

Improving the Toughness of Electron Beam Curable Cationic Epoxy Resins

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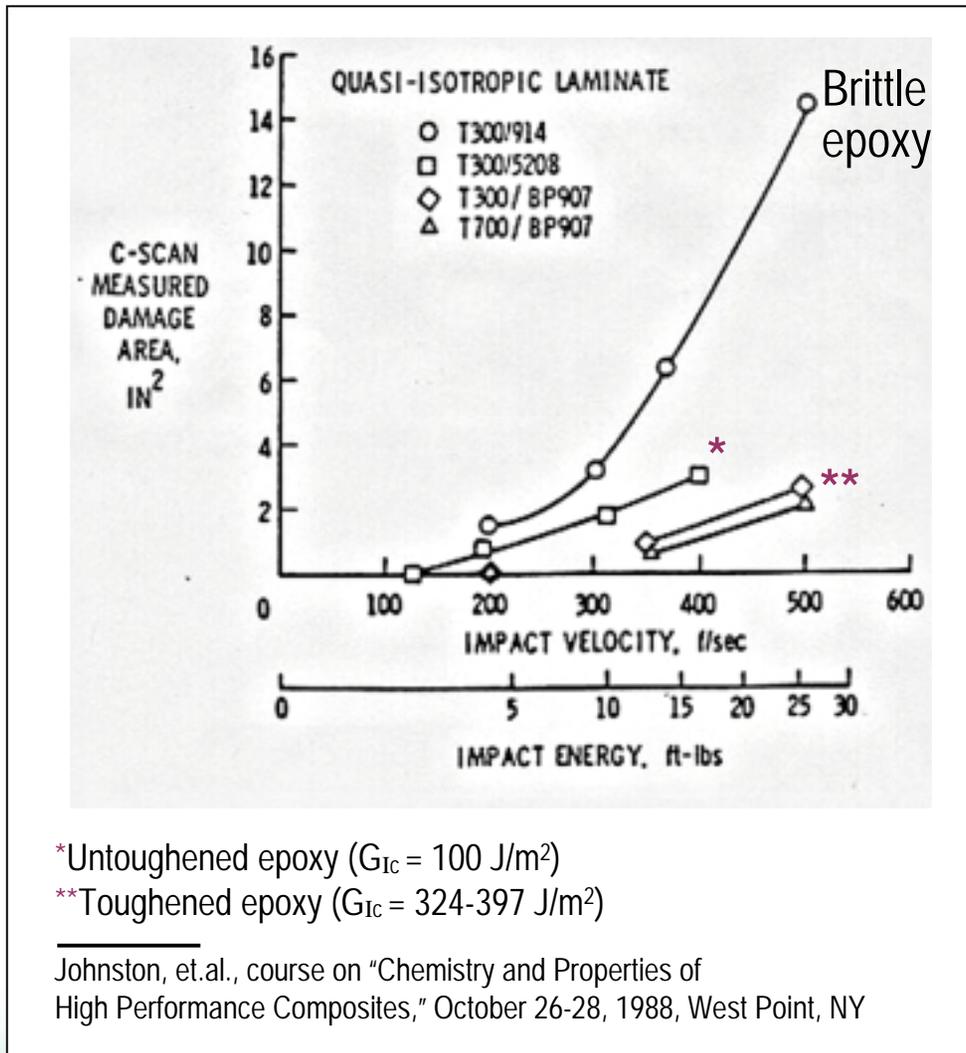
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Outline

- **Why are tough resins important?**
- **What is toughness and how is it measured?**
- **Relationships between fracture toughness and other composite properties**
- **Toughening strategies for conventional, thermally curable epoxies**
- **Previous toughening results on EB curable cationic epoxies from DOE DP CRADA (1994-1997)**
- **Latest toughening results on EB curable cationic epoxies from DOE LTR CRADA (1999-2002)**

Effect of Resin Toughness and Impact Energy on Damage Size



- Why are tough resins important?
 - Tough resins can significantly reduce the probability of catastrophic failure caused by impact damage
 - There is a significant decrease in the damage size for composites having toughened epoxies versus brittle epoxies

