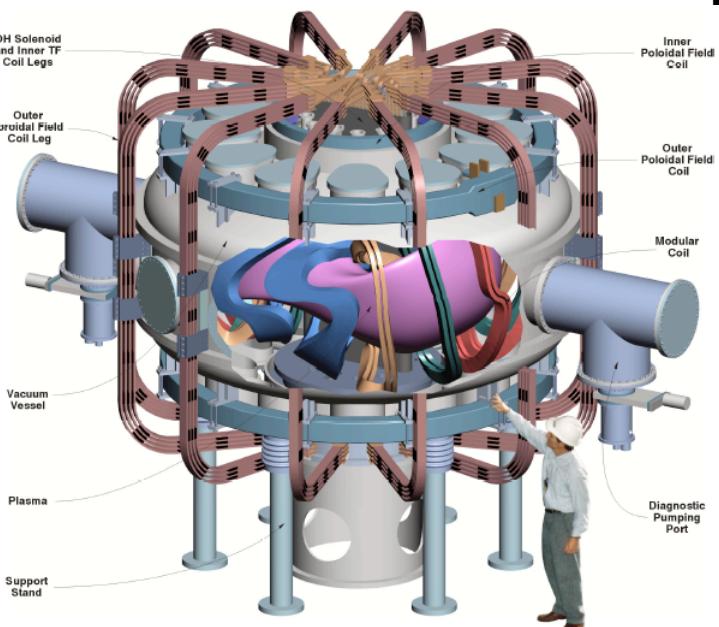


# QPS TRANSPORT AND ENERGETIC PARTICLE PHYSICS

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- QPS is a very low aspect ratio ( $A = 2.7$ ) Quasi-poloidal stellarator that will test:

- Equilibrium robustness at low  $A$
- Neoclassical and anomalous transport
- Stability limits up to  $\langle B \rangle = 2.5\%$
- Bootstrap current effects
- Reduced poloidal viscosity effects on shear flow transport reduction
- and Configurational flexibility

- Design parameters:  $\langle R_0 \rangle = 0.9$  m,  $\langle a \rangle = 0.33$  m,  $\langle B \rangle = 1$  T  $\pm 0.2$  T for 1sec,  $I_p \approx 150$  kA,  $P_{ECH} = 0.6-1.2$  Mw,  $P_{ICH} = 1-3$  Mw

