

**ASME Internal Combustion Engine Division
2004 Fall Technical Conference**

**High-T NO_x Sensing Elements using
Conductive Oxides and Pt**

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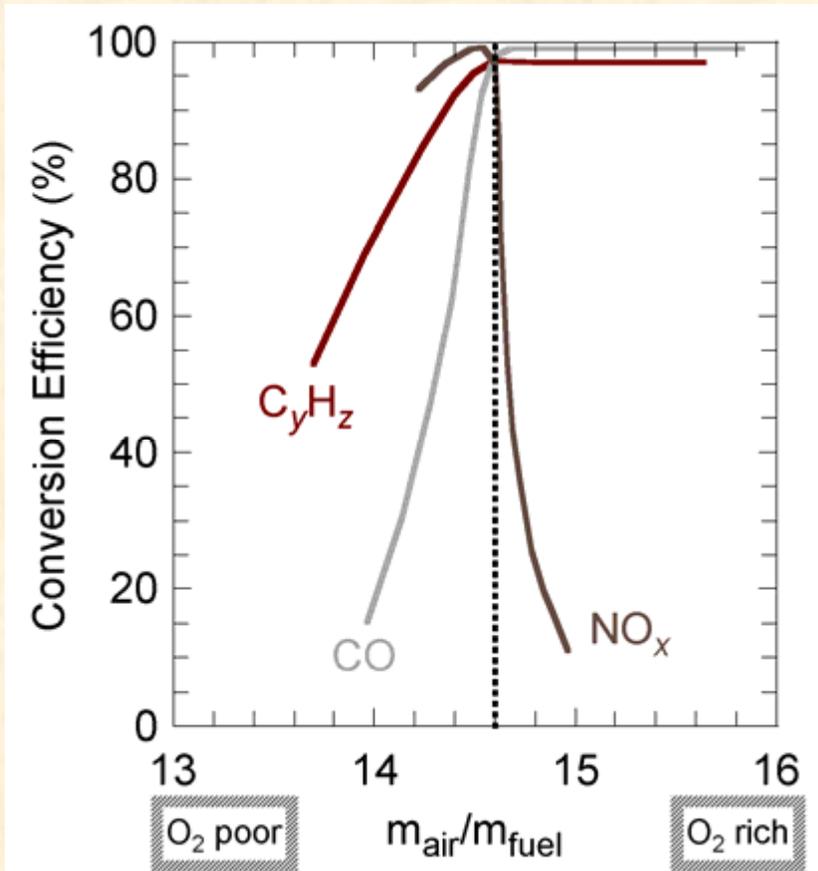
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Background I – need for NO_x sensors