Definitions

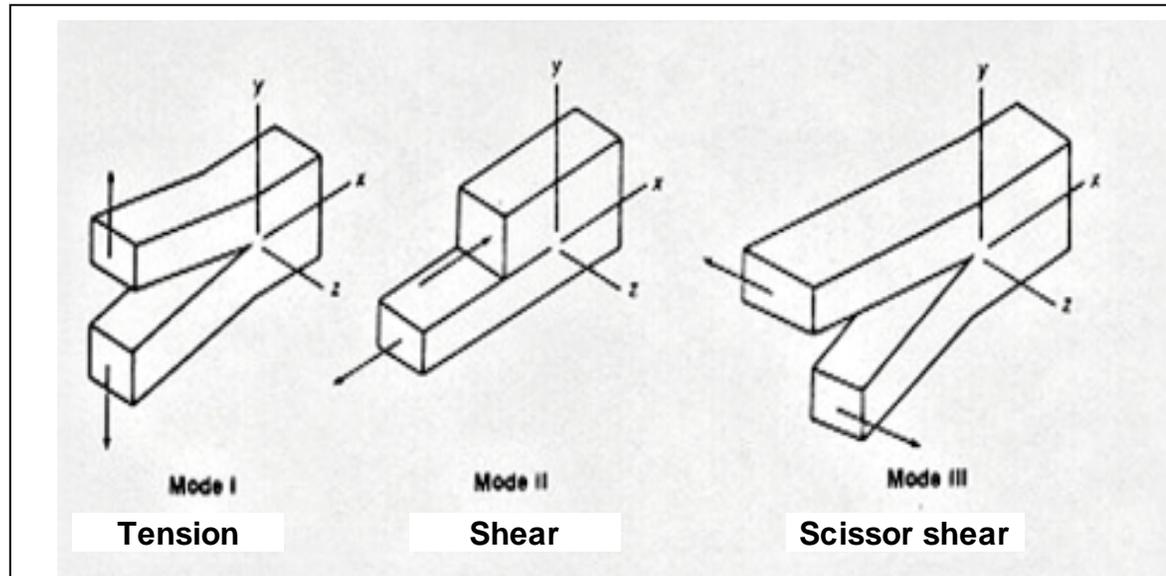
- **Fracture Toughness**

- Measure of the damage tolerance of a material containing initial flaws or cracks
- The resistance of a material to crack propagation
- Fracture toughness, K_{Ic} , and fracture energy, G_{Ic} are measures of material toughness

$$G_{Ic} = \frac{(1 - \nu^2) K_{Ic}^2}{E}$$

Where ν is poisson's ratio and
E is Young's Modulus

Basic Fracture Modes of Loading Involving Different Crack Surface Displacements



Mode I - opening or tensile loading, the crack surfaces move directly apart
- weakest and most sensitive mode
- considered the single best measure for toughness

Mode II - sliding or in-plane shear, the crack surfaces slide over one another in a direction perpendicular to the leading edge of the crack

Mode III - tearing or antiplane shear (scissor shear), the crack surfaces move relative to one another and parallel to the leading edge of the crack

ASM Intl., "Vol. 1 Engineered Materials Handbook Composites," 1987

Battling Trade-Offs

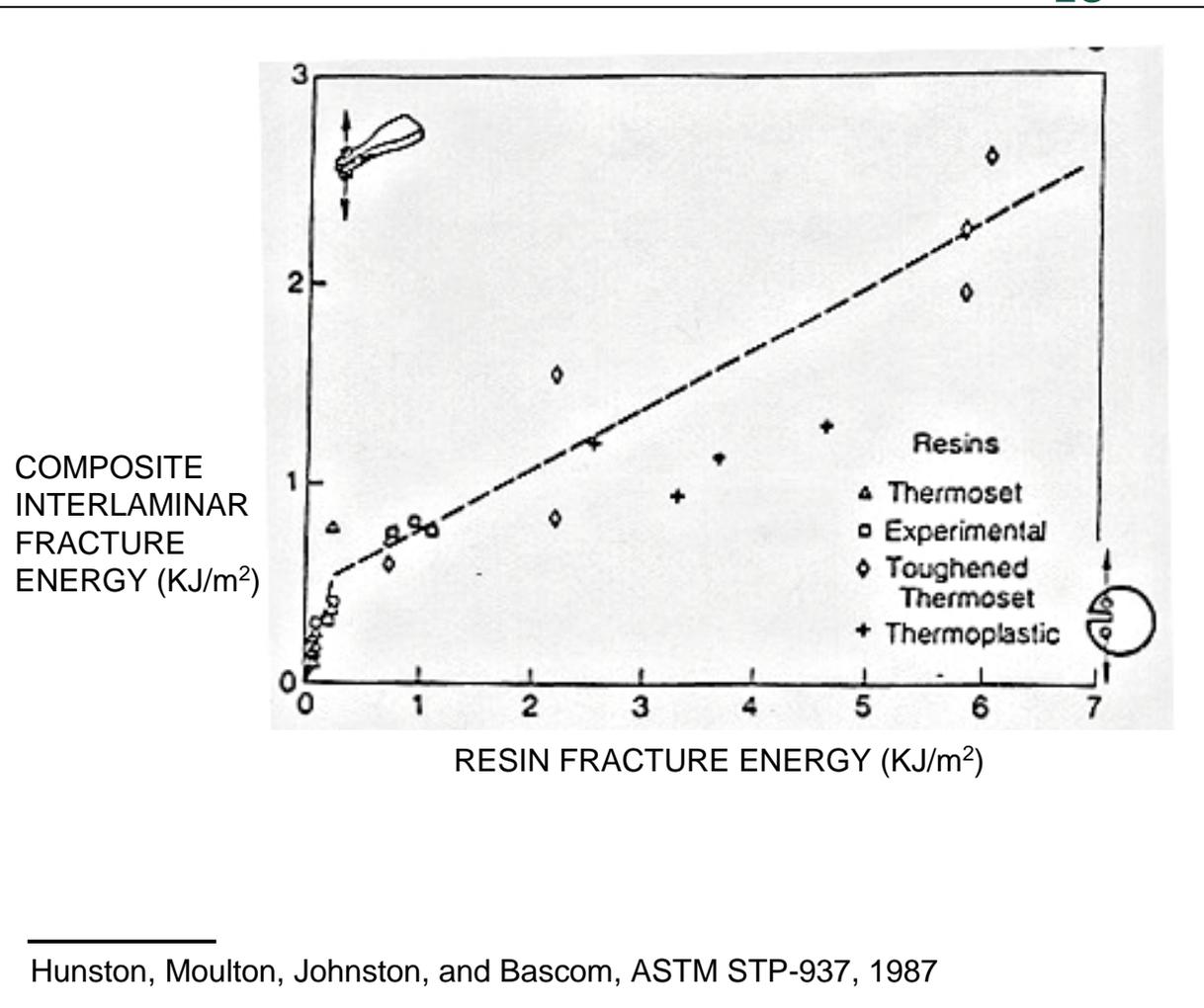
- **CAI properties can be increased by toughening the resin matrix, BUT:**
 - **Improving CAI strength and toughness properties typically results in the reduction of 1 or more of the following:**
 - **T_g**
 - **Modulus**
 - **Hot/wet mechanical properties (esp. compression strength)**
 - **Processability**

What are the relationships between fracture toughness and other composite properties?