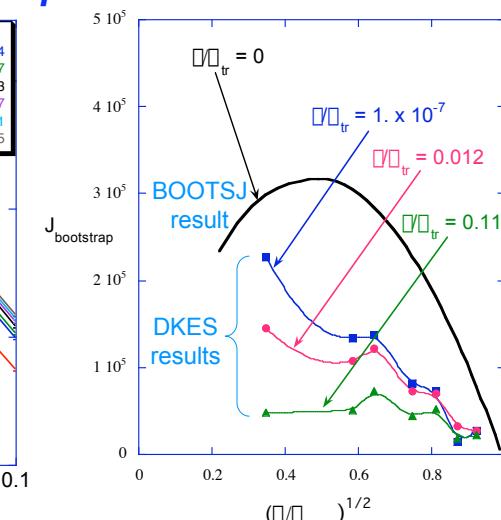
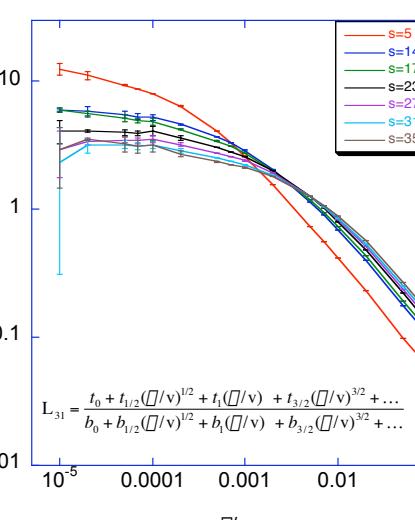
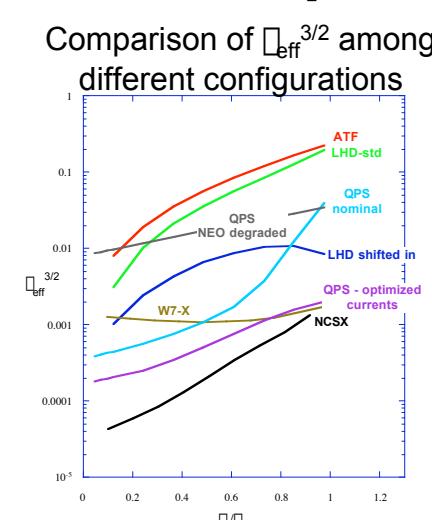
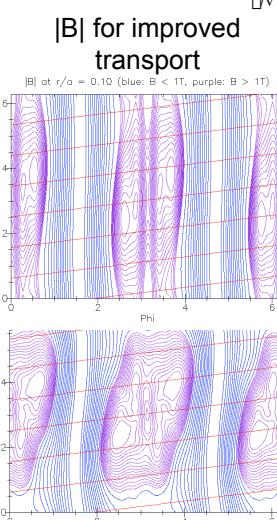
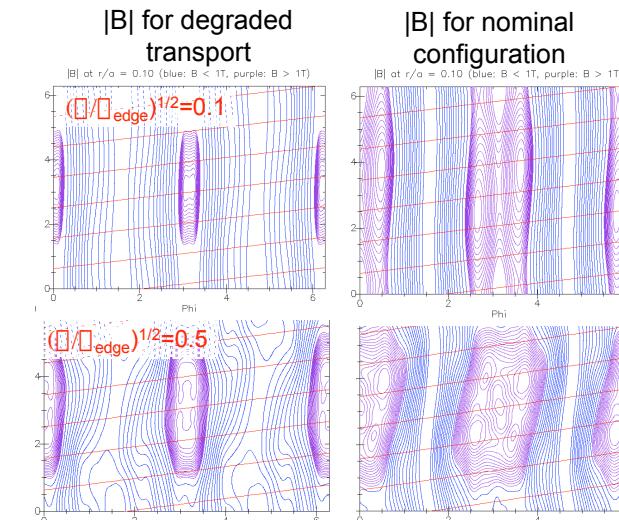
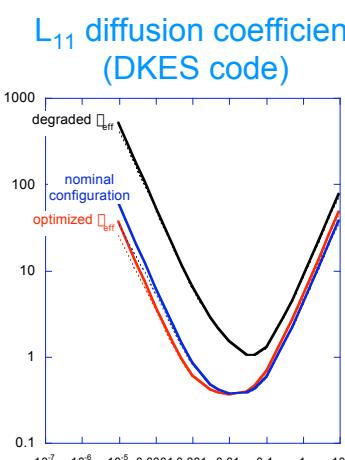
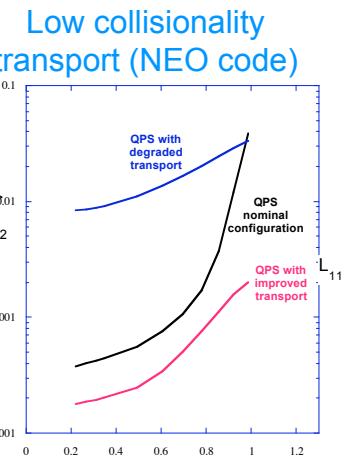
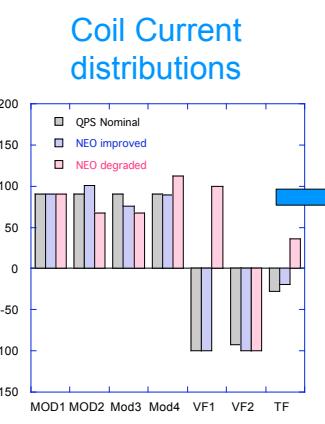
## Optimization Strategy

- QPS optimization targets:

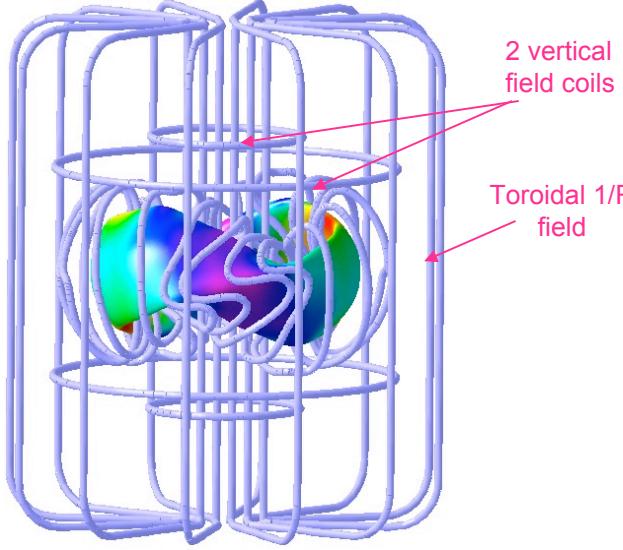
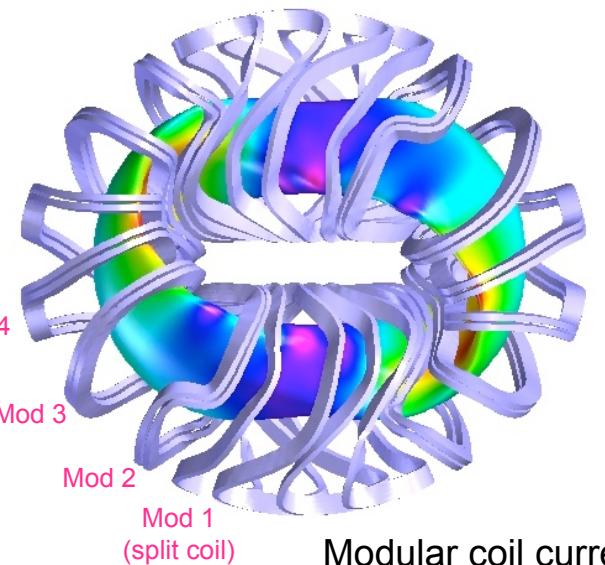
- $\Delta_{eff}$
- Poloidal symmetry
- DKES
- $J, B_{min}, B_{max}$
- Ballooning stability (COBRA)
- Bootstrap consistency
- Iota profile
- Mercier, well
- Minimize  $B_{normal}$  on outer surface
- Coil engineering
  - Coil-coil, coil-plasma separation,
  - Minimum radius of curvature

## Evaluation Tools

- TRANSPORT
- NEO  $\Delta_{eff}$ , Poloidal symmetry
- DKES
  - Setup, mode selection
  - Parallel runs
  - Energy integration
- DELTA5D Monte Carlo
  - Global full-f model
  - ICRF heating
  - NBI heating efficiency
  - Alpha losses
  - $\Delta_f$  bootstrap current
- 1-1/2 D fluid transport model



## Transport flexibility studies (7 independently variable coil currents)



Modular coil currents can vary  $\pm 25\%$   
 Vertical field currents can vary  $\pm 100$  kA  
 Toroidal field currents can vary  $\pm 70$  kA

## Diffusive transport studies using the DKES model

$$\begin{aligned} \bar{I}_i &= \frac{1}{T} \bar{Q} \cdot \bar{\mathbf{s}} \\ &= \frac{n}{\sqrt{I}} \sum_{j=1}^3 L_{ij} A_j \\ &= \frac{n}{\sqrt{I}} \left( \bar{u} \cdot \bar{u}_s \right) \cdot \bar{B} \end{aligned}$$

$$A_j = \frac{T}{T} \frac{e}{\bar{E}} \cdot \frac{\bar{B}}{\langle B^2 \rangle}$$