Three-way catalyst (TWC) efficiency†



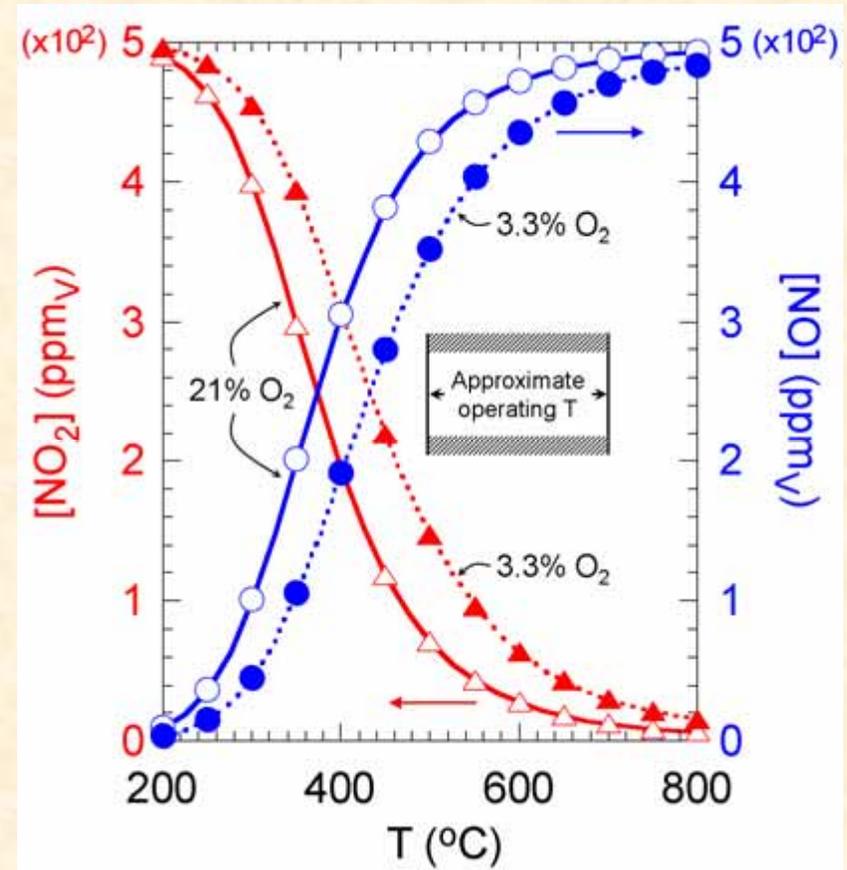
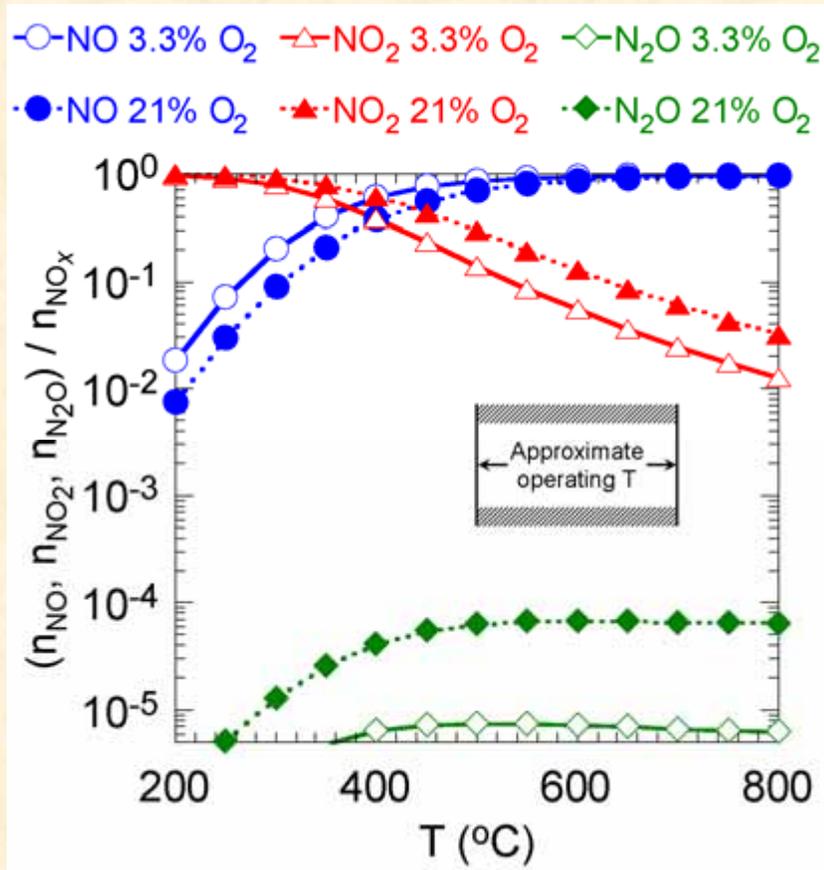
- ⇒ Currently, TWC unable to remove NO_x from O₂-rich (e.g., diesel, lean-burn) exhausts.
- ⇒ These exhausts will require NO_x remediation with NO_x traps (LNT) or reagent injection (SCR).
- ⇒ Both technologies will require compact and robust NO_x sensors.
- ⇒ Sensor controls trap regeneration for LNT, reagent injection for SCR.
- ⇒ Sensor operating conditions:
T ~600°C, ~10–1000 ppm_V NO_x,
varying [O₂].‡

†Woestman and Logothetis, *The Industrial Physicist*, **1**, (1995).

‡Menil, Coillard, and Lucat, *Sensors and Actuators B*, **67**, (2000).

Background II: NO_x species

Equilibrium NO_x abundances†



⇒ NO is dominant equilibrium NO_x species above 500 °C.

†In mixtures of N₂ and O₂, FactSage (Thermfact Ltd., Quebec) used for calculations.

Experimental approach and methodology

⇒ Experimental approach

- ◆ High-T NO_x sensing elements based on YSZ.
 - ⇒ Co-planar sensing elements (conductive oxide / Pt).
- ◆ Vary conductive oxide and element geometry.
- ◆ Study effects of DC constant current "bias".[†]

⇒ Methodology

- ◆ Electrodes applied by screen printing and thermal treatment.
- ◆ Tube furnace used to simulate elevated temperature service.
- ◆ Test parameter boundaries:
 - ⇒ $500\text{ °C} \leq T \leq 700\text{ °C}$.
 - ⇒ $20\text{ ppm}_V \leq [\text{NO}_x] \leq 1500\text{ ppm}_V$, $[\text{O}_2] = 7\text{--}20\text{ vol\%}$, bal. = N₂.

