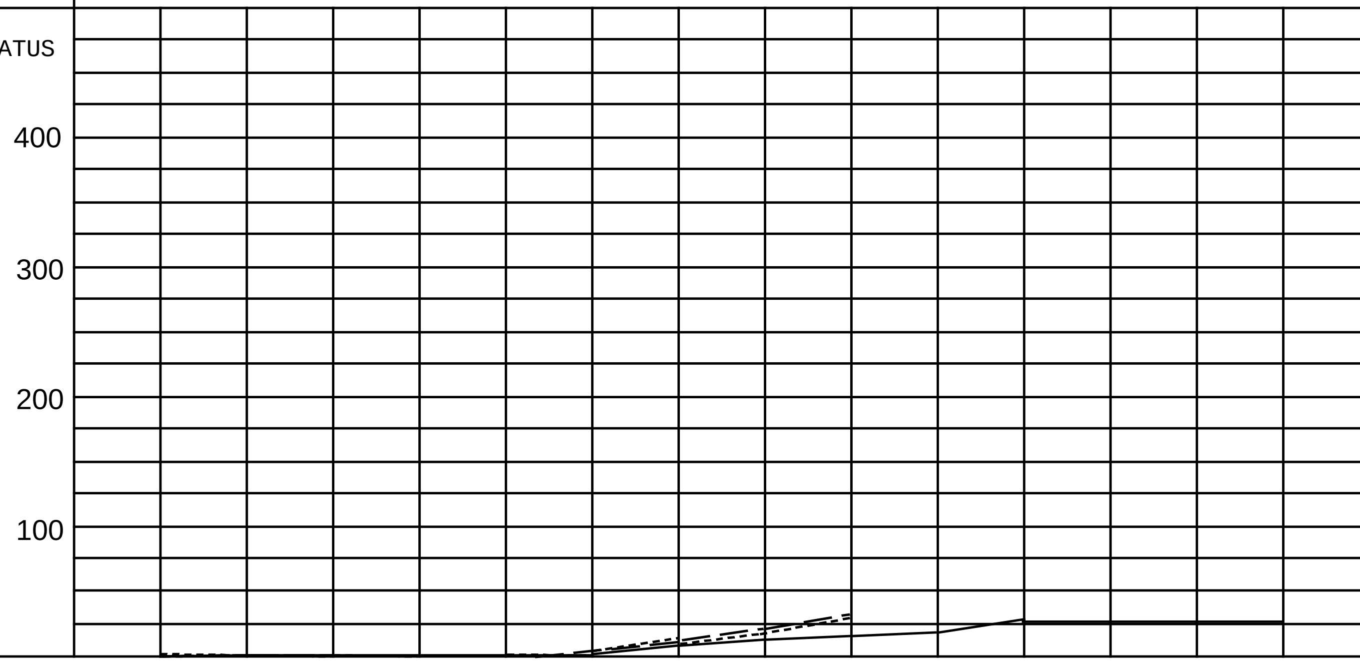
ACCRUED COSTS ($K)	O	N	D	J	F	M	A	M	J	J	A	S	O	N	D
PLANNED	10	9	10	10	10	15	20	23	30	11	11	11	11	0	
ACTUAL	16	9	9	9	10	7	4	16	8						
EARNED	15	10	9	11	12	12	11	11	13						
CUM. PLAN.	16	25	35	45	55	70	90	113	143	154	165	176	187	187	
CUM. ACT.	16	25	34	43	53	60	64	80	88						
CUM. EARN.	15	25	34	45	57	69	80	91	104						

11. REMARKS:

1. CONTRACT REPORTING ELEMENT **HSSI - 7. Embrittlement DB & Dosimetry Evaluation**	2. REPORTING PERIOD **5/29/00 - 6/25/00**	3. JCN NO. **W6953**
4. CONTRACTOR (NAME AND ADDRESS) **OAK RIDGE NATIONAL LABORATORY** **P.O. BOX 2008** **OAK RIDGE, TN 37831**	5. CONTRACT PERIOD **FY 1999-2000** 7. NRC B&R NO. **860 15 21 20 05**	6. ACTIVITY NUMBER **41 W6 95 3W 1** 8. DOE B&R NO. **40 10 01 06**

9. MONTHS: O N D J F M A M J J A S O N D

10. COST STATUS ($K)



PLANNED COSTS (BCWS) ———

ACTUAL COSTS (ACWP) — — —

EARNED VALUE (BCWP) - - - - -

COST PLAN DATES: 1/4/00

PLANNED COSTS FOR ELEMENT ($K): 26

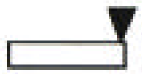
ELEMENT COSTS FOR PRIOR FYS ($K): 1

ACCRUED COSTS ($K)	O	N	D	J	F	M	A	M	J	J	A	S	O	N	D
PLANNED	0	1	0	0	0	0	5	5	5	5	5	0	0	0	
ACTUAL	0	1	0	0	0	0	7	12	7						
EARNED	0	1	0	0	0	0	8	8	9						
CUM. PLAN.	0	1	1	1	1	1	6	11	16	21	26	26	26	26	
CUM. ACT.	0	1	1	1	1	1	8	20	27						
CUM. EARN.	0	1	1	1	1	1	9	17	26						