$$L_{ij} = n \frac{2}{\sqrt{I}} \int dK \sqrt{K} e^{iK} g_i g_j D_{ij}$$

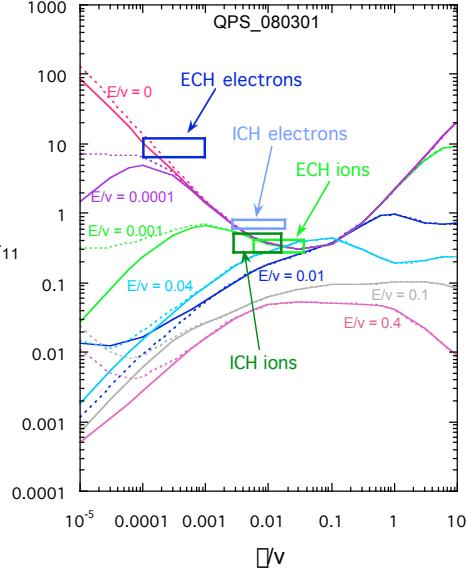
$$\text{where } g_1 = g_3 = 1, g_2 = K, K = \frac{v}{v_{th}}$$

$$D_{11} = D_{12} = D_{21} = D_{22} = \frac{v_{th}}{2} \frac{\partial B_{th}}{\partial r} \frac{d}{dr} \frac{\partial B}{\partial r} \frac{1}{K} \sqrt{K} D_{11}$$

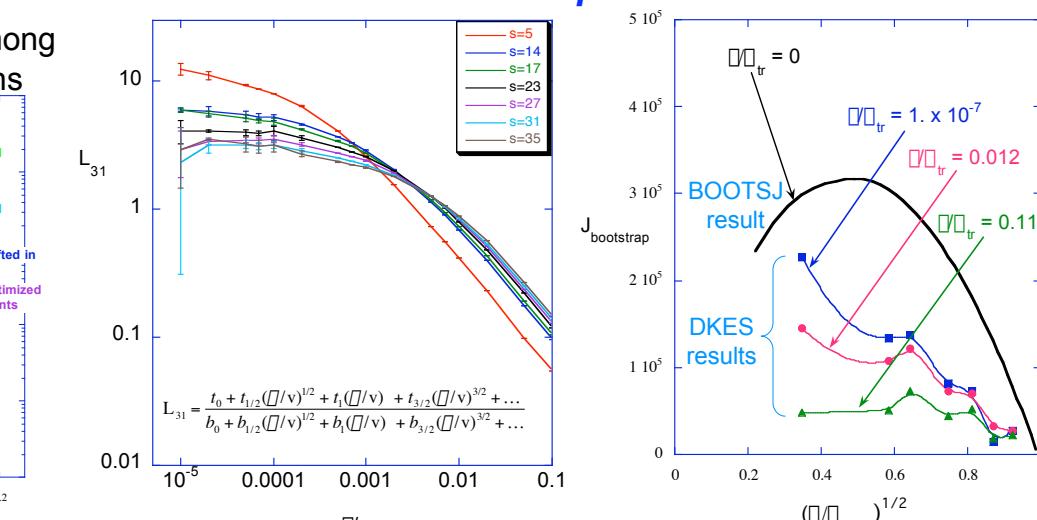
$$D_{31} = D_{32} = D_{13} = D_{23} = \frac{v_{th}}{2} \frac{\partial B_{th}}{\partial r} \frac{d}{dr} \frac{\partial B}{\partial r} K D_{11}$$