⇒ Performance metrics

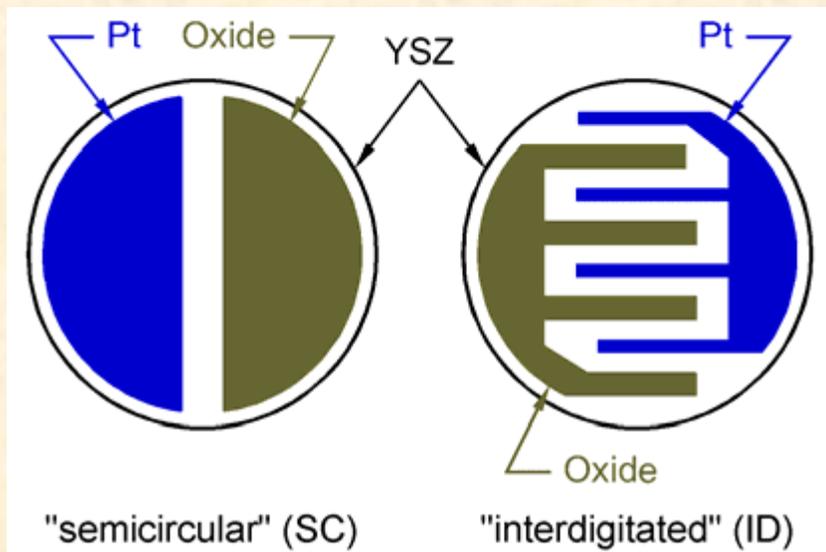
- ◆ NO₂ and NO response magnitude, effect of varying [O₂].
- ◆ Response/recovery time.

[†]Miura *et al.*, *Solid State Ionics*, **65**, pp. 283-90 (1999);

Ho *et al.*, *Journ. Cer. Soc. Jpn.*, **104**, pp. 995-9 (1996);

Grilli *et al.*, *Journ. Electrochem. Soc.*, **148**, pp. H98-102 (2001);

Sensing element geometries, test fixture schematic



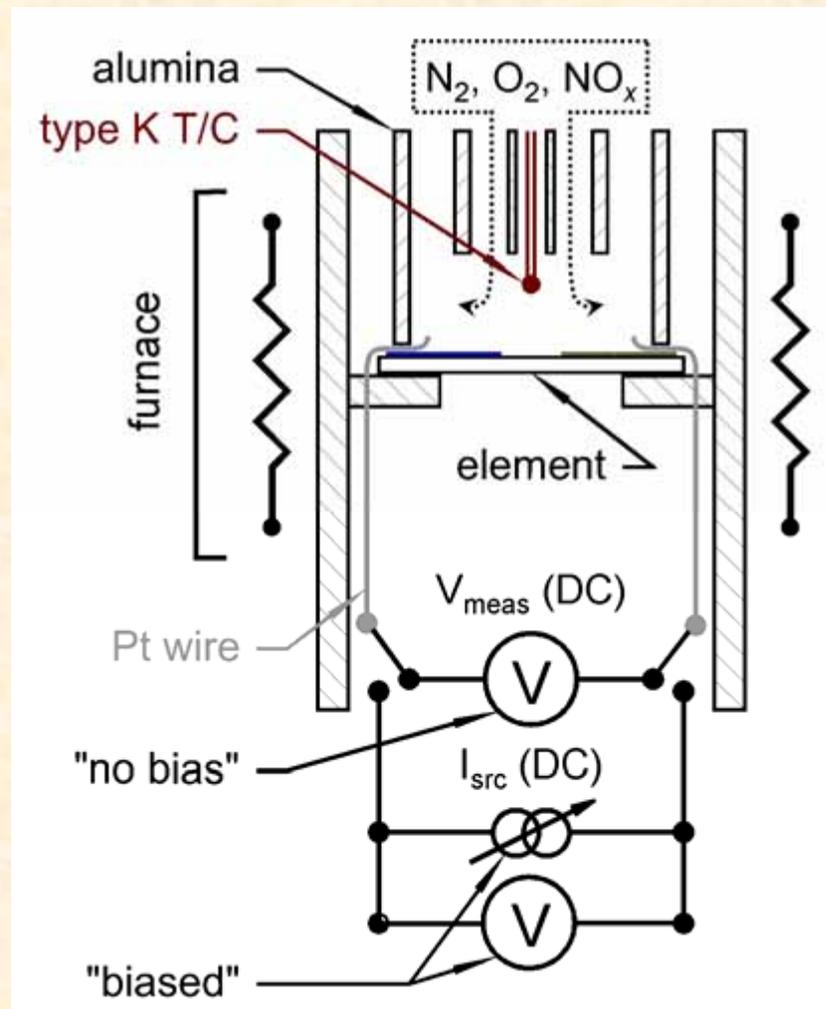
⇒ YSZ (Tosoh TZ8YS) substrate.

