

# **Advances in the Development of Silicon Nitride and Other Materials**

**Environmental Barrier Coatings Workshop**

**November 6, 2002 - Nashville, TN**

**Mark van Roode**

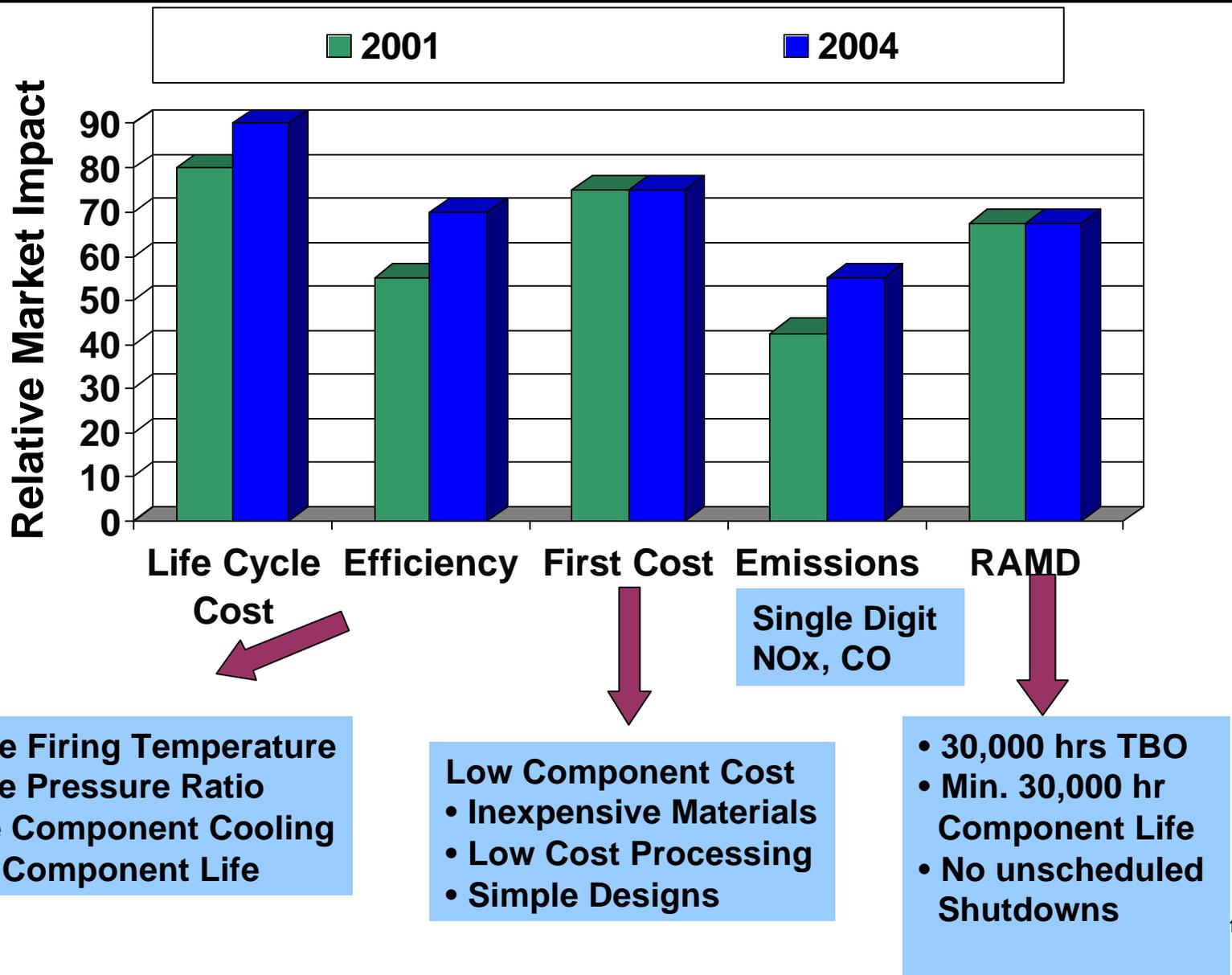
- **Ceramics for Gas Turbines**
- **Evolution of Monolithics**
- **Critical Technical Issues**
- **Commercialization Issues**
- **Summary**

**Solar Turbines**

*A Caterpillar Company*

# ***Ceramics For Gas Turbines***

# Gas Turbine End User Buying Criteria



- **Superior Ductility and Thermal Conductivity**
- **Operating Temperature Limitation: 900°C for Uncooled Components**
- **Turbine Inlet Temperatures (TITs) are increasing**
- **Emissions of NO<sub>x</sub>, CO Need to be Reduced**
- **Management of Air is Required**
  - **Sophisticated Cooling Schemes and Coatings for Higher TITs**
  - **Spatial Limitations to Cooling for Smaller Engines**
  - **Inconvenience of Steam Cooling for Larger Engines**

**Good Mechanical Properties up to 1300 - 1400°C**

**Reduced Cooling Air Requirements**

**Increase Turbine Inlet Temperatures → Increased Efficiency and Output Power**

**More Air Available for NOx and CO Emissions Reduction**

**Light Weight – Important for Transportation Applications**

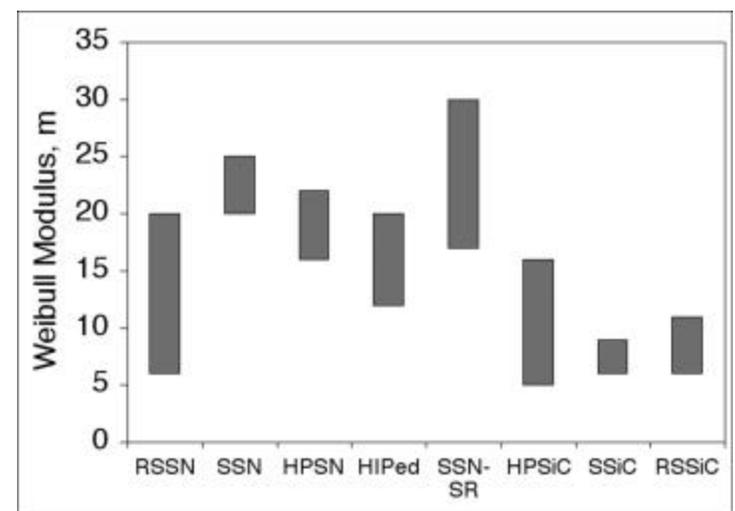
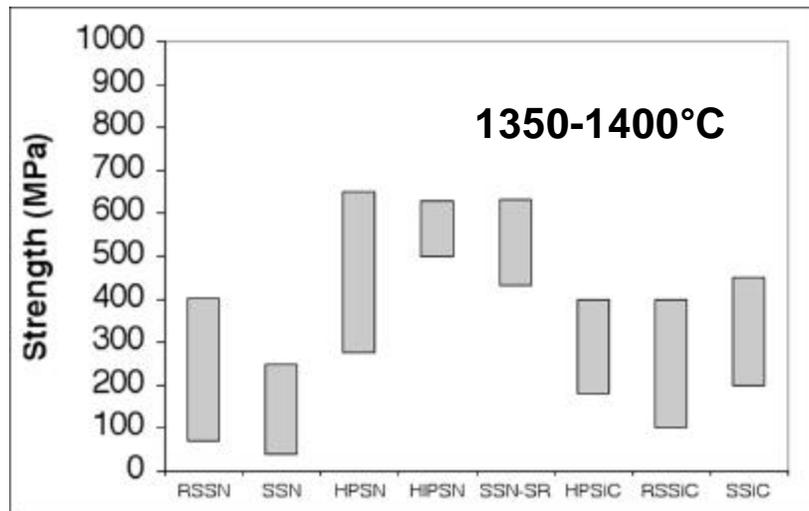
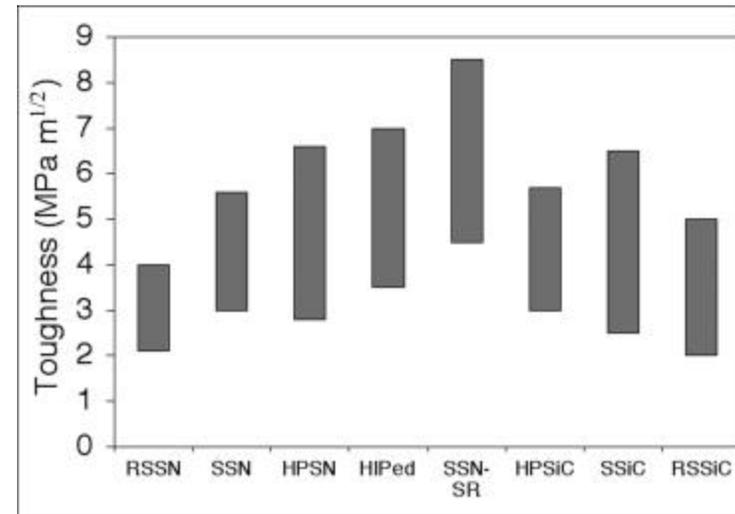
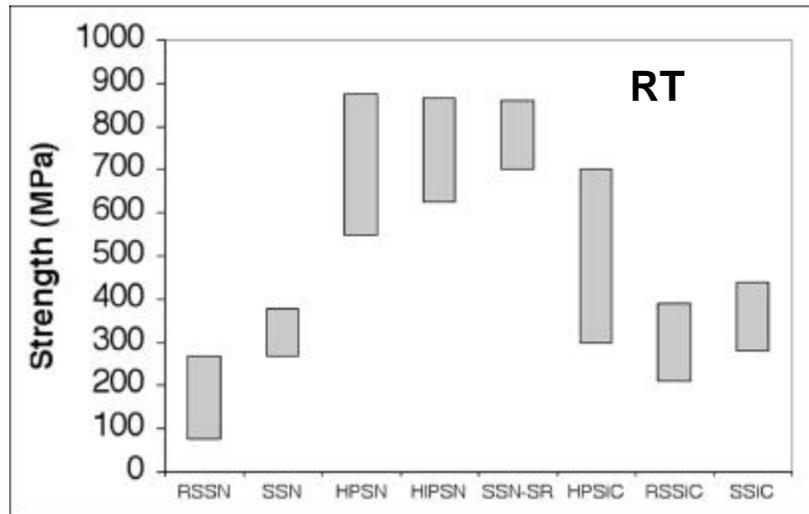
- **Anson et al. , ASME 92-GT-393 (US data)**
  - **Potential annual fuel savings from more efficient small gas turbines incorporating ceramics:**
    - **US: 0.2 Quads by 2010 - \$ 600M @ \$ 3/MBtu Nat.Gas**
- **Grondahl and Tsuchiya, ASME 98-GT-186**
  - **MS9001FA Gas Turbine**
    - **Ceramic transition piece, two stages of buckets, nozzles, shrouds**
    - **2-3 Percentage points in combined cycle efficiency improvement compared to current metal engine**
- **Solar Turbines: Potential component cost savings**
  - **Silicon nitride blade: 30% of cost of cooled single crystal blade**
  - **Silicon nitride nozzle: 65% of cost of cooled superalloy nozzle**