11. REMARKS:

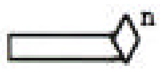
Milestone Symbology

 Intermediate milestone planned

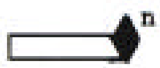
 Intermediate milestone completed

 Major milestone planned

 Major milestone completed



Rescheduled milestone planned

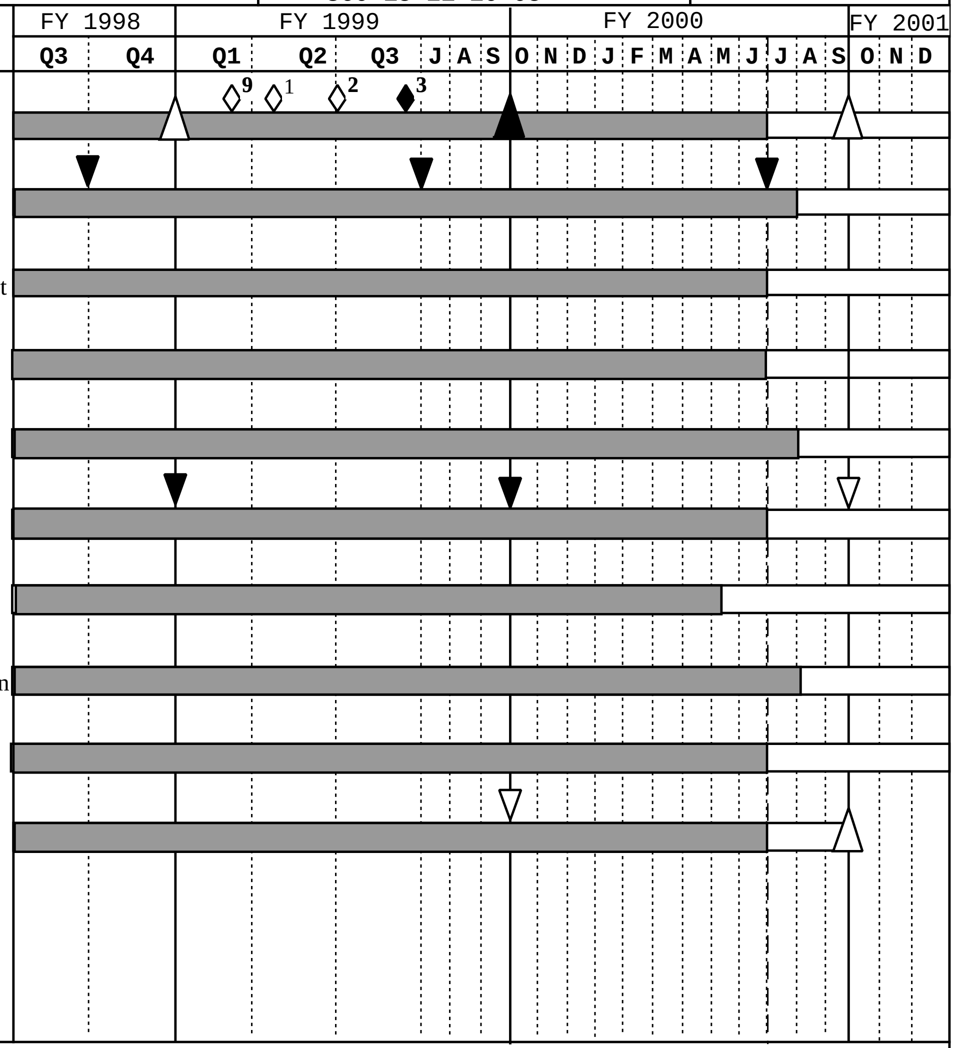


Rescheduled milestone completed

n = number of calendar-year month in which milestone was rescheduled

1. CONTRACT REPORTING ELEMENT **HSSI - 1. Program Management**	2. REPORTING PERIOD **5/29/00 - 6/25/00**	3. JCN NO. **W6953**
4. CONTRACTOR (NAME AND ADDRESS) **OAK RIDGE NATIONAL LABORATORY** **P.O. BOX 2008** **OAK RIDGE, TN 37831**	5. CONTRACT PERIOD **FY 1998-2001** 7. NRC B&R NO. **860 15 21 20 05**	6. ACTIVITY NO. **41 W6 95 3W 1** 8. DOE B&R NO. **40 10 01 06**

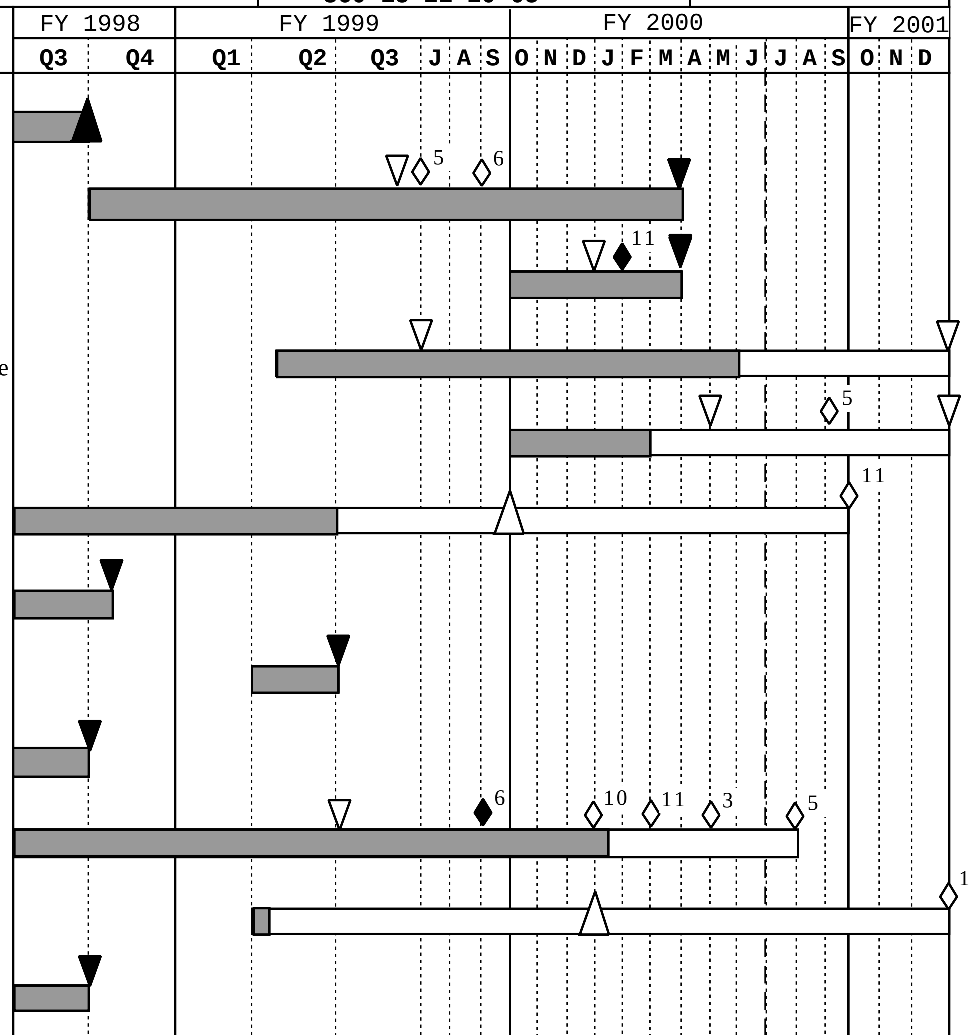
9. MILESTONE IDEN. NO.	10. MILESTONE DESCRIPTION
1.1.A.	Issue Project & Budget Proposal
1.1.B.	Select and Administer Subcontracts
1.2.A.	Issue Earned Value Based Monthly Management Reports (by the end of subsequent month)
1.2.B.	Ensure QA Requirements are met
1.3.A.	Participate in Appropriate Codes and Standards Committees
1.3.B.	Participate in NRC-Sponsored Meetings and Discussions
1.3.C.	Coordinate NRC and Internal Reviews
1.3.D.	Coordinate Domestic and Foreign Information Exchange as Approved by NRC-RES
1.3.E.	Coordinate HSSI Letter and NUREG Reports
1.3.F.	Document the Historical Information Generated by the Old HSSI Program