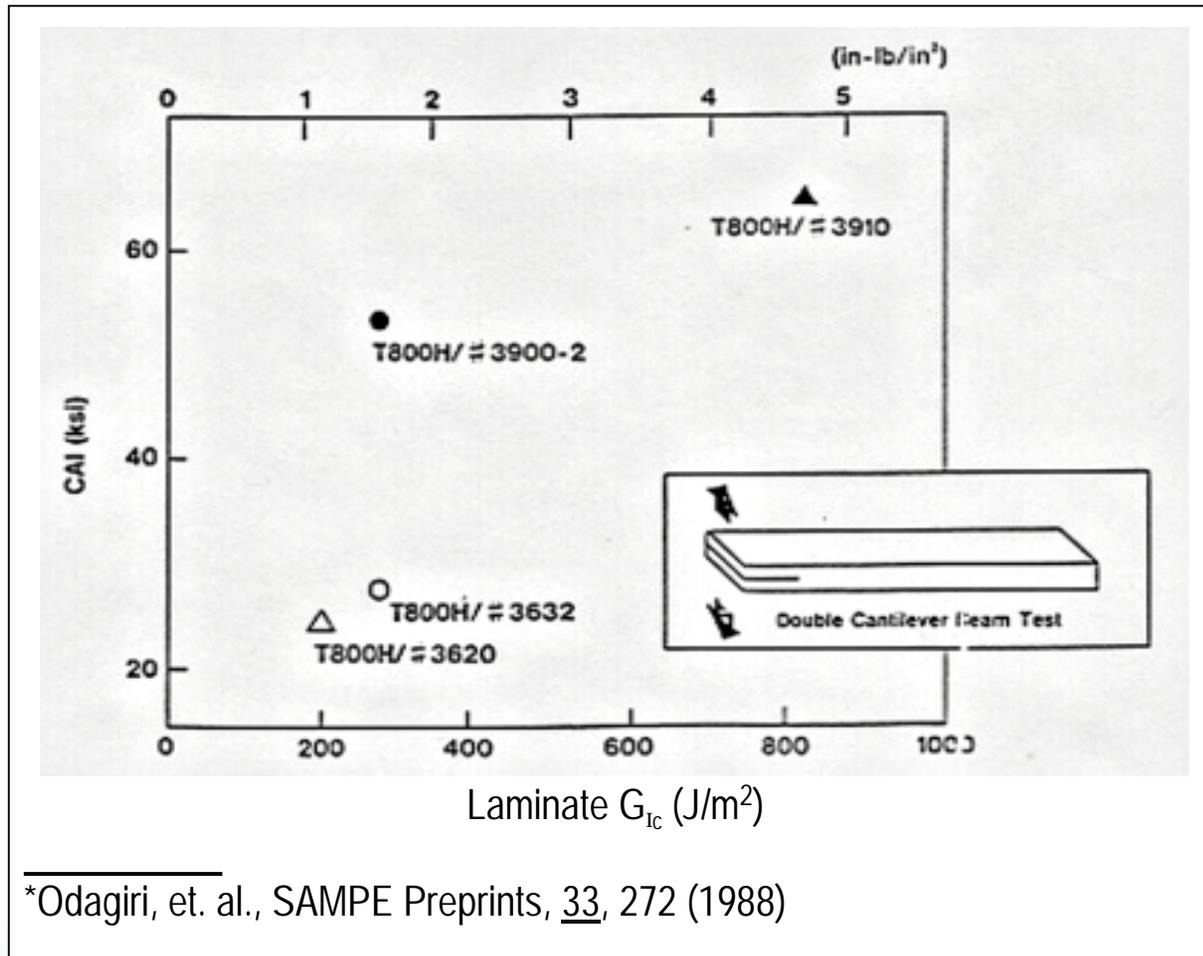
Relationship Between Resin G_{Ic} and Composite Interlaminar G_{Ic}