<b>Monolithics</b>	<b>Ceramic Matrix Composites</b>
<b>Si<sub>3</sub>N<sub>4</sub>, SiC, Sialons</b>	<b>SiC/SiC, Oxide/Oxide</b>
<b>Superior HT Strength</b>	<b>Lower HT Strength</b>
<b>Lower K<sub>1C</sub> &lt; ~ 9 MPa.m<sup>1/2</sup></b>	<b>Higher K<sub>1C</sub> &lt; ~ 25 MPa.m<sup>1/2</sup></b>
<b>Design Stress up to 200-300 MPa</b>	<b>Design Stress &lt; 70-100 MPa</b>
<b>Limited to Small Components</b>	<b>Can Be Used for Larger Components</b>
<b>Lower Cost</b>	<b>Higher Cost</b>
<b>For Smaller Engines</b>	<b>For Larger Engines</b>

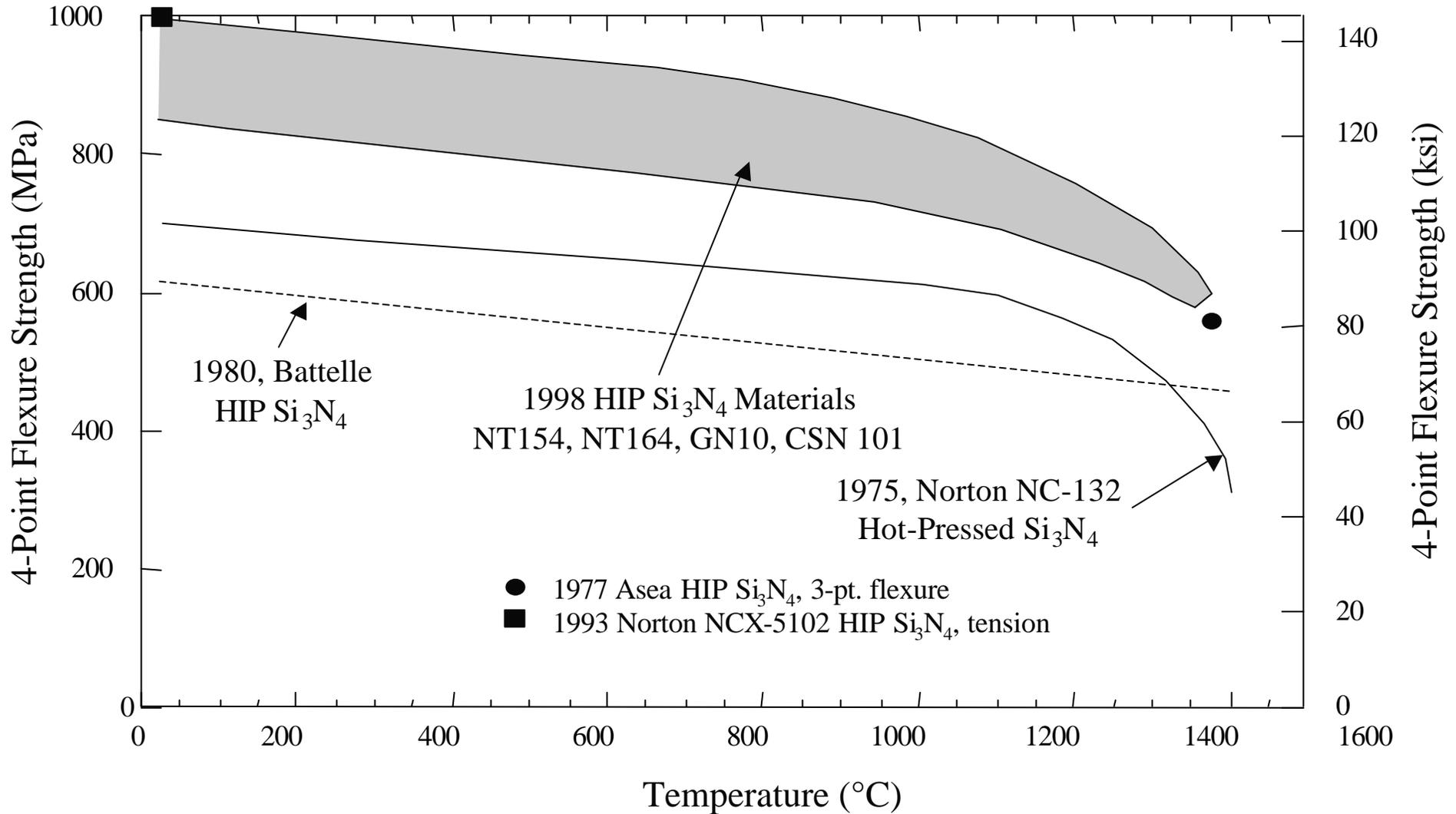
**Solar Turbines**

*A Caterpillar Company*

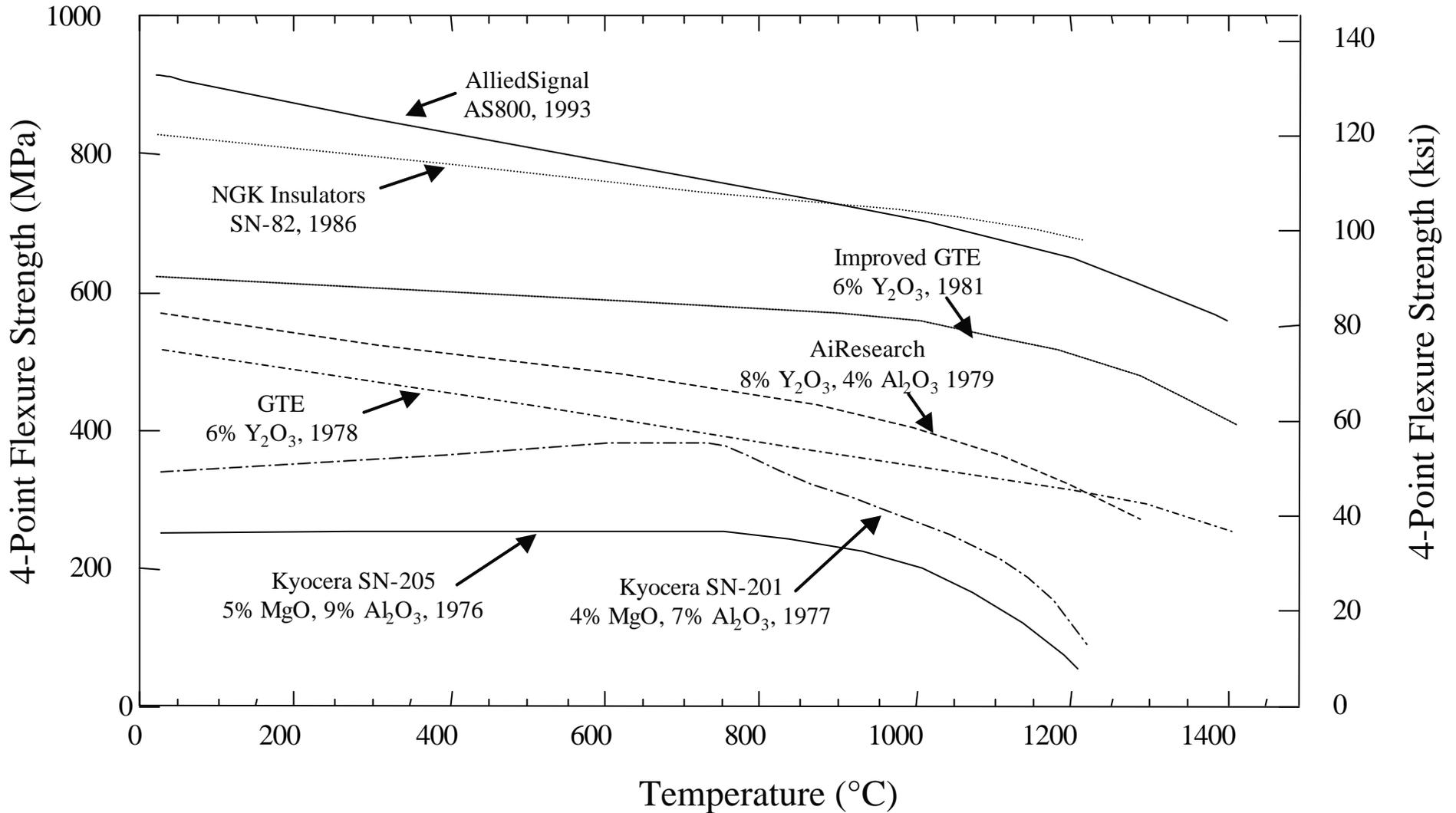
# ***Evolution of Monolithics***



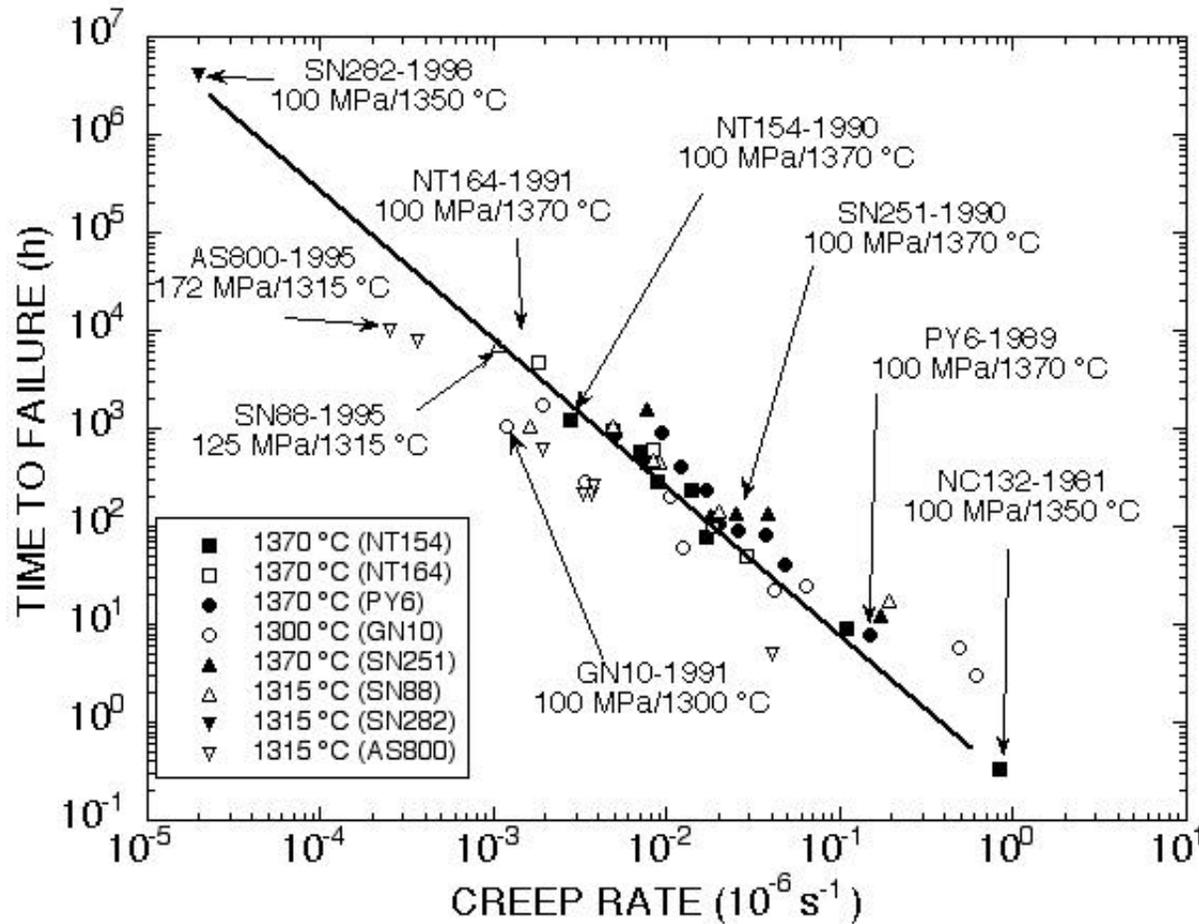
Courtesy M.K. Ferber, ORNL



Courtesy D.W. Richerson



Courtesy D.W. Richerson



Courtesy M.K. Ferber, ORNL

**Solar Turbines**

*A Caterpillar Company*

# ***Critical Technical Issues***

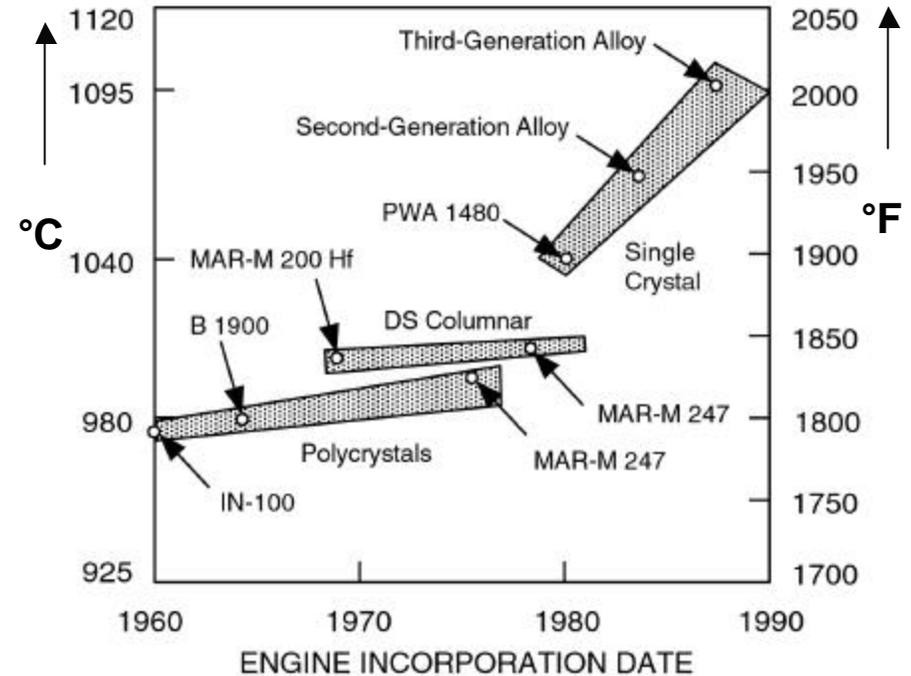
Ceramics have improved but so  
have metals