11. REMARKS

1. CONTRACT REPORTING ELEMENT **HSSI - 2. Fracture Toughness Transition & MC Methodology**	2. REPORTING PERIOD **5/29/00 - 6/25/00**	3. JCN NO. **W6953**
4. CONTRACTOR (NAME AND ADDRESS) **OAK RIDGE NATIONAL LABORATORY** **P.O. BOX 2008** **OAK RIDGE, TN 37831**	5. CONTRACT PERIOD **FY 1998-2001**	6. ACTIVITY NO. **41 W6 95 3W 1**
	7. NRC B&R NO. **860 15 21 20 05**	8. DOE B&R NO. **40 10 01 06**

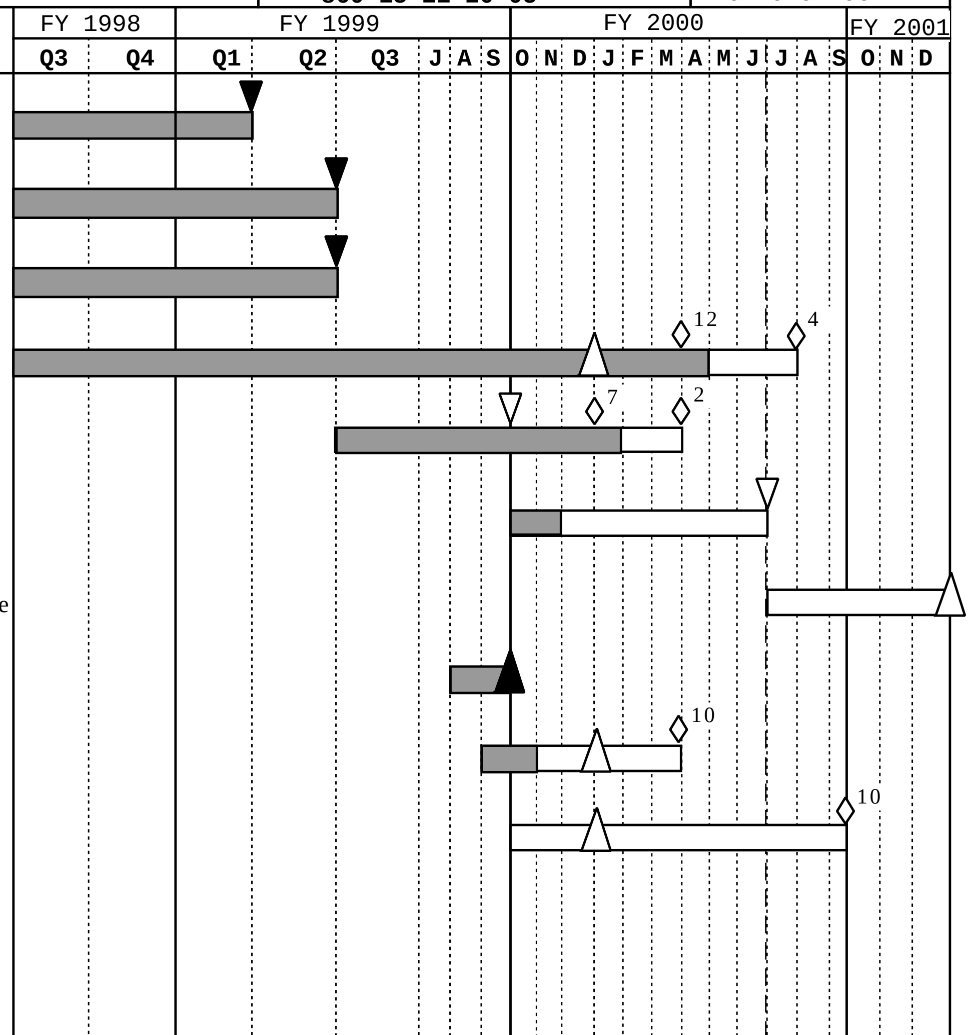
9. MILESTONE IDEN. NO.	10. MILESTONE DESCRIPTION
2.1.A.	Complete Draft NUREG Report on Comparison of CVN and Fracture Toughness Shifts
2.2.A.	Sample Preparation and Irradiation for Master Curve
2.2.B.	Receive Specimens
2.2.C.	Test Unirradiated & Irradiated Master Curve Specimens
2.2.D.	Draft Letter and NUREG Reports
2.3.A.	Design, Fabrication, Calibration, Evaluation and NUREG Report for Phase I
2.4.A.	Midland Weld Evaluations
2.4.B.	Pressure Vessel and Piping (ASME) Report
2.5.A.1.	Test Midland Crack Arrest Specimens
2.5.A.2.	Analyze Crack Arrest Data & Draft NUREG
2.5.B.	Prepare a Comprehensive NUREG
2.6.A.	IG Fracture Obtain & Machine HT Pieces



11. REMARKS

1. CONTRACT REPORTING ELEMENT **HSSI - 2. Fracture Toughness Transition & MC Methodology**	2. REPORTING PERIOD **5/29/00 - 6/25/00**	3. JCN NO. **W6953**
4. CONTRACTOR (NAME AND ADDRESS) **OAK RIDGE NATIONAL LABORATORY** **P.O. BOX 2008** **OAK RIDGE, TN 37831**	5. CONTRACT PERIOD **FY 1998-2001** 7. NRC B&R NO. **860 15 21 20 05**	6. ACTIVITY NO. **41 W6 95 3W 1** 8. DOE B&R NO. **40 10 01 06**