◆ dia. ~16 mm, thickness ~1 mm.

⇒ Screen printed electrodes.

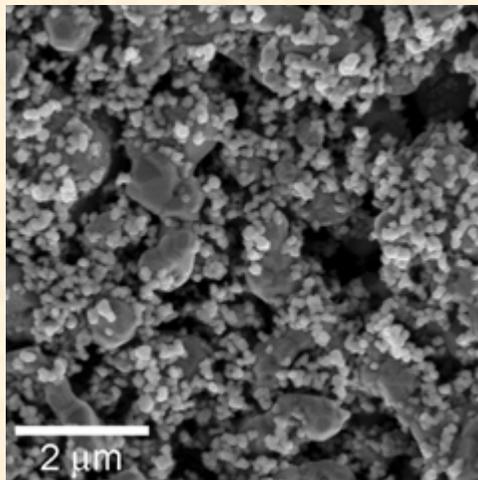
◆ T_{fire} (°C) = 1100 (Pt), 900 (oxide).

◆ Oxides: $\text{La}_{0.85}\text{Sr}_{0.15}\text{CrO}_3$ (LSC),
 $\text{La}_{0.85}\text{Ba}_{0.15}\text{CrO}_3$ (LBC),
 $\text{La}_{0.80}\text{Sr}_{0.20}\text{FeO}_3$ (LSF).

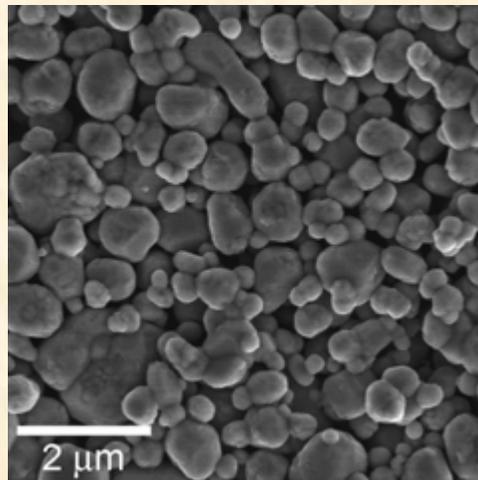


Electrode microstructures and thickness

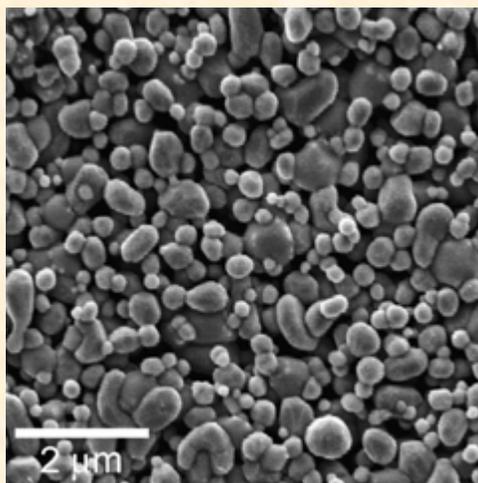
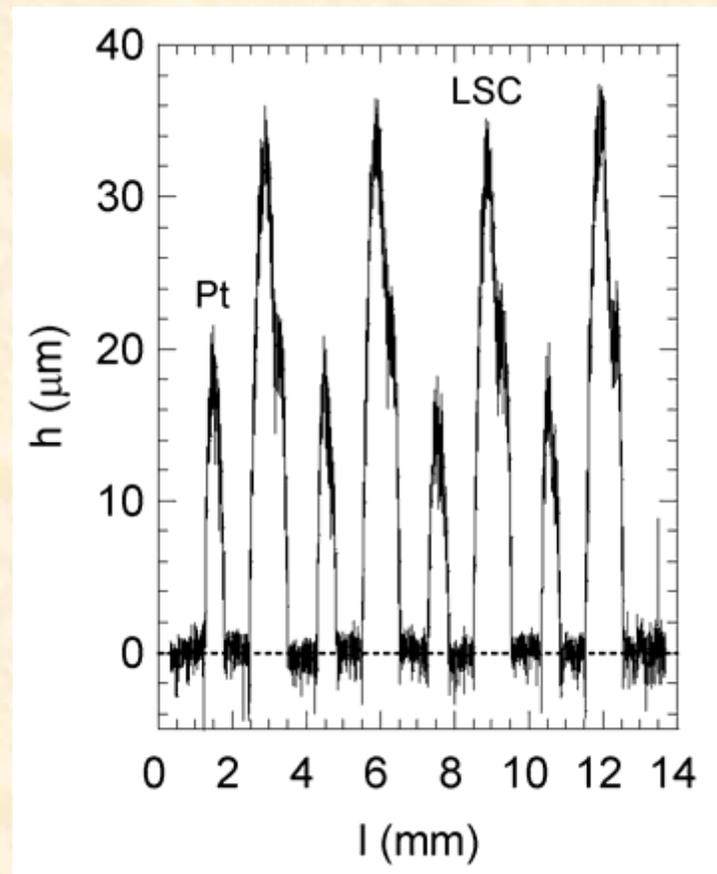
Pt



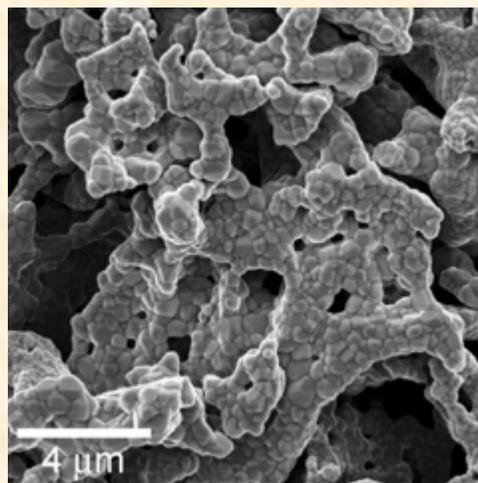
LSC



LSC/Pt interdigitated



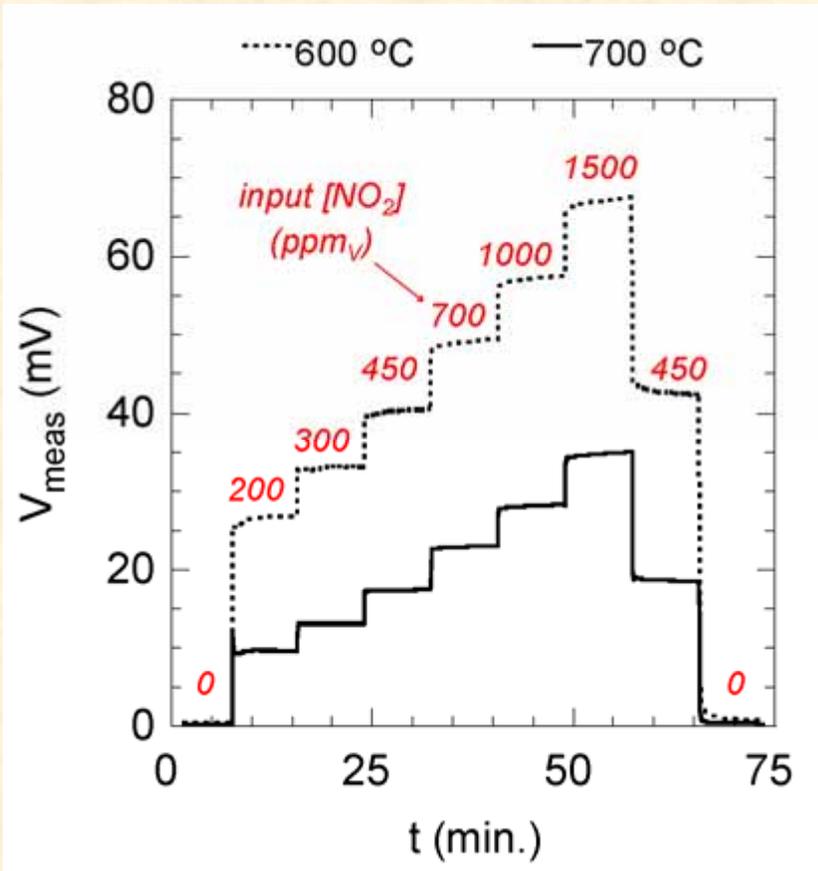
LBC