- Composite G_{Ic} increases with resin G_{Ic}

—The relative effect being more significant for low values of toughness

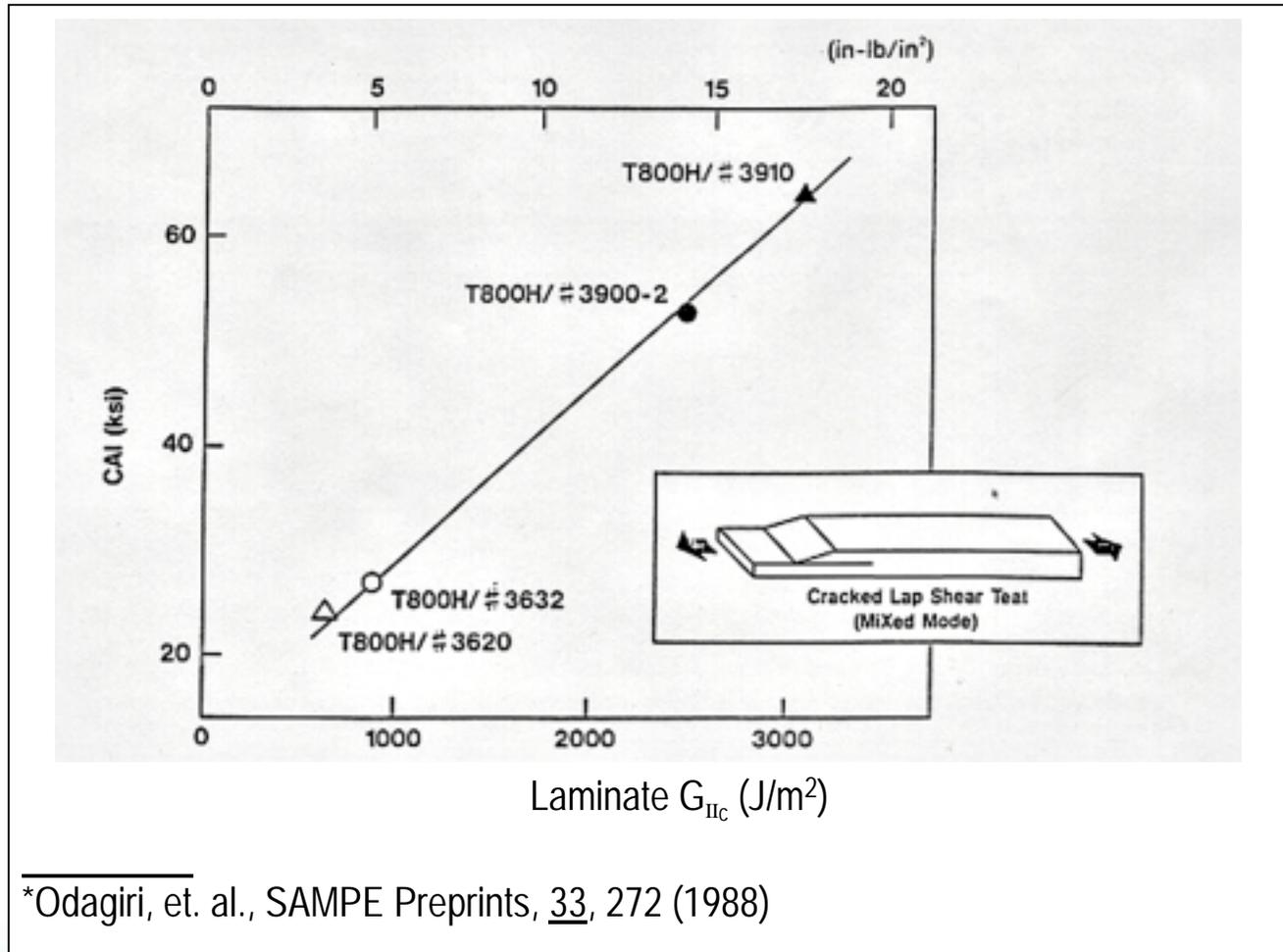


Relation Between CAI and Mode I Fracture Toughness*



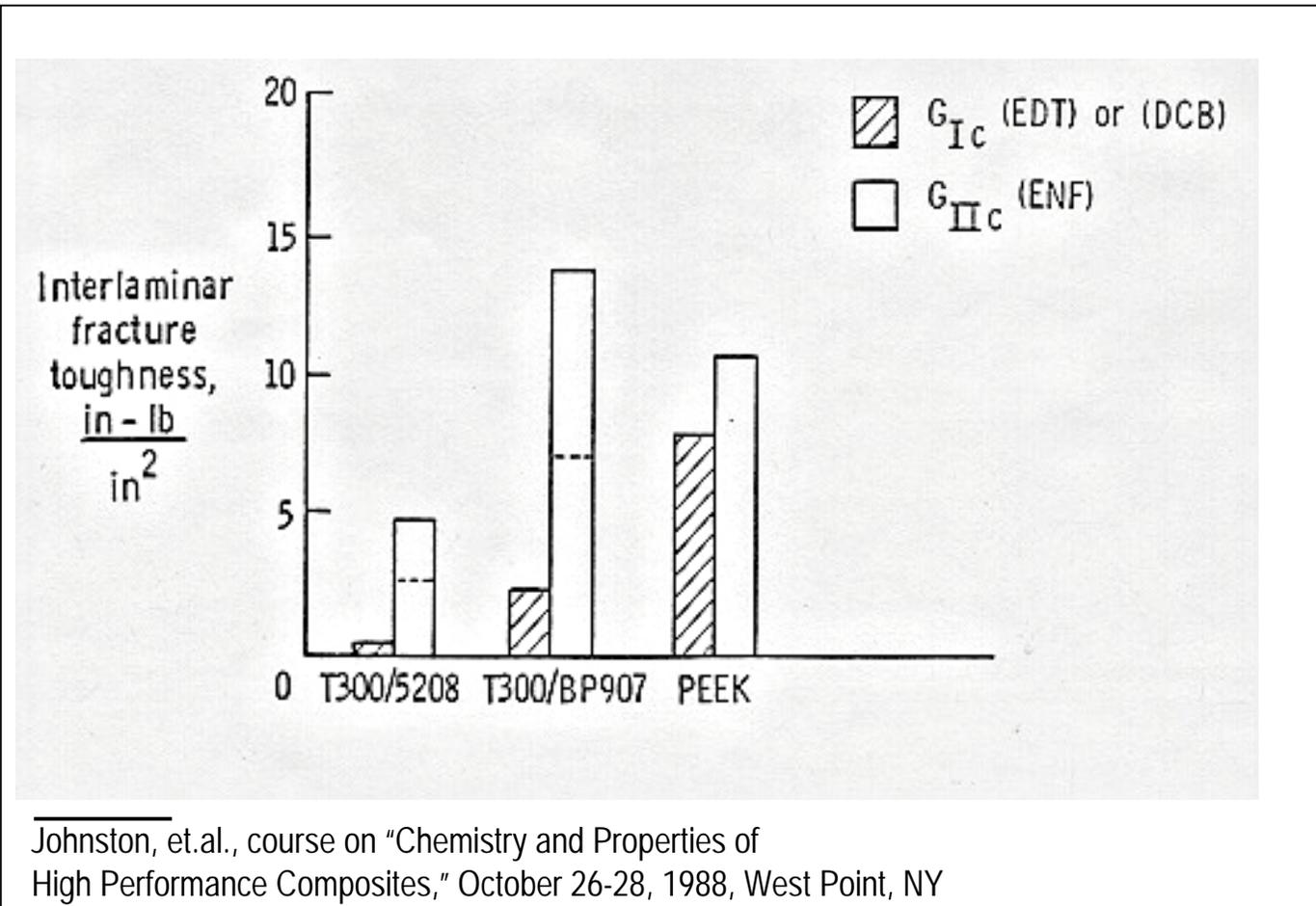
- Laminate G_{Ic} typically tracks CAI