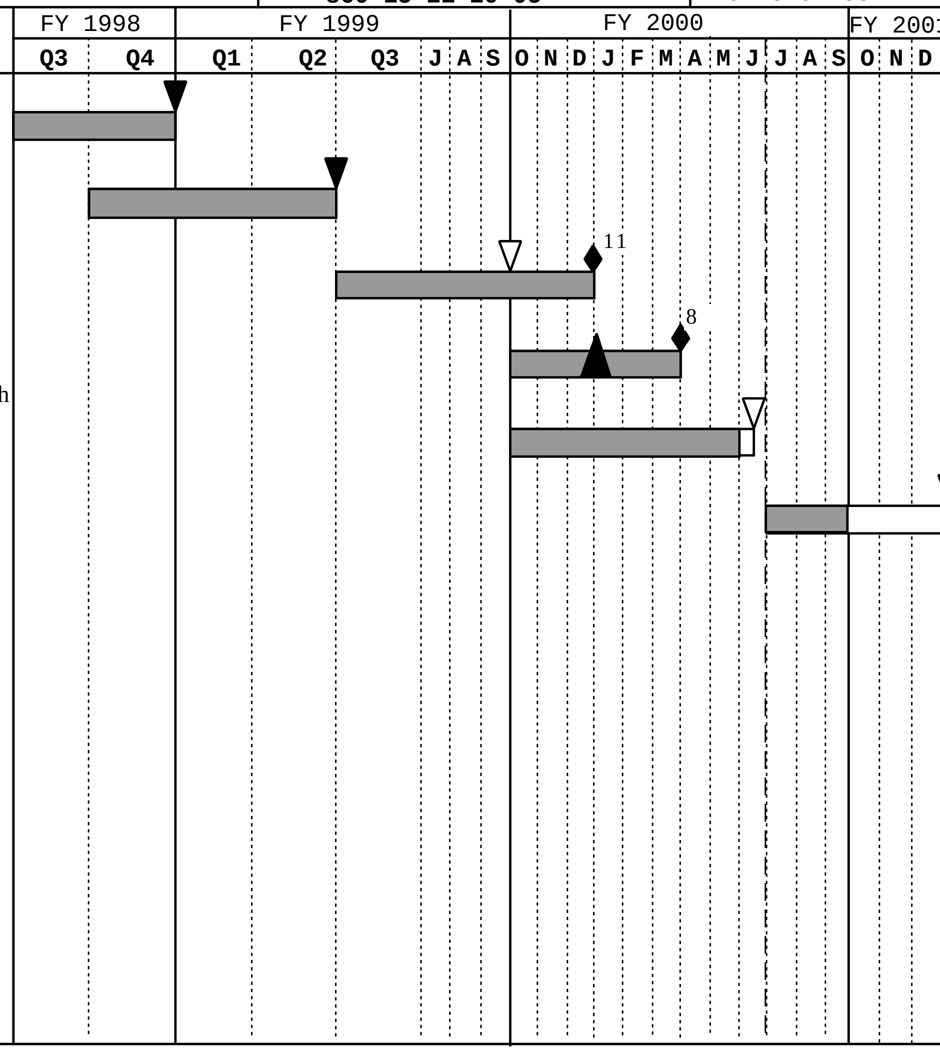
9. MILESTONE IDEN. NO.	10. MILESTONE DESCRIPTION
2.6.B.	Age & Evaluate by CVN
2.6.C.	Machine C(T)s and Test
2.6.D.	MC Impact Evaluations
2.6.E.	Reports and Administration
2.7.A.	Complete Fabrication and Preliminary Testing of Subsize Specimen
2.7.B.	Complete Testing of Subsize Specimens
2.7.C.	Complete NUREG Report on Results of Subsize Specimen Fracture Toughness Tests
2.7.D	Fabricate A302B PCVNs from 3 Heats
2.7.E.	Test and Analyze
2.7.F.	Prepare Letter Report



11. REMARKS

1. CONTRACT REPORTING ELEMENT **HSSI - 2. Fracture Toughness Transition & MC Methodology**	2. REPORTING PERIOD **5/29/00 - 6/25/00**	3. JCN NO. **W6953**
4. CONTRACTOR (NAME AND ADDRESS) **OAK RIDGE NATIONAL LABORATORY** **P.O. BOX 2008** **OAK RIDGE, TN 37831**	5. CONTRACT PERIOD **FY 1998-2001** 7. NRC B&R NO. **860 15 21 20 05**	6. ACTIVITY NO. **41 W6 95 3W 1** 8. DOE B&R NO. **40 10 01 06**

9. MILESTONE IDEN. NO.	10. MILESTONE DESCRIPTION
2.8.A.	Complete Plan for Assembly and Compilation of Surrogate Materials Data Base
2.8.B.	Complete Assembly and Compilation for Unirradiated Materials
2.8.C.	Complete Statistical Analyses of Data Base for Unirradiated Materials
2.8.D.	Complete Draft NUREG Report on Guidelines for use of Surrogate Materials to Establish
2.8.E.	Complete Assembly and Compilation for Irradiated Materials
2.8.F.	Complete Statistical Analysis of Data Base for Irradiated materials