$$D_{33} = \frac{v_{th}}{2} \sqrt{K} D_{33}$$

$$D_{ij} = \frac{D_{ij}}{L} \frac{E}{v}, \frac{E}{v} = \frac{v}{v_{th}}$$



## Comparison of collisional/collisionless bootstrap current:

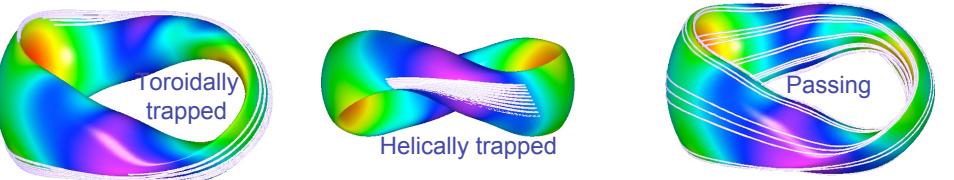
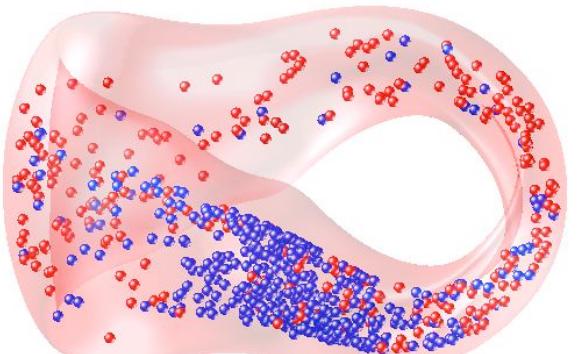


# Monte Carlo transport studies using the DELTA5D model

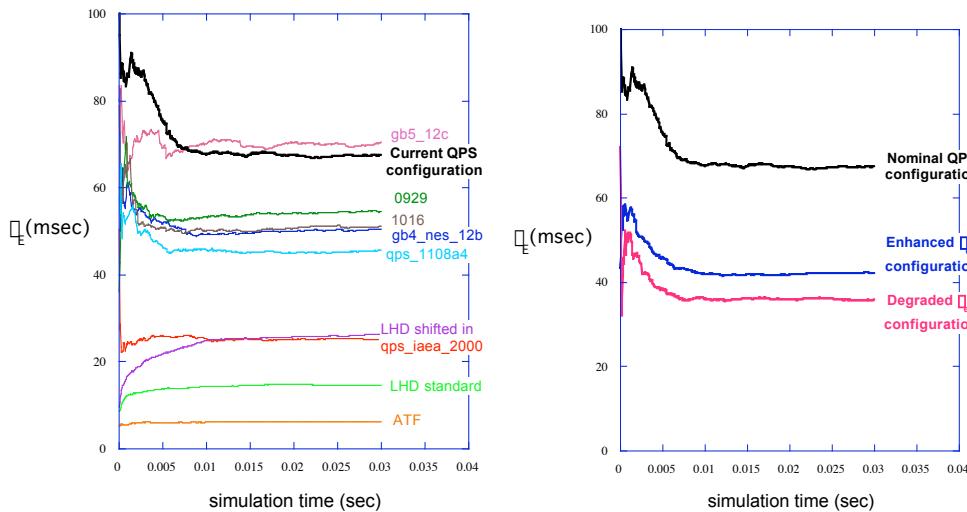
# Alfvén Gap structure using STELLGAP code

## Bootstrap Current Calculation

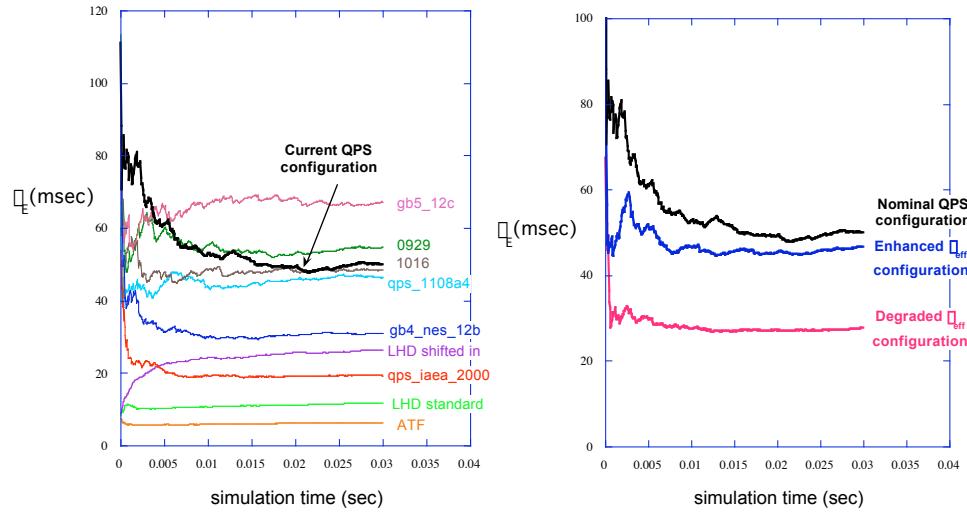
[uses method of A. Boozer and M. Sasinowski, Phys. Plasmas 2 (1995) 610]