Relation Between CAI and Mode II Fracture Toughness*



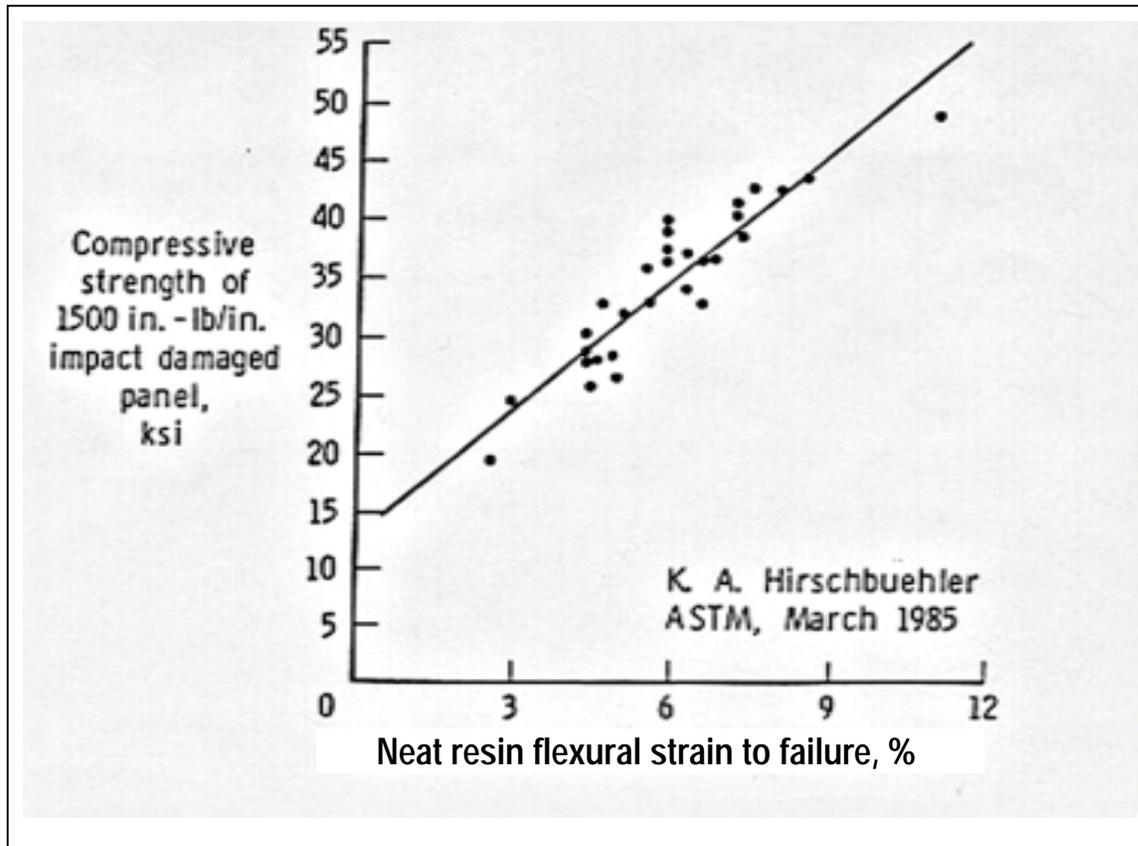
- There is a close connection between laminate G_{IIc} and CAI

Relationship Between Composite Mode I & II as Resin Toughness Increases



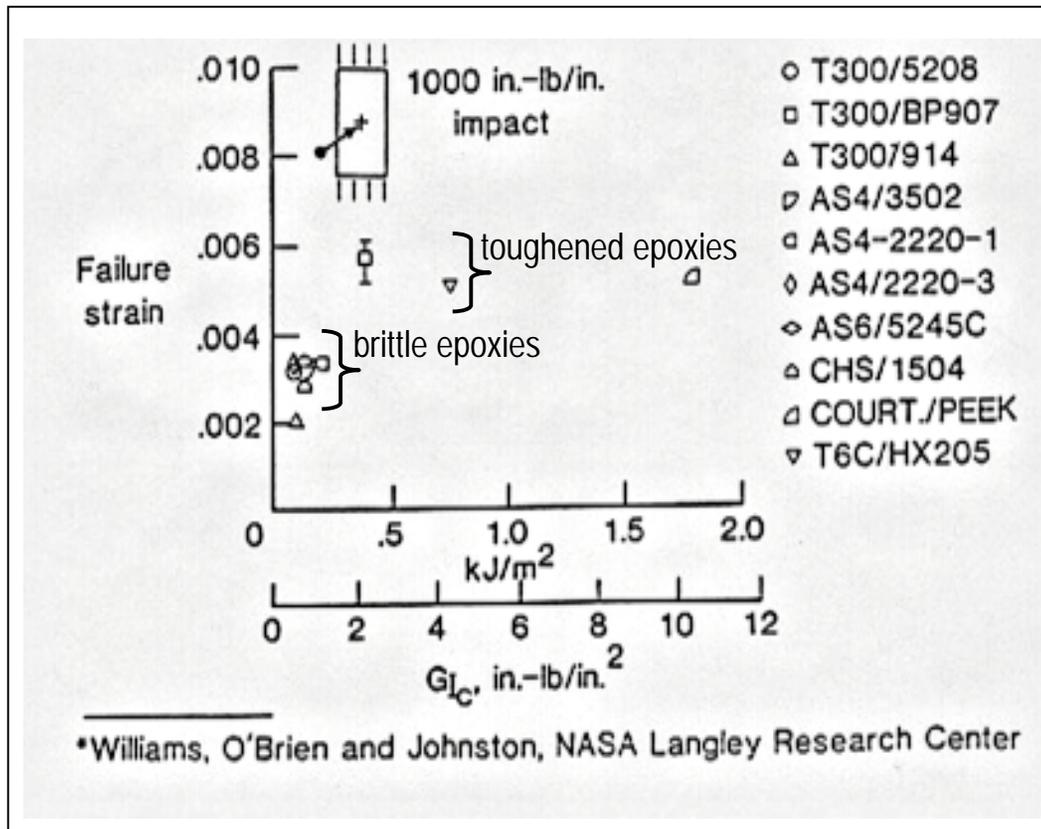
- G_{Ic} and G_{IIc} values merge closer as resin toughness increases

CAI Strength Versus Neat Resin Flexural Strain



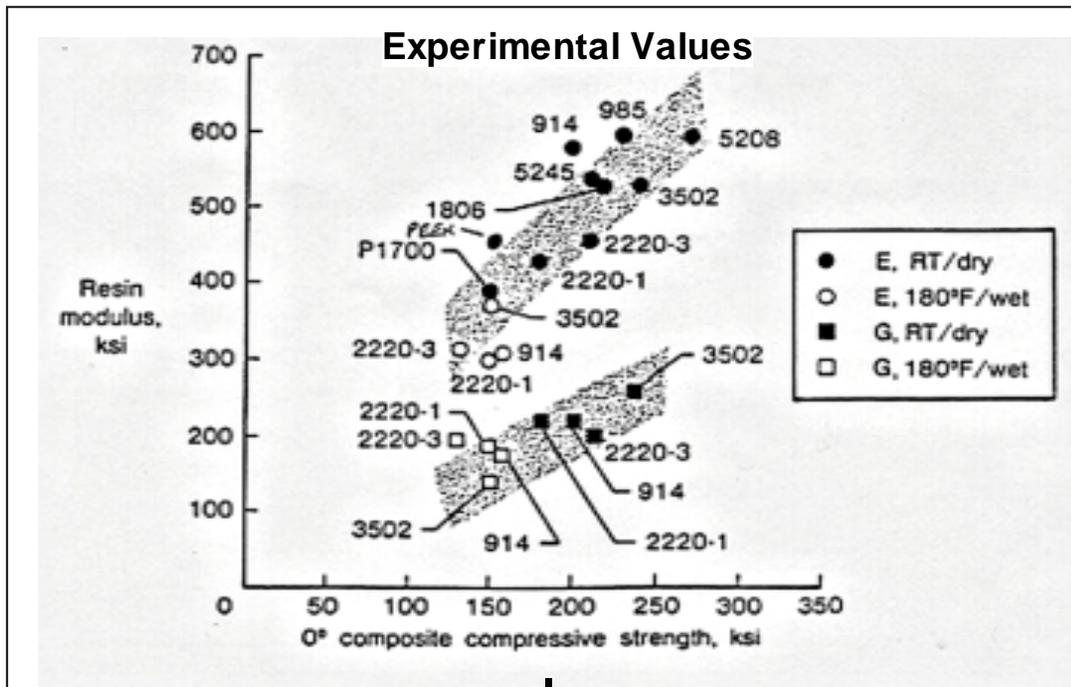
- CAI improves as resin strain to failure increases

CAI Failure Strain Versus Fracture Toughness*



- Tougher resins exhibit higher CAI failure strain and composite G_{Ic}

Resin Modulus Versus 0° Composite Compressive Strength

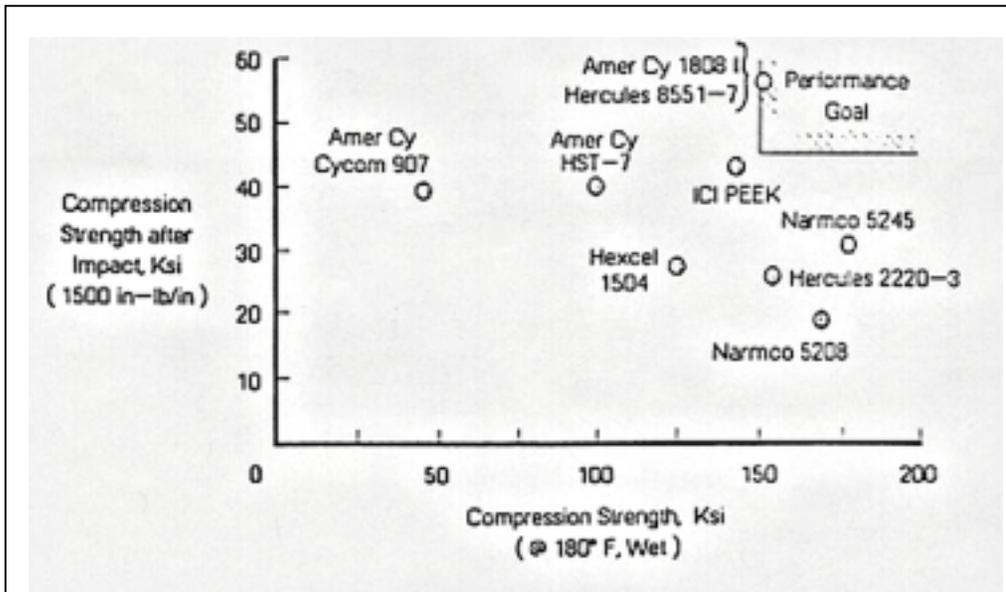


- High resin modulus is required for achieving high composite compression strength