11. REMARKS

1. CONTRACT REPORTING ELEMENT
HSSI - 3. Irradiation Embrittlement of RPV Steel

2. REPORTING PERIOD
5/29/00 - 6/25/00

3. JCN NO.
W6953

4. CONTRACTOR (NAME AND ADDRESS)
OAK RIDGE NATIONAL LABORATORY
P.O. BOX 2008
OAK RIDGE, TN 37831

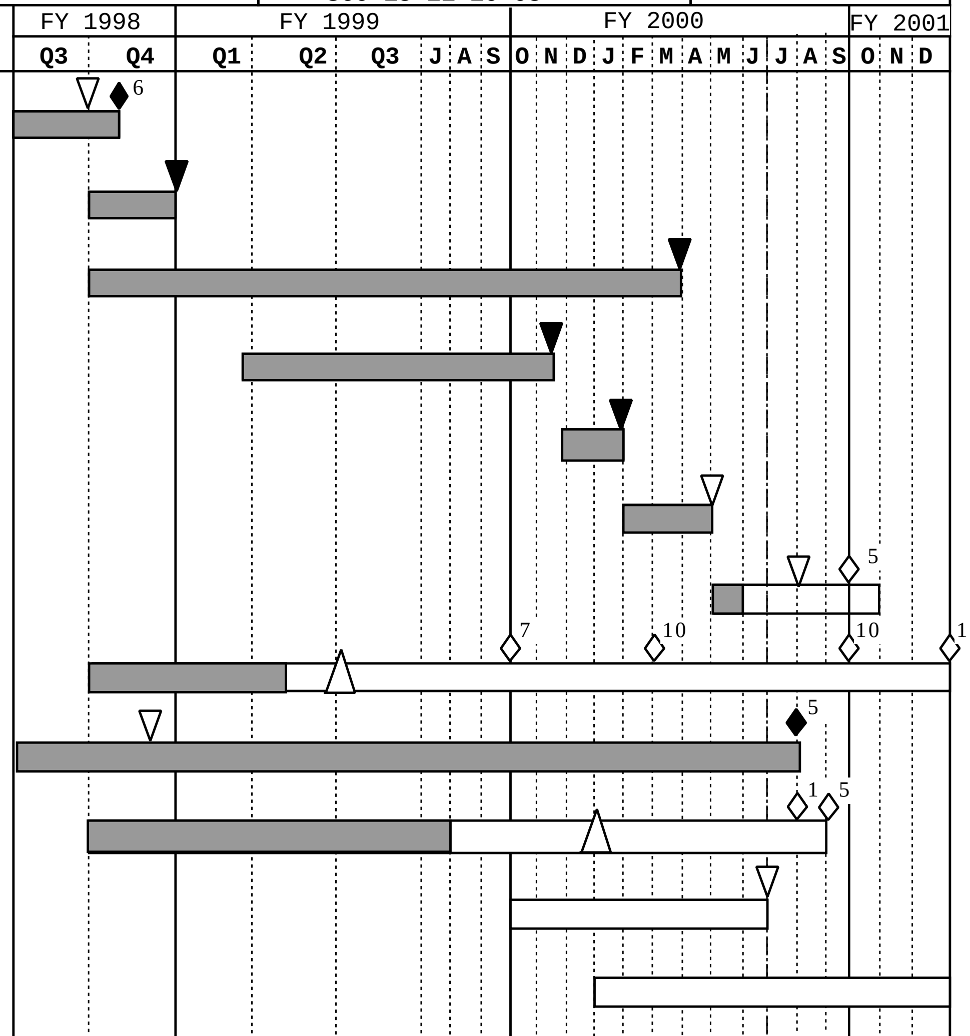
5. CONTRACT PERIOD
FY 1998-2001

6. ACTIVITY NO.
41 W6 95 3W 1

7. NRC B&R NO.
860 15 21 20 05

8. DOE B&R NO.
40 10 01 06

9. MILESTONE IDEN. NO.	10. MILESTONE DESCRIPTION
3.1.A.	Age HAZ Materials
3.1.B.	Machine CVN Specimens
3.1.C.	Evaluate Results and Prepare Letter Report
3.1.D.	Irradiate Capsules
3.1.E.	Ship Specimens
3.1.F.	Test Specimens
3.1.G.	NUREG Report
3.2.A.	NUREG on IA Work to Date
3.2.B.	Dosimetry of 30 CVNs
3.2.C.	NUREG on 30 CVNs (IAR)
3.2.D.	Test Plan for Critical Materials
3.2.E.	IAR of Critical Materials

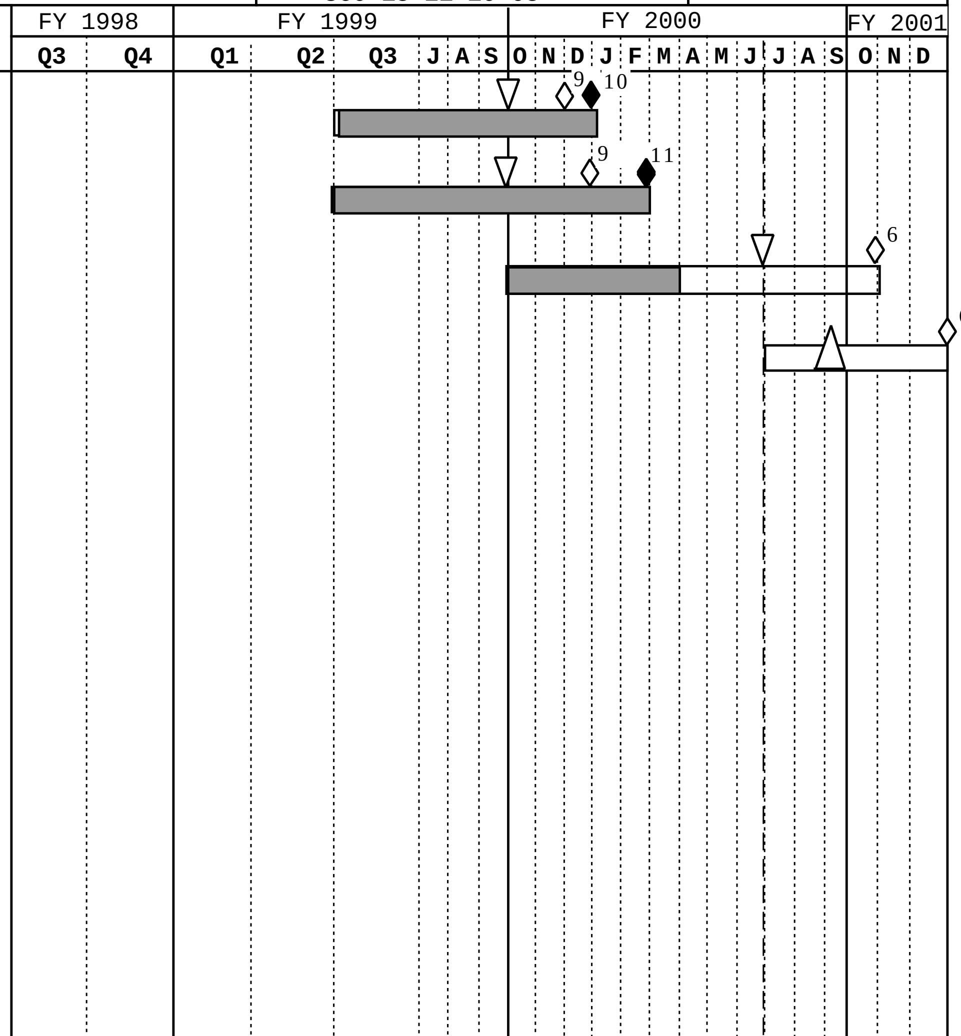


11. REMARKS

1. CONTRACT REPORTING ELEMENT	2. REPORTING PERIOD	3. JCN NO.
HSSI - 3. Irradiation Embrittlement of RPV Steel	**5/29/00 - 6/25/00**	**W6953**

4. CONTRACTOR (NAME AND ADDRESS)	5. CONTRACT PERIOD	6. ACTIVITY NO.
OAK RIDGE NATIONAL LABORATORY	**FY 1998-2001**	**41 W6 95 3W 1**
P.O. BOX 2008	7. NRC B&R NO.	8. DOE B&R NO.
OAK RIDGE, TN 37831	**860 15 21 20 05**	**40 10 01 06**