Metal Design Options up to 1500°C

- Complex Expensive Cooling Schemes

Example – TEPCO 20 MW Program

- Combined Cycle Power Plants
- Ceramic Nozzles, Blades, Combustor, Transition Piece
- 1984: Metal Components - 1100°C Capability
  - Ceramic Components for 1300°C Class Gas Turbine
- 1990: Metal Components - 1300°C Capability
  - New Ceramic Target: 1500°C Class Gas Turbine



M.D. Fitzpatrick & J.R. Price  
Solar Turbines Incorporated

093-003M

## Issue 2. Ceramics Have Insufficient Impact Resistance

- Critical for Rotor Blades, Integral Rotors (Blisks)
- Stresses > 200 MPa – Significant Mechanical Stress Component
- Foreign Object Damage (FOD), Domestic Object Damage (DOD)
  - Rig test at Daimler-Benz
  - HPSN (NC132) Gasifier Rotor
  - Survived ~ 57 hrs at T up to 1060°C
  - Failure at 42,000 rpm and 1000°C
  - Cause FOD/DOD from piece of combustor metal, melted after overheating

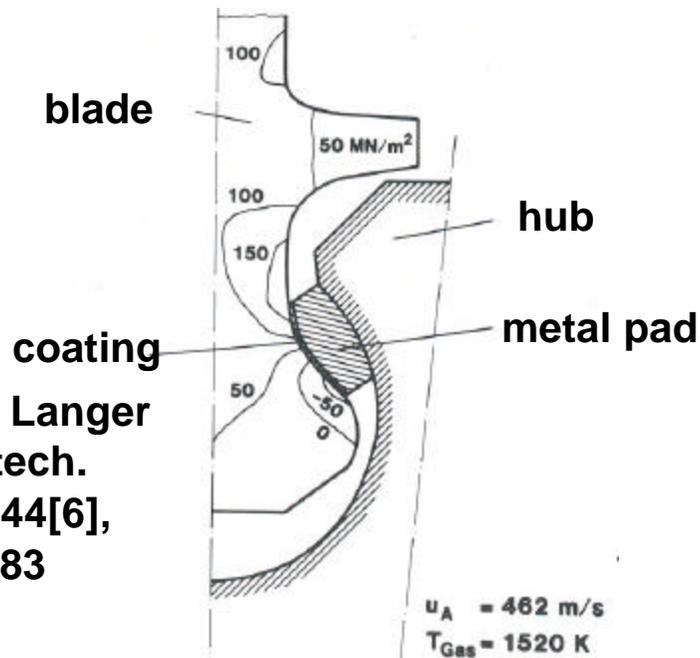


Hagemeister et al., ASME 83-GT-305, 1983



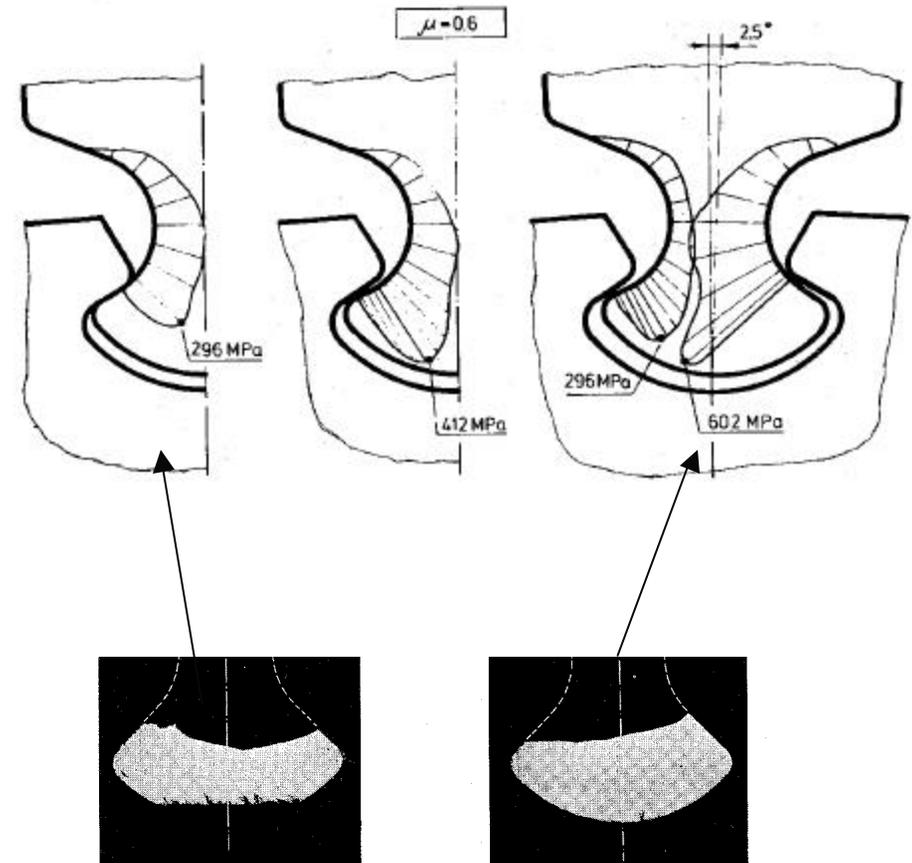
## Issue 4. Ceramics Suffer Contact Stress Damage at Metal Interface

- Critical for Inserted Rotor Blades
- Use Compliant Layer to Mitigate Contact Stresses at Blade Root
- Source of Failure in Rotor Blade Tests
- Long Term Durability of Compliant Layer Interface Uncertain



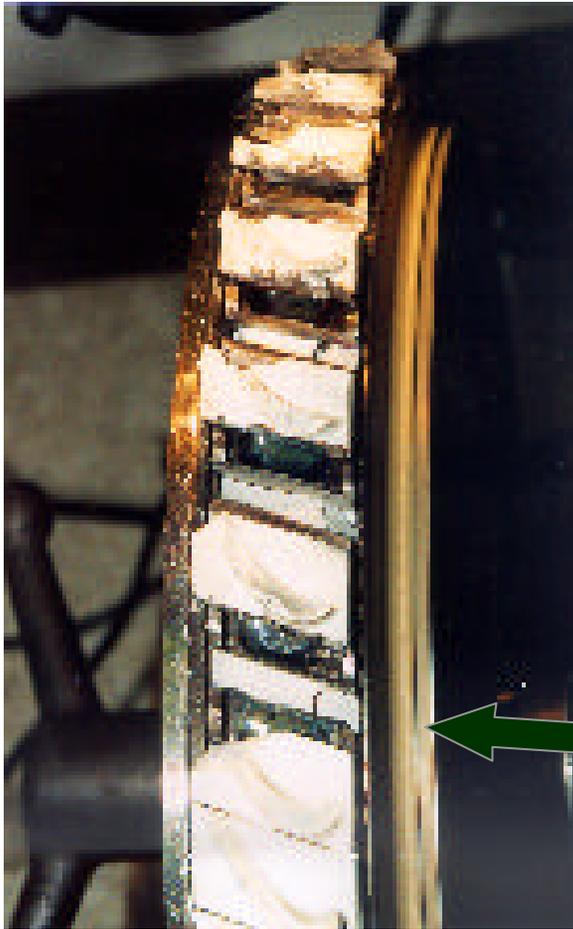
Walzer and Langer  
MTZ Motortech.  
Zeitschrift, 44[6],  
225-228, 1983