Untoughened epoxies		Toughened epoxies	
	G_{Ic} (J/m ²)		G_{Ic} (J/m ²)
5208	100	2220-1	256
3502	120-150	2222-3	220-250

Johnston, et.al., course on "Chemistry and Properties of High Performance Composites," October 26-28, 1988, West Point, NY

CAI Strength Versus Compression Strength



- Maximizing either CAI or compression strength alone typically results in the reduction of the other
- Goal is to maximize both properties by developing high modulus, highly toughened resins

Untoughened epoxies	G_{Ic} (J/m ²)	Toughened epoxies	G_{Ic} (J/m ²)
5208	100	8551-7	500
1504	95-123		

*Johnston, et. al., course on "Chemistry and Properties of High Performance Composites," October 26-28, 1988, West Point, NY

Fracture Toughness Trends

- Modest interlaminar fracture toughness is required to prevent delamination of the composite
- Composite G_{Ic} increases with resin K_{Ic} and resin G_{Ic}
Relative effect is more important for low values of toughness
- CAI strength is related to:
 - Composite G_{Ic}
 - Composite G_{IIc}
 - Resin strain to failure

Fracture Toughness Trends Continued

- **High resin modulus is required for achieving high composite compression strength**
- **Fatigue lowers interlaminar fracture toughness**
- **Poor fiber/resin interfacial adhesion lowers interlaminar fracture toughness**

Attributes of High Performance Epoxy Resins for Military Aircraft Applications

- **High toughness** \longrightarrow **High CAI**
- **High modulus** \longrightarrow **High compression strength**
- **High T_g** \longrightarrow **High service temperature**

- **Easily processable**

Typical Methods Used for Toughening Thermally Curable Epoxy Resins

- **Addition of a 2nd phase**
 - **Reactive rubbers (CTBN-ATBN types)**
 - Acrylonitrile group inhibits cure of EB curable cationic epoxies
 - **Core shell rubbers**
 - **Thermoplastics**
- **Addition of Thermoplastics (single phase)**
- **Increase length between crosslinks**
- **Interleafing**
- **Combinations of above**

Core-Shell Rubbers

- **Description**

Preformed particles containing an acrylic based outer-shell and a rubber core

Outer shell may contain a reactive functional group to increase compatibility to the epoxy resin

- **Important factors affecting fracture toughness**

Shell chemistry greatly influences resin/CSR interfacial adhesion

- **Fracture toughness mechanisms**

Localized matrix shear-yielding

Particle cavitation

Rubber particle-bridging across and behind the crack tip

Advantages of CSRS Over Reactive XTBN Rubbers

- **CSR particles having specific sizes are relatively easy to make**
- **CSRs enhance toughness with less tradeoff in thermomechanical properties**
- **Offers superior UV-light and thermal-oxidative aging properties**

Disadvantages of CSRs

- **Relatively high initial viscosity**
- **Particle agglomeration**

Chain Extended Polymers (Increased Length Between Cross-links)

- **History (1980s)**

Dow and Shell Chemical developed single phase, lightly crosslinked, toughened epoxy resins:

- Crosslinkable epoxy thermoplastics (CET resins) and
- Lightly crosslinked thermosets (LXT resins)

- **Description**

CETs and LXTs are tough, thermoplastic-like molecular structures made in-situ using “stiff backbone” components and “flexible backbone” components

Chain Extended Polymers (Increased Length Between Cross-links)

- Advantages of CETs and LXTs

- High T_g s

- High modulus

- Excellent inherent toughness

- Disadvantages

- High temperatures (150-200°C) are required for proper chain extension reactions to occur

- EB curing favors reactions which result in poor chain extension

- Prepolymers are too viscous for EB processing

One of the Preferred Methods for Toughening High Performance, Thermal Cure Epoxies

- **Modification of epoxy resins with engineering thermoplastics (TP)**
 - **Note: Rubber-toughened epoxies (ie., XTBNs) are not used in high-performance structural composites**
 - **XTBNs improve CAI strength and strain but fail to meet hot/wet compression strength requirements due to the rubber's low T_g and low modulus**

Several Cured Morphologies Are Possible for Epoxy/TP Blends, but Not All Morphologies Are Effective

- **Non-preferred morphologies**
 - Homogeneous, single phase
 - TP or epoxy particulate, second phase
- **Preferred morphology**
 - Co-continuous, two-phase Spinodal

Co-continuous (Two-Phase Spinodal) Morphology Yields Optimum Fracture Toughness

- **Consists of epoxy continuous and TP continuous phases**
- **Submicron phase sizes**
- **Requires TP loadings exceeding 15-20%**
 - TP loadings of 30-40% are the norm for high-performance, epoxy formulations
- **Morphology, phase sizes, and ultimate toughness is controlled by TP backbone, reactive end group, molec. wt. and epoxy type**
- **Nature of the toughening mechanism is not apparent other than a roughened fracture surface**
- **Kinetics and thermodynamics of the phase separation process during cure is extremely complex**

Relevance of Co-continuous Morphology to EB Curing

Co-continuous, spinodal morphology is not considered a viable method for toughening EB curable resins because:

- **High TP loadings make resin viscosities too high for processing and consolidation**
- **Spinodal formation during cure may not be possible with EB due to incompatible phase separation kinetics**