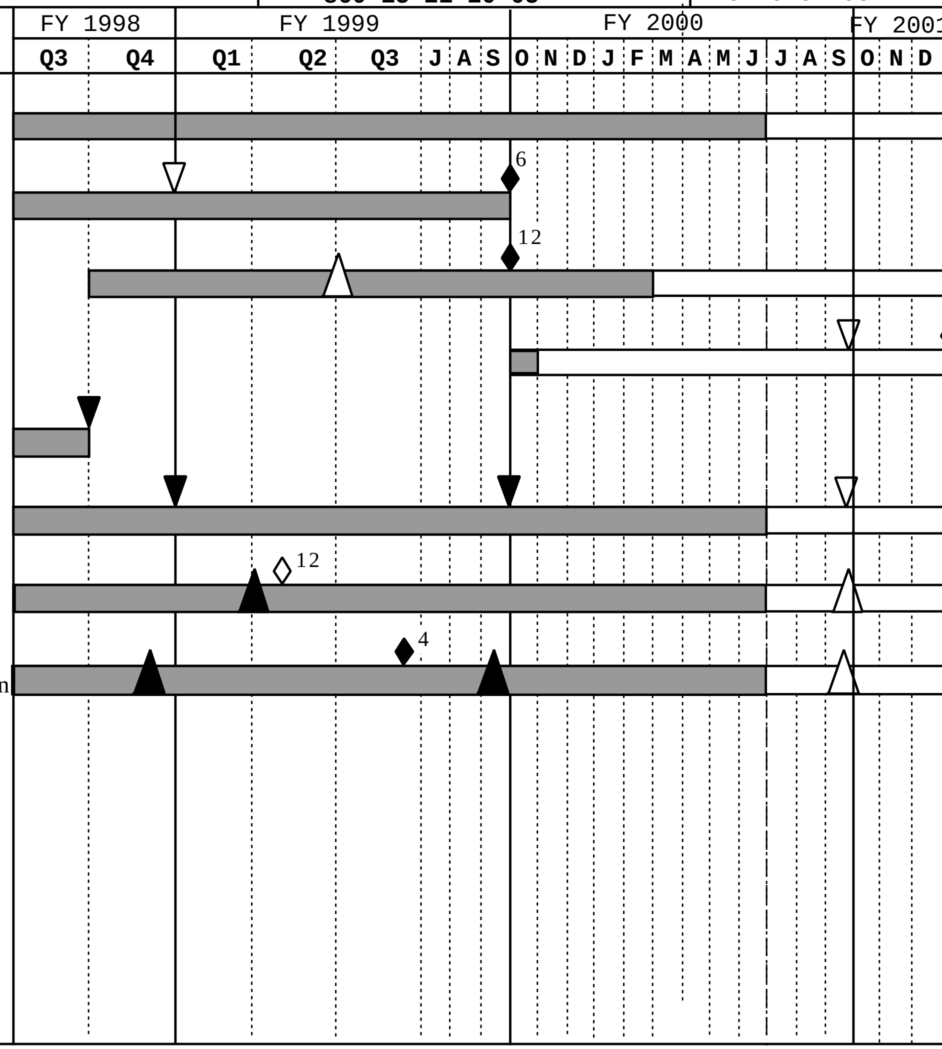
9. MILESTONE IDEN. NO.	10. MILESTONE DESCRIPTION
3.3.A.	Ship JRQ Specimens From PSI to ORNL
3.3.B.	Complete Test Plan
3.3.C.	Complete JRQ Specimen Testing
3.3.D.	Complete Draft NUREG Report on IAR Results of JRQ



11. REMARKS

1. CONTRACT REPORTING ELEMENT **HSSI - 4. Validation of Irradiated and Aged Materials**	2. REPORTING PERIOD **5/29/00 - 6/25/00**	3. JCN NO. **W6953**
4. CONTRACTOR (NAME AND ADDRESS) **OAK RIDGE NATIONAL LABORATORY** **P.O. BOX 2008** **OAK RIDGE, TN 37831**	5. CONTRACT PERIOD **FY 1998-2001** 7. NRC B&R NO. **860 15 21 20 05**	6. ACTIVITY NO. **41 W6 95 3W 1** 8. DOE B&R NO. **40 10 01 06**

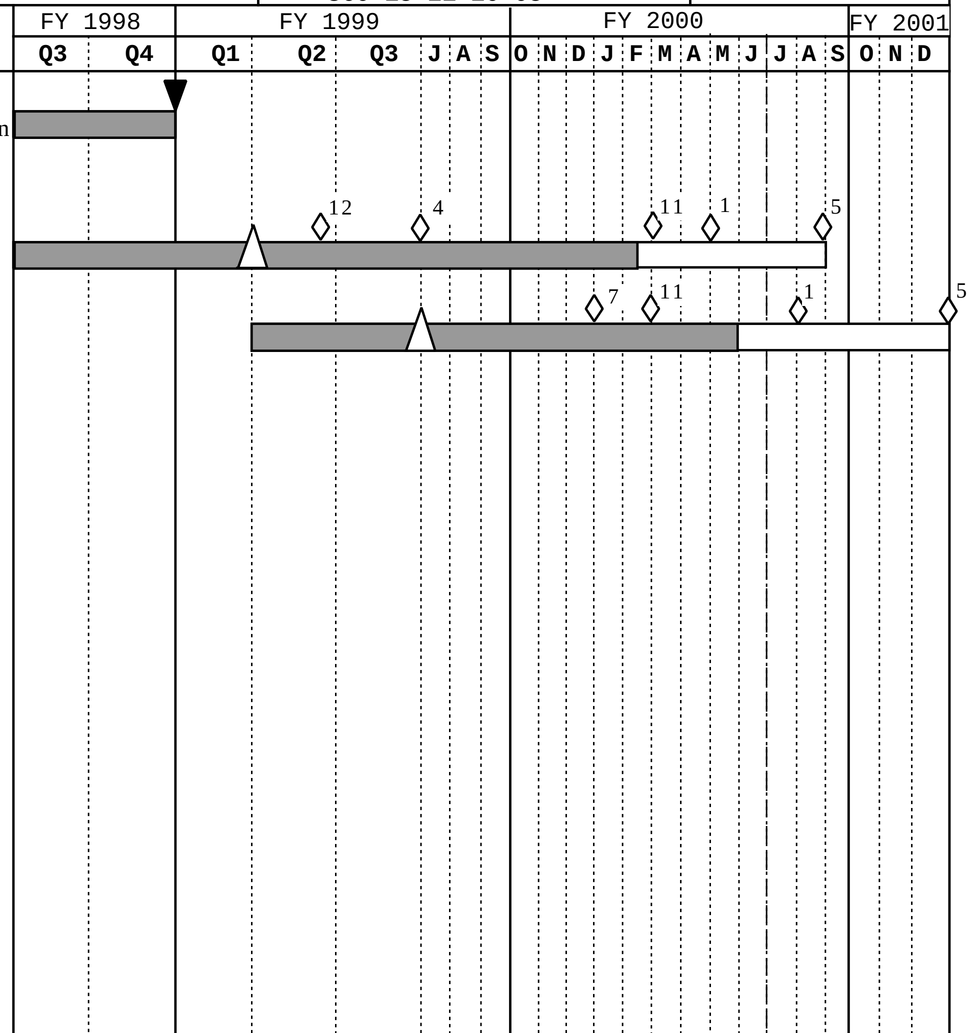
9. MILESTONE IDEN. NO.	10. MILESTONE DESCRIPTION
4.1.1.A.	JPDR Information Exchange with JAERI
4.1.1.B.	Machining & Inspection of JPDR
4.1.1.C.	Testing, Letter & NUREG Report
4.1.3	Maine Yankee RPV Feasibility Study
4.3.B.	Complete Draft NUREG Report on Thermal Aging of SS Welds
4.4.A.	Complete Preparation of List of Anticipated Foreign Travel
4.4.B.	Participate in Periodic Meetings of IGRDM
4.4.C.	Complete Progress Reports of Collaboration Activities



11. REMARKS

1. CONTRACT REPORTING ELEMENT **HSSI - 4. Validation of Irradiated and Aged Materials**	2. REPORTING PERIOD **5/29/00 - 6/25/00**	3. JCN NO. **W6953**
4. CONTRACTOR (NAME AND ADDRESS) **OAK RIDGE NATIONAL LABORATORY** **P.O. BOX 2008** **OAK RIDGE, TN 37831**	5. CONTRACT PERIOD **FY 1998-2001** 7. NRC B&R NO. **860 15 21 20 05**	6. ACTIVITY NO. **41 W6 95 3W 1** 8. DOE B&R NO. **40 10 01 06**