Hagemeister et al., ASME 83-GT-305, 1983



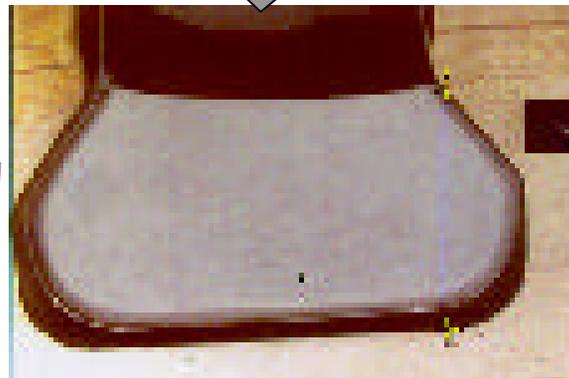
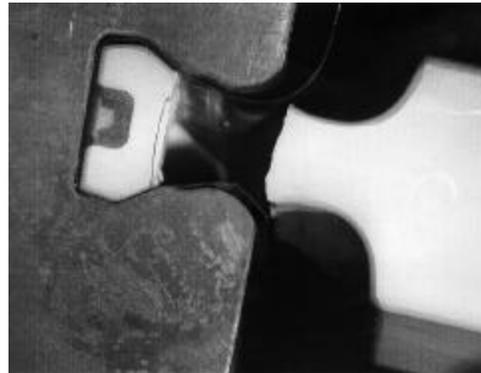
Dovetail Blade Failure, Trappman  
And Rottenkolber, 1978

# Compliant Layer and Impact Failure



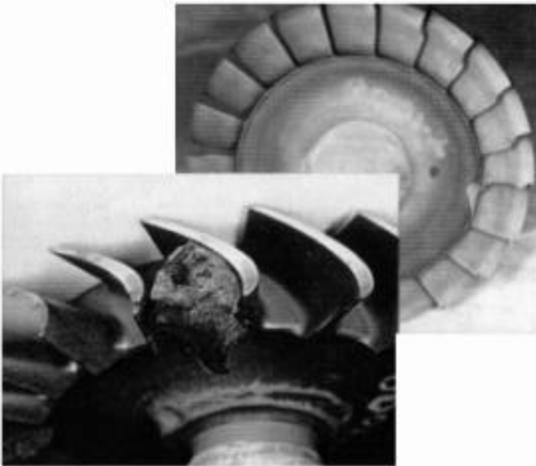
(a) Rotor with AS-800 blade residues

(c) Attachment test failure  
Ni-alloy+Pt compliant layer



(b) Failed blade root:  
Ni-alloy+Pt compliant layer

- In-house engine test 1996
- 58 hrs at 1010°C TRIT
- AS800 Si<sub>3</sub>N<sub>4</sub> Blade – Honeywell Ceramic Components
- Failure initiated as a result of compliant layer Failure
- Ni-alloy/PT CL failed in the root
- Ni-alloy/Pt/BN failed above the platform
- Secondary Impact Failure
- Attachment Test
  - Ni-alloy/Pt CL: 2 cycles
  - Ni-alloy/Pt/BN: 5000 cycle

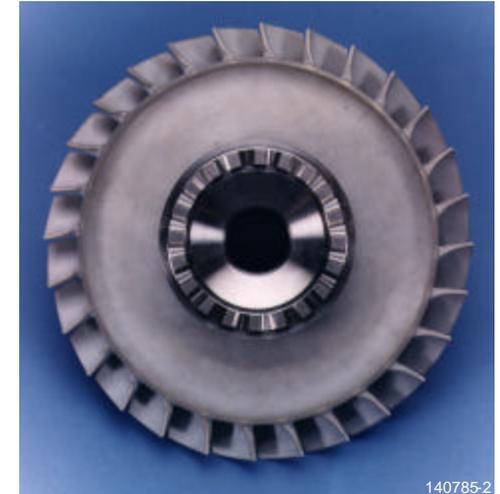


- SN252  $\text{Si}_3\text{N}_4$  Rotor
- 1000 hr Durability Test
- $T > 1427^\circ\text{C}$
- Blade Tip Rubs
- C Particle Impact
- Molten Superalloy Debris

P.Khandelwal & P. Heitman,  
Rolls-Royce, in Ceramic Gas  
Turbine Design and Test Experience  
ASME Press, 2002

### INTEGRAL ROTORS

- No Compliant Layer with Disk
- Attachment Ceramic Rotor to Metal Shaft
- Primarily Small Parts
- Ability to Fabricate Larger Parts Has Improved
- Integral Rotors are Replacing Metal Disks with Inserted Blades



140785-2



140785-3

Honeywell Rotor Operating for > 6000 hrs  
In Industrial Facility in Utah

Courtesy Honeywell Engines, Systems & Services

## Issue 5. Ceramics Need Rub Tolerance

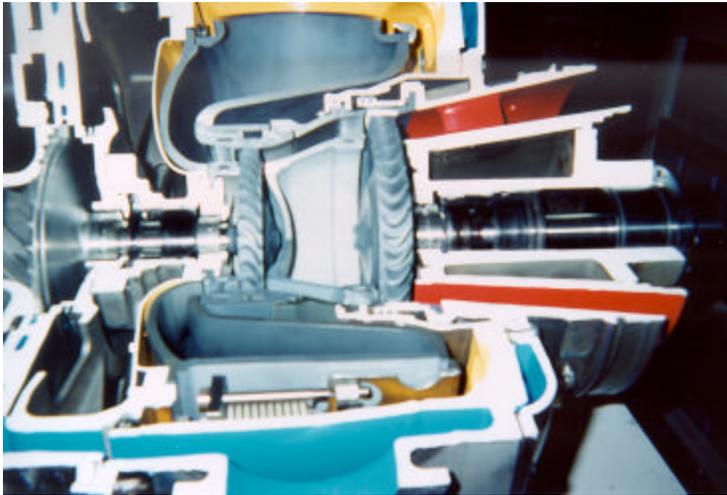
- Durability to Withstand Rubs: Critical For Optimizing Efficiency Gains
- Rotating Parts: Inserted Blades, Integral Rotors
- Important for Small Engines: Example IHI CGT301 300 kW Program

Clearance	Turbine Efficiency	Cycle Efficiency	TIT	Comments
0.2 mm	87.5%	42%	1350°C	Design Point – Engine Failure
0.8 mm (Cold) 0.5 mm (Hot)	76% 79%	35%	1350°C	Eff. Loss Primarily from Excess Clearance

Data courtesy IHI

- Need Abradable (Rub Tolerant) Tip Shroud for Clearance Control
  - Dense Silicon Nitride Base – Low-Density Surface

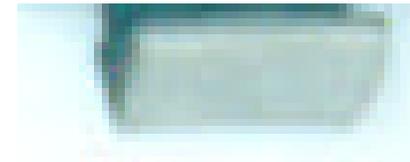
# Abradable Shroud Contributes to Efficiency



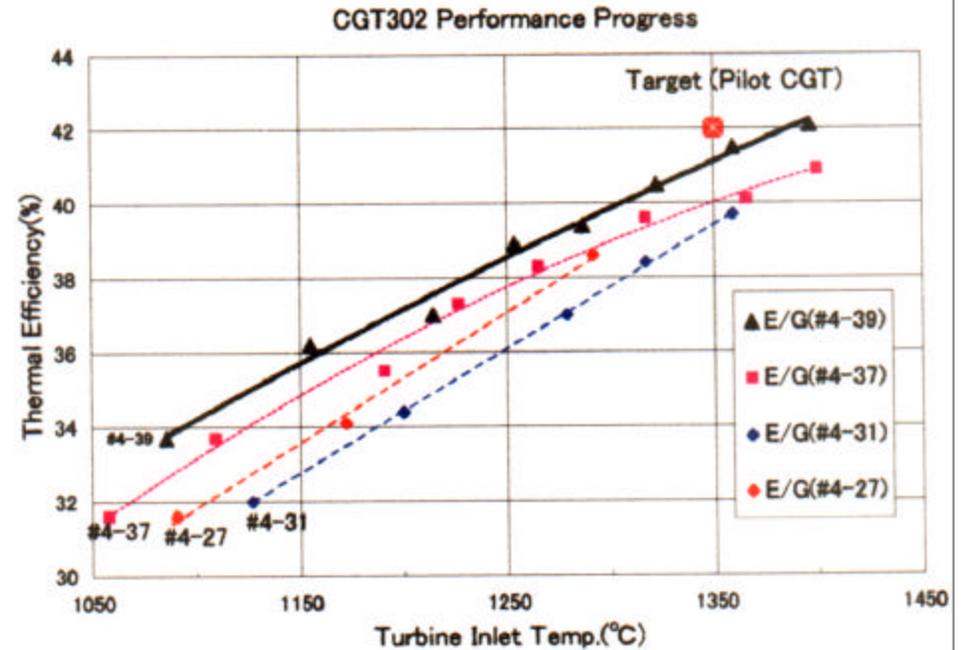
KHI CGT302 Engine Achieved 42.1% Efficiency and 322 kW Output Power at 1396°C TIT (Courtesy of KHI)



Abradable  $\text{Si}_3\text{N}_4$  Power Turbine Shroud  
(Fabricated by Kyocera Corp.)