Toughening Composites by Interleafing

- **Interleafing incorporates high strain, resin rich zones between prepreg plies and a separate resin which surrounds the fiber**
- **The interleaf concept consist of an inhomogeneous resin matrix**
 - Resin A between plies is significantly different from Resin B surrounding the fiber bundles
- **Interleafing can produce extremely high, damage tolerant composites, but**
 - Resin B must have high toughness
 - Resin A must have a rheological profile that is conducive to EB processing

Previous Toughening Results on EB Curable Cationic Epoxies From DOE DP CRADA (1994-1997)

Many Toughened and Untoughened EB Curable Cationic Epoxy Resin Systems Were Developed During DOE DP CRADA (1994-1997)

Epoxies

- Bisphenol A liquid epoxy resins
- Bisphenol F epoxy liquids
- Epoxy novolac resins
- Multifunctional epoxy resins
- Cycloaliphatic epoxy liquids
- Hydrocarbon epoxies
- Toughened epoxies
- Flexible epoxies
- Fusion solid epoxies
- Multi-epoxy resins (blends)
- Diluted liquid epoxy resins
- Multifunctional epoxy diluents

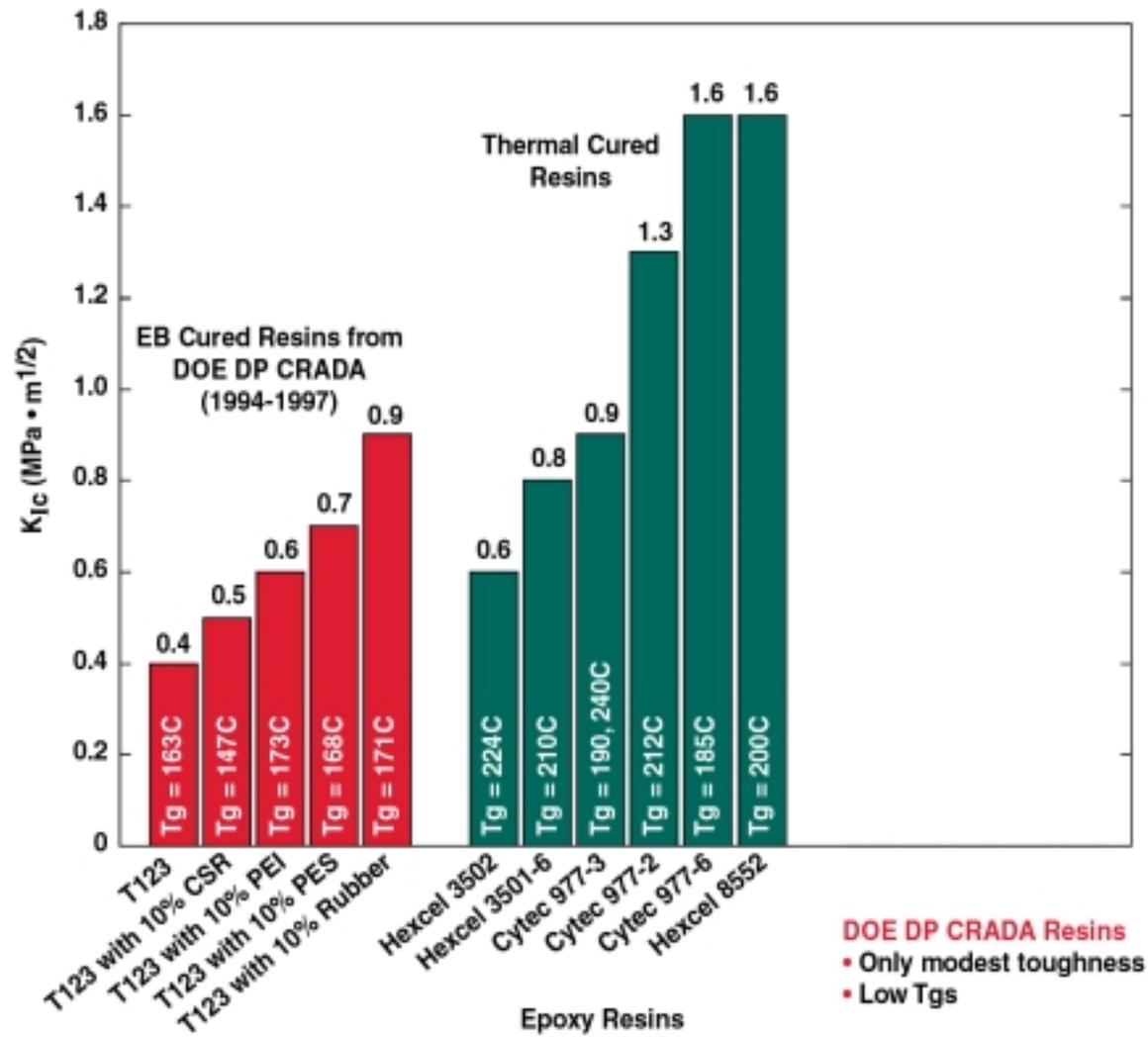
Cationic initiators (w/ various anions)

- Diaryliodonium salts
- Triarylsulfonium salts
- Iron complexes
- Diaryldisulfones
- Triazine compounds

Tougheners

- Engineering thermoplastics
- Hydroxy-containing thermoplastics
- Reactive flexibilizers
- Elastomers
- Rubbers
- Undissolved thermoset particles
- Undissolved thermoplastic particles
- Polyarylates

K_{IC} Fracture Toughness Properties on EB Cured and Thermal Cured Epoxy Resins



Latest Toughening Results on EB Curable Cationic Epoxyes From DOE LTR CRADA (1999-2002)

K_{Ic} Fracture Toughness Properties on EB Cured and Thermal Cured Epoxy Resins