9. MILESTONE IDEN. NO.	10. MILESTONE DESCRIPTION
4.5.A.	Complete Plans for Testing of Specimens in MEA Capsule, Procurement and Testing of Palisades Capsule & Evaluation of PWHT Sheets
4.5.B.	Complete Letter Report Regarding RPV Materials Available for Irradiation Study
4.5.D.	Complete Letter Report on Test results From MEA Capsule

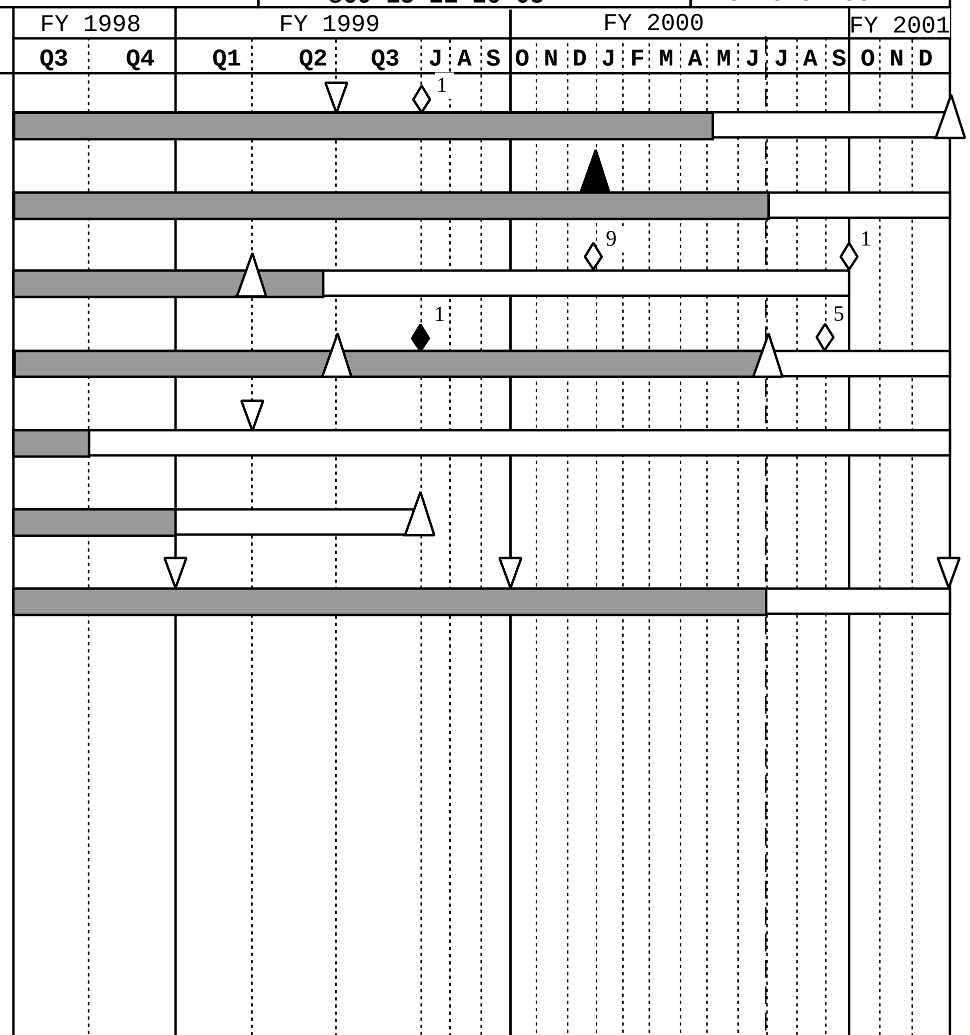


11. REMARKS

1. CONTRACT REPORTING ELEMENT	2. REPORTING PERIOD	3. JCN NO.
HSSI - 5. Modeling & Microstructural Analysis	**5/29/00 - 6/25/00**	**W6953**

4. CONTRACTOR (NAME AND ADDRESS)	5. CONTRACT PERIOD	6. ACTIVITY NO.
OAK RIDGE NATIONAL LABORATORY **P.O. BOX 2008** **OAK RIDGE, TN 37831**	**FY 1998-2001**	**41 W6 95 3W 1**
	7. NRC B&R NO. **860 15 21 20 05**	8. DOE B&R NO. **40 10 01 06**

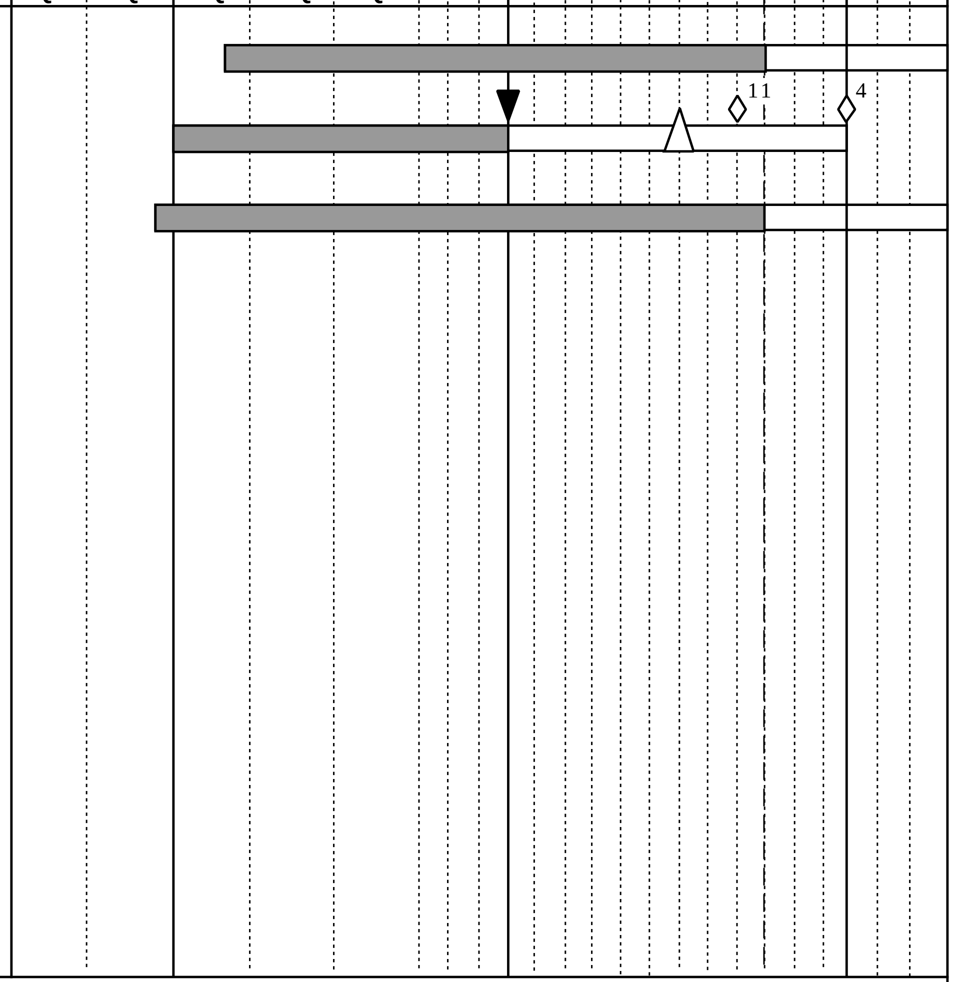
9. MILESTONE IDEN. NO.	10. MILESTONE DESCRIPTION
5.1.A.	Development and Predictive use of Embrittlement Model
5.1.B.	Model Validation and Data Analysis
5.2.A.	Coordinate and Analyze APFIM/SANS/FEGSTEM Round Robin Experiment
5.2.B.	APFIM Characterization
5.3.A.	Conduct and Coordinate Experiments in HFIR HFBR, and FNR
5.3.B.	High-Flux Irradiation-Annealing-Reirradiation in HFIR
5.4	Administration of Task Activities