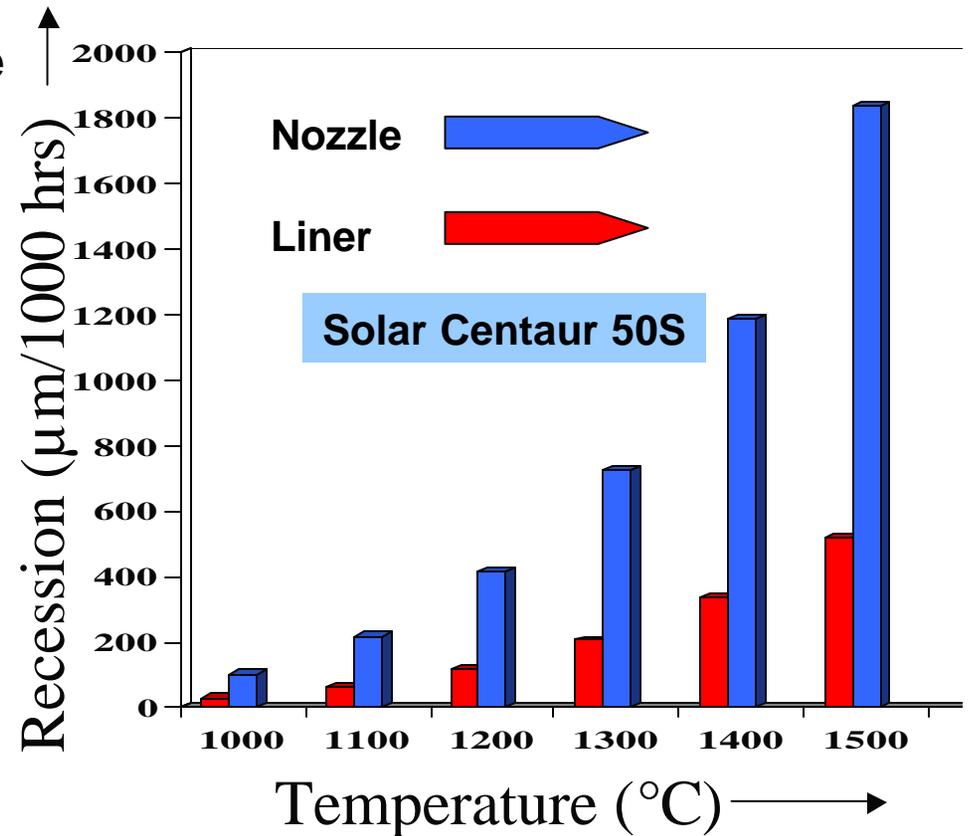
Abradable  $\text{Si}_3\text{N}_4$  Shroud Fabricated By Technolghia (Russia)



Courtesy of KHI

# Issue 6. Environmental Degradation

- Silicon-Based Ceramics Degrade in the Gas Turbine Environment
- Solar CSGT Centaur 50S Surface Recession (30,000 hrs)
  - TRIT = 1121°C
  - Nozzle
    - Hot Spot - 1300°C: 24 mm
    - Nominal - 1150°C: 12 mm
  - Combustor Liner
    - Hot Spot - 1250°C: 5 mm
    - Cold Spot - 1000°C: 1 mm



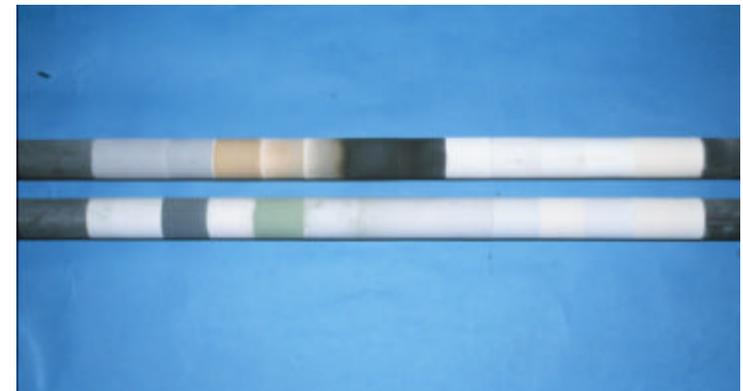
NASA Formula (SiC):

$$k(\text{lean}) = 2.04 \exp(-108,000/RT) P^{1.5} v^{0.5}$$

- Corrosion Resistant Coatings for Ceramic Heat Exchanger Tubes (GRI Contract to Solar)
  - M. van Roode et al. ASME 91-GT-38
- Aluminum Remelt Processing – Corrosive Attack by Alkali Chlorides, Cryolite on Heat Exchanger Tubes
- Ceramic Oxide-Based Coatings (0.5 – 1.3 mm thick)
  - **Mullite, Zircon, Hafnia, Alumina, Zirconia, mullite-alumina-zirconia**
  - Single-Layer, Multi-Layer, Graded
  - a-SiC (Hexoloy SA, Si-SiC (Coors SCRB 210), Nextel/SiC (Syconex), SiC/alumina Substrates
  - Coatings Applied by Air Plasma Spray
  - Alkali Etch to Roughen Substrate Surface



Tubes Exposed for 4000+ hrs  
In Aluminum Remelt Heat  
Exchanger Test, Reynolds  
Aluminum, Mussel Shoals, AL

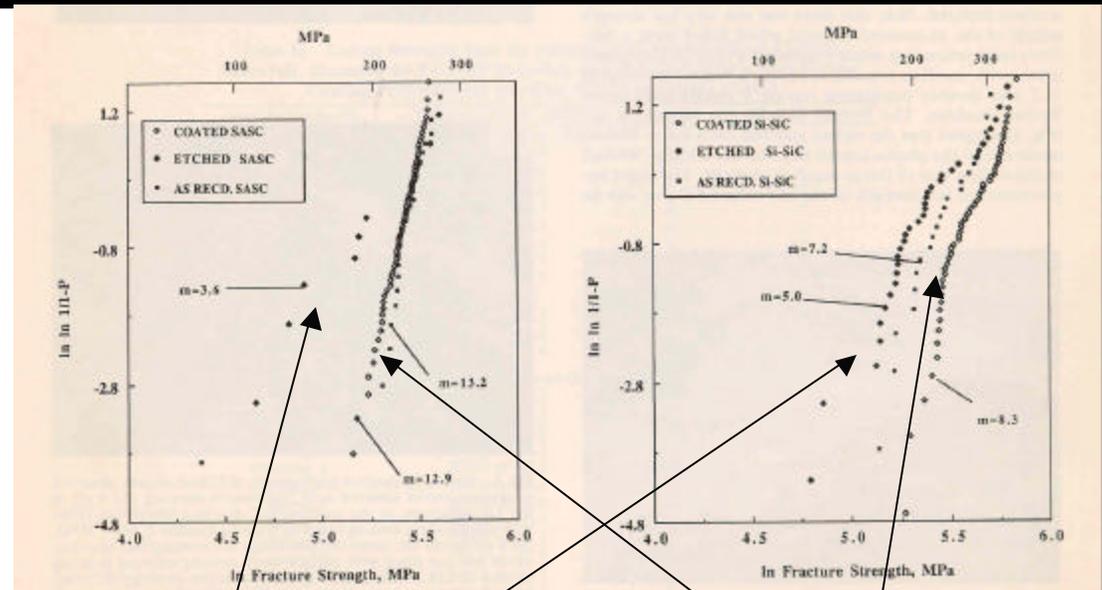


Chemical compatibility, Expansion Match with Substrate, Low Modulus

ORNL: Thermal Cycling in Air (50 cycles/300-1300°C/2 hrs) – Coatings showed no degradation