Global ion confinement times for ICH parameters between devices (all at same  $R_0$ ) and for QPS coil current variations



Global ion confinement times for ECH parameters between devices (all at same  $R_0$ ) and for QPS coil current variations



$$f = f_M + \mathcal{J}$$

$$f_M = \frac{n}{(2\pi k T)^{3/2}} e^{\frac{mv^2}{kT}}$$

$$\frac{d(\mathcal{J})}{dt} \square C(\mathcal{J}) = \square \frac{\partial \square}{\partial t} \frac{\partial f_M}{\partial \square}$$

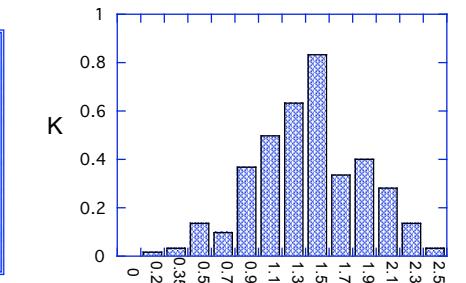
$$\mathcal{J} = \square (\square \square) \frac{\partial f_M}{\partial \square} \quad (\text{evaluated at particle locations})$$

$$J_{\text{bootstrap}} = q \int d^3x \int d^3v \sqrt{g} \mathcal{J}$$

$$= \frac{2q}{\int d^3x g^{1/2}} \int d^2v \int d^3x v_i g^{1/2} \mathcal{J}$$

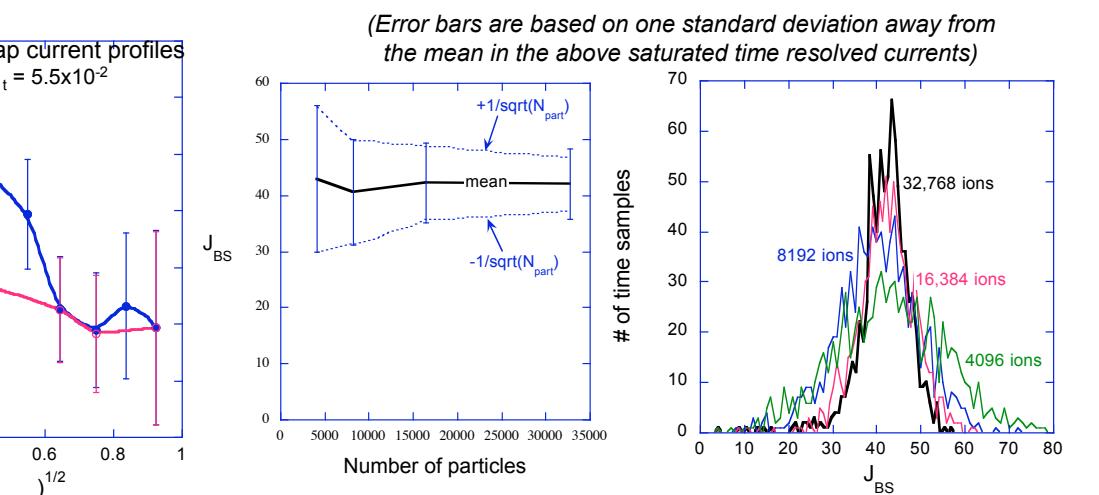
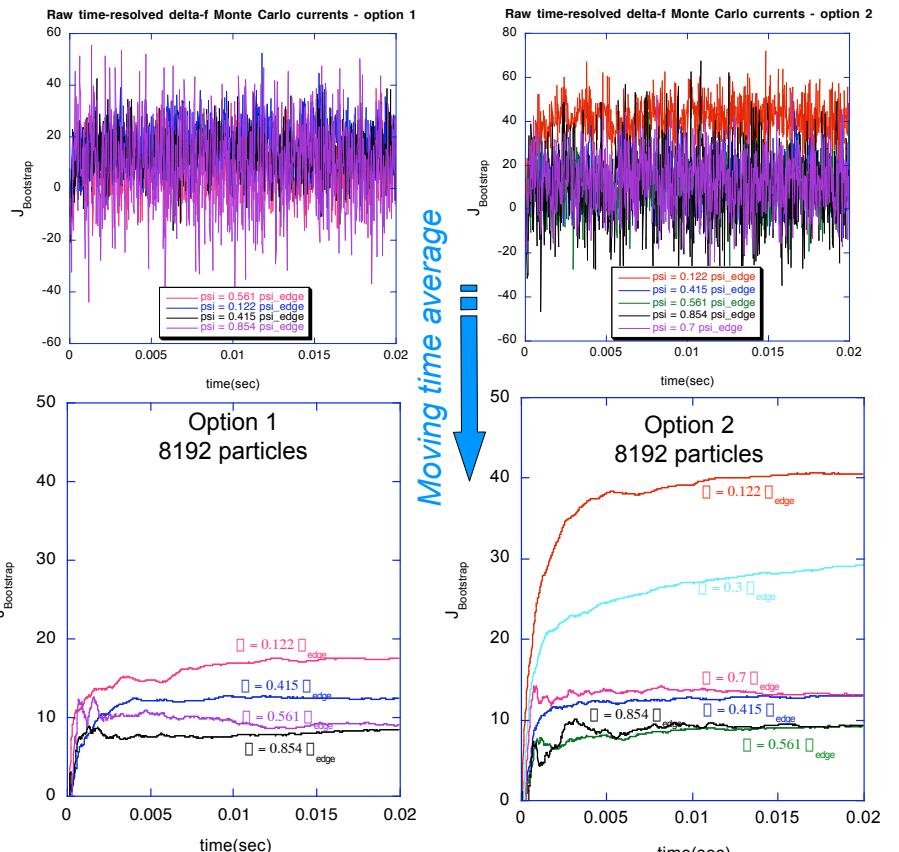
$$\text{with } \sqrt{g} = \text{Jacobian} = \square (G + iI)/B^2$$

$$J_{\text{bootstrap}} = 4 \int d^2v \int K(\square, v, t) \frac{\partial f_M}{\partial \square} \quad \text{where } K(\square, v, t) = \frac{\prod_{i=1}^N v_{i,i}(\square, \square) g_i^{1/2}}{2 \prod_{i=1}^N g_i^{1/2}}$$



Two options have been considered:

1. Radial drifts are included in  $d(\mathcal{J})/dt$ , but orbits are kept bounded to within an annular flux shell
2. Radial drifts are not included in  $d(\mathcal{J})/dt$ , and orbits remain confined to a single flux surface; radial drifts are confined to the same annular flux shell as for option 1



## Stellarator Alfvén Couplings

Alfvén coupling condition:  $k_{l,m,n} = \square k_{l,(m+\square),(n+\square N_{fp})}$

$\square, \square = \text{integers}$

$$n \square mi = \square (n + \square N_{fp} \square mi \square \square i)$$

$$i = \frac{2n + \square N_{fp}}{2m + \square} \quad \square = \frac{v_A}{R} \frac{n \square m N_{fp}}{2m + \square}$$

- GAE (global Alfvén mode):  $\square = 0, \square = 0$
- TAE (toroidal Alfvén mode):  $\square = 0, \square = \pm 1$
- EAE (elliptical Alfvén mode):  $\square = 0, \square = \pm 2$
- NAE (noncircular Alfvén mode):  $\square = 0, \square > 2$
- MAE (mirror Alfvén mode):  $\square = 1, \square = 0$
- HAE (helical Alfvén mode):  $\square = 1, \square \neq 0$