11. REMARKS

1. CONTRACT REPORTING ELEMENT **HSSI - 6. Irradiation Coordination**	2. REPORTING PERIOD **5/29/00 - 6/25/00**	3. JCN NO. **W6953**
4. CONTRACTOR (NAME AND ADDRESS) **OAK RIDGE NATIONAL LABORATORY** **P.O. BOX 2008** **OAK RIDGE, TN 37831**	5. CONTRACT PERIOD **FY 1998-2001** 7. NRC B&R NO. **860 15 21 20 05**	6. ACTIVITY NO. **41 W6 95 3W 1** 8. DOE B&R NO. **40 10 01 06**

9. MILESTONE IDEN. NO.	10. MILESTONE DESCRIPTION	FY 1998	FY 1999	FY 2000	FY 2001
		Q3 Q4	**Q1 Q2 Q3 J A S**	**O N D J F M A M J J A S**	**O N D**
6.1.A.	Coordinate the Operation, Data Collection, and Maintenance of the HSSI IAR Facility				
6.1.B.	Comprehensive Report on Reusable Irradiation Facilities				
6.2.A.	Coordinate the Operation, Data Collection, and Maintenance of the UCSB Irrad.Facility				



11. REMARKS

1. CONTRACT REPORTING ELEMENT
HSSI - 7. Embrittlement DB & Dosimetry Evaluation

2. REPORTING PERIOD
5/29/00 - 6/25/00

3. JCN NO.
W6953

4. CONTRACTOR (NAME AND ADDRESS)
OAK RIDGE NATIONAL LABORATORY
P.O. BOX 2008
OAK RIDGE, TN 37831

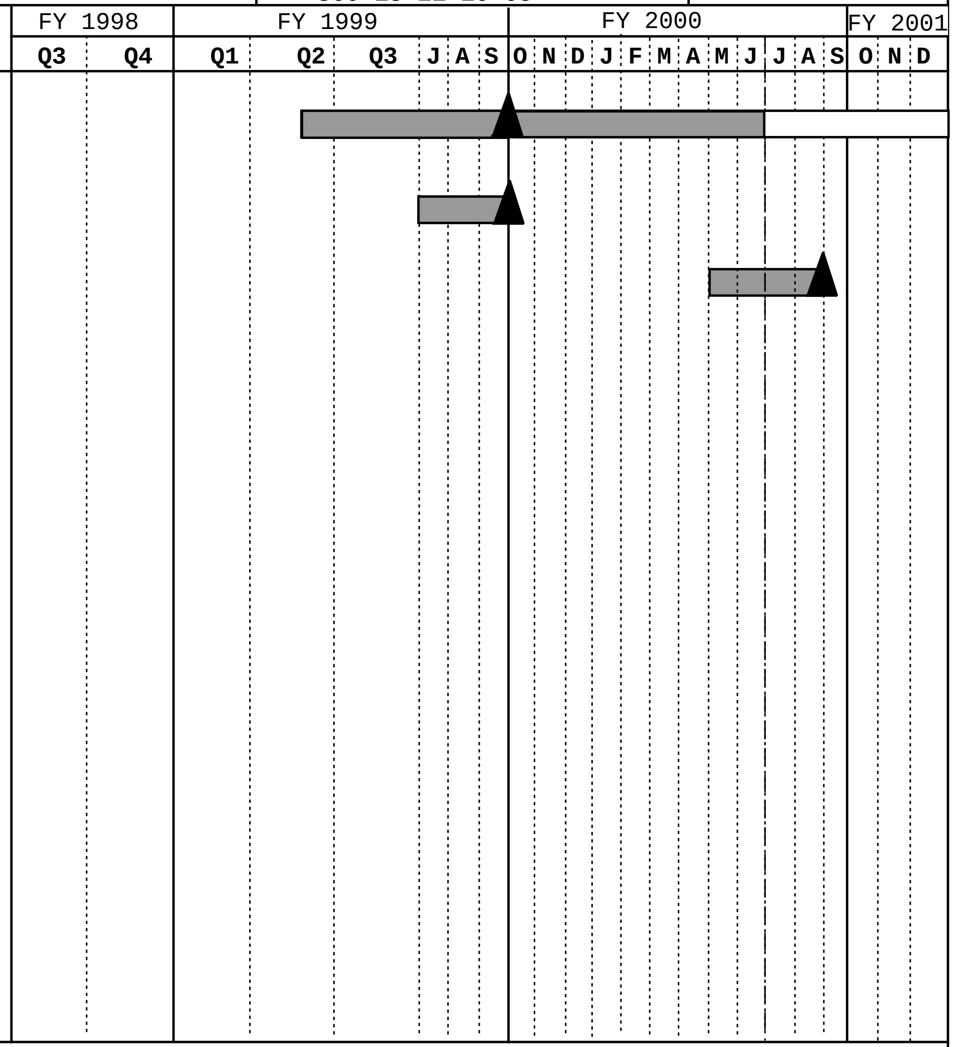
5. CONTRACT PERIOD
FY 1998-2001

6. ACTIVITY NO.
41 W6 95 3W 1

7. NRC B&R NO.
860 15 21 20 05

8. DOE B&R NO.
40 10 01 06

9. MILESTONE IDEN. NO.	10. MILESTONE DESCRIPTION
7.1.A.	Evaluate and Input Surveillance Reports into Embrittlement Database
7.1.B.	Complete Update 10
7.1.C.	Complete Update 11



11. REMARKS