Corrosion Rig: 1000–3000 hrs

- Coatings Were Protective
- Long Term: Cracking Debonding

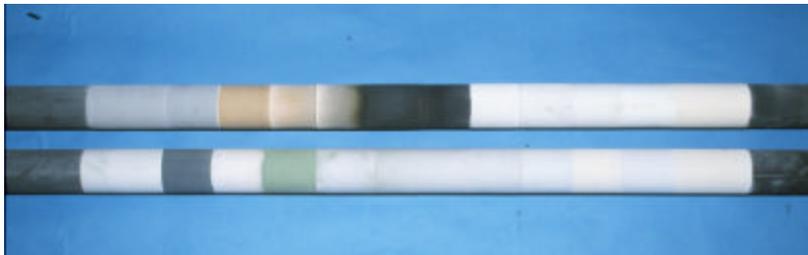
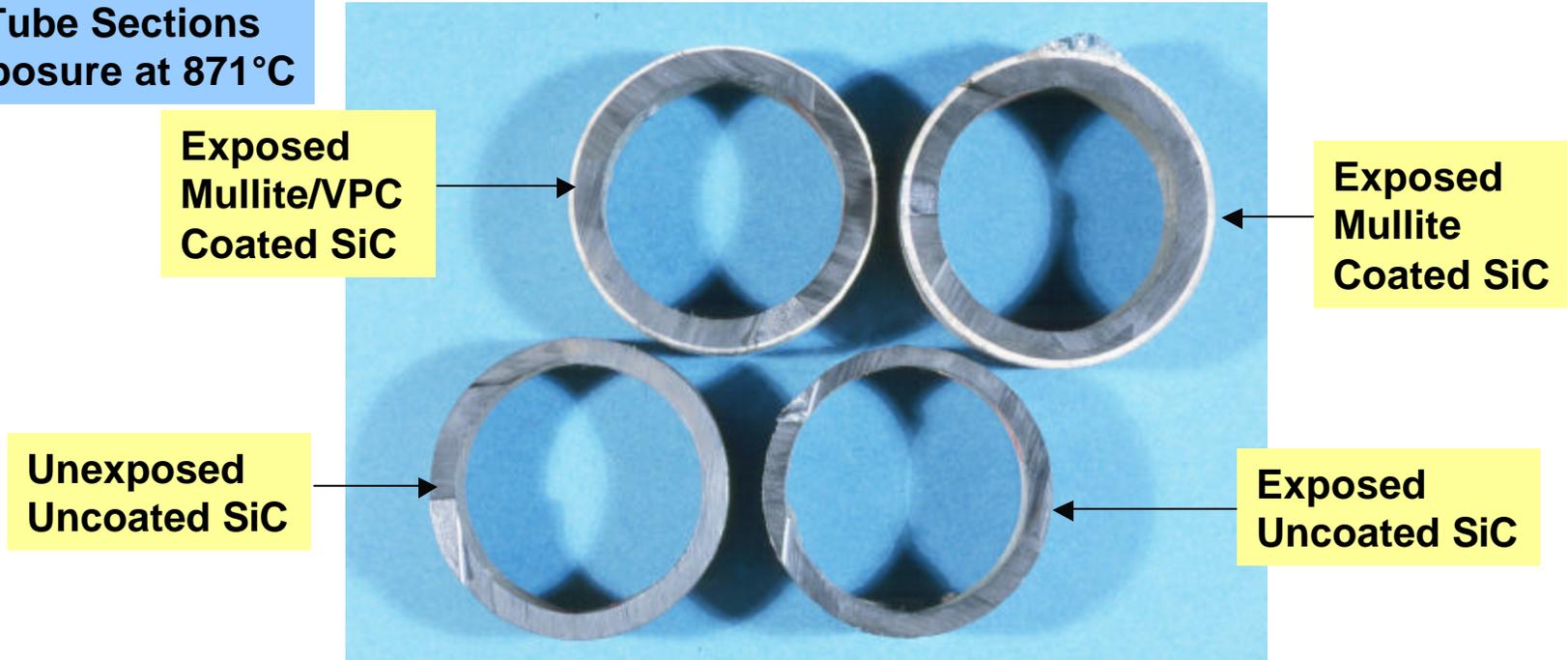


Etched Substrate  
Strength Loss

Coating Restored  
Strength

C-Ring Testing at Penn State CAM  
D. P. Butt et al. J.Am.Ceram.Soc., 73[9],2690-6(1990)

Coors SCR210 Tube Sections  
after 2000 hrs Exposure at 871°C



As Coated Coors SCR210 Tubes



After 1000 hrs Exposure at 871°C

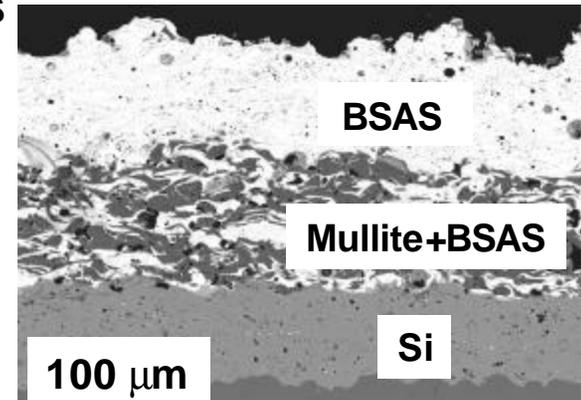
- DOE/Solar CSGT and Advanced Materials Contracts – 1996 – Current
- SiC/SiC CMCs (DuPont Lanxide/AS-ACI/HACI/PSC and Goodrich Corp.)
- GC, Hi-Nicalon, Tyranno ZM Fibers – CVI and MI Matrices - Multi-Layer EBC (UTC)
- 50,000 hrs of Engine Testing – 13,937 Hrs and 15,144 Hrs
- **EBC Extends Life of CMC 2-3 Fold**



**ChevronTexaco  
Bakersfield, CA**



**Malden Mills  
Lawrence, MA**

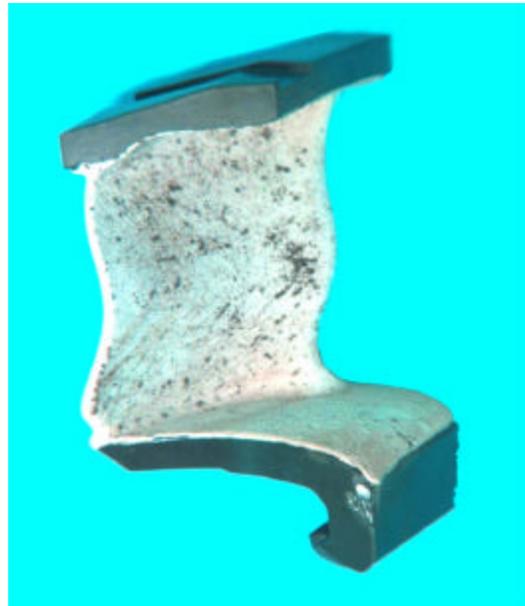


### Initial EBC Coating Trials with Solar Centaur 50S Nozzle (SN88) Promising

No Spallation Observed



As-Coated

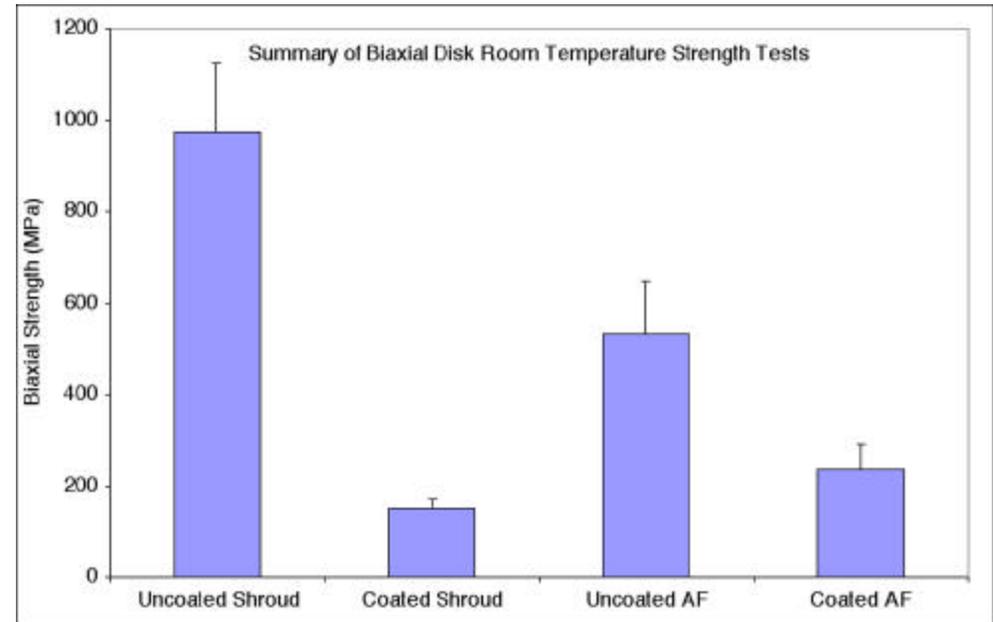


After Thermal Cycling  
and Burner Rig Testing

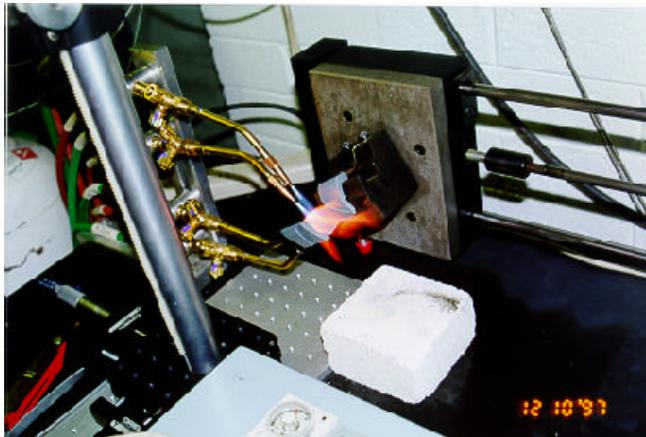
#### UTRC Development Work

- Solar SN88 nozzle coated with 3 layer EPM/DOE EBC
- \* Thermal cycled 50X RT to 1300°C in air, 1 hour cycles
- 457 m.s<sup>-1</sup>/1250°C burner rig testing 5 hrs/5 cycles

- Limited Study for CSGT Program
- One SN88 and two SN282 Si<sub>3</sub>N<sub>4</sub> Nozzles
- Test in Gradient Temperature Rig
  - RT-> 1190°C in 18s
  - 113% of Max. SS Stress
- Nozzles that Had Passed the Proof Test were Coated with UTRC EBC



Data Courtesy M.K. Ferber, ORNL



**SN88/EBC Nozzle Survived Intact**  
**2 SN282/EBC Nozzles Failed**  
**1 SN282/EBC Nozzle Not Tested**



**Solar Turbines**

*A Caterpillar Company*

# ***Commercialization Issues***

- **Gas Turbine Applications are a Small Niche Market for Ceramics**
- **Large Scale Applications Have Not Materialized To-Date**
- **Insufficient Durability in Industrial Gas Turbine Environment**
  - **Impact Resistance, Environmental Degradation**
- **Component Cost Needs to be Competitive with Cost of Metal Parts**
  - **CMC Components: Cost Substantially Greater**
  - **Volume Cost of Monolithic Parts is Competitive**
- **Need a Strong Supplier Base**
  - **Suppliers Have Exited the Gas Turbine Component Arena**
  - **Suppliers Have Reduced Development Efforts**
  - **Suppliers Have Restricted Sale of Materials**
- **Less Funding for Ceramic R&D Programs**

● **Next Generation of Monolithics**

● **Further Improvements in Strength and Toughness**

● **Improved Impact Resistance**

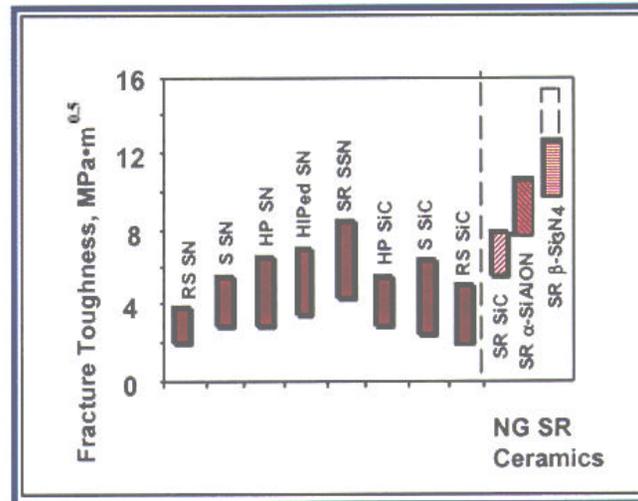
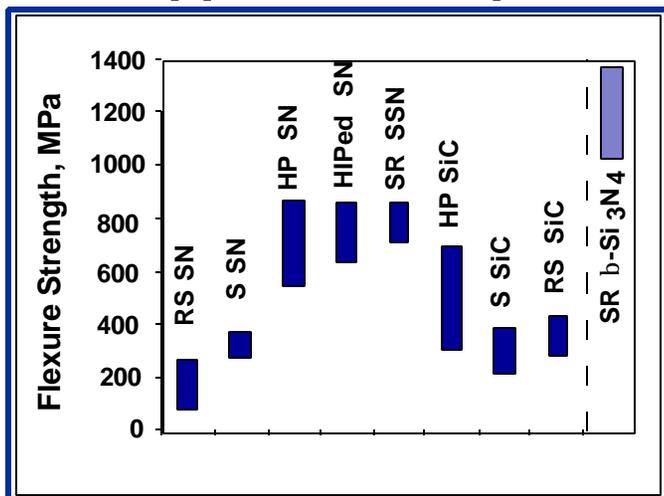
● **Fundamental Research in Processing**

● **Highly Aligned Elongated Reinforcing Grains (Seeding of Powders)**

● **Tailoring of Sintering Additives**

● **NG SR Ceramics:  $\beta$ -Silicon Nitrides,  $\alpha$ -Sialons, SiC**

● **Supplier Participation**



W.D. Carruthers et al.,  
ASME GT-2002-30504

- **Less Mature than SiC/SiC EBCs**
- **Chemical Stability/Inhibit Oxidation in Gas Turbine Environment**
- **Adherence to Substrate**
- **Thermal Expansion Match with Substrate**
  - **EBC on  $\text{Si}_3\text{N}_4$  EBC Lower CTE than EBC on SiC/SiC CMC**
- **Not Adversely Affect Mechanical Properties of Substrate**
- **Minimize Surface Damage During Application**
- **Combine Environmental and Impact Resistance**
- **Thinner EBC (compared to CMC EBC) to Retain Favorable Aerodynamics**
- **Mechanical Property and Oxidation/Recession Testing**
- **NDE Methodology to Establish EBC Integrity**
- **EBC Life Prediction Methodology**

**Solar Turbines**

*A Caterpillar Company*

# *Summary*

- **Ceramics are Enabling Materials for Improving Performance and Emissions Reduction in Gas Turbines**
- **Properties and Processing of Monolithic Ceramics and CMCs Have Significantly Improved over the Past 40 Years**
- **Ceramic Components Have Been Demonstrated for Thousands of Hours in Test Rigs and Gas Turbines - Need 30,000+ Hrs of Life**
- **Critical Issues for Monolithics to be Competitive with Metals**
  - **Impact Resistance, Surface Condition, Contact Stress Resistance (Slow Crack Growth Resistance), Rub Tolerance, Environmental Resistance**
- **Durable High Performance Component Designs**
- **Develop EBCs for Long Service Life**
- **Cost Goal: Competitive with Cost of Metal Components**
- **Fundamental Research to Resolve Barriers to Commercialization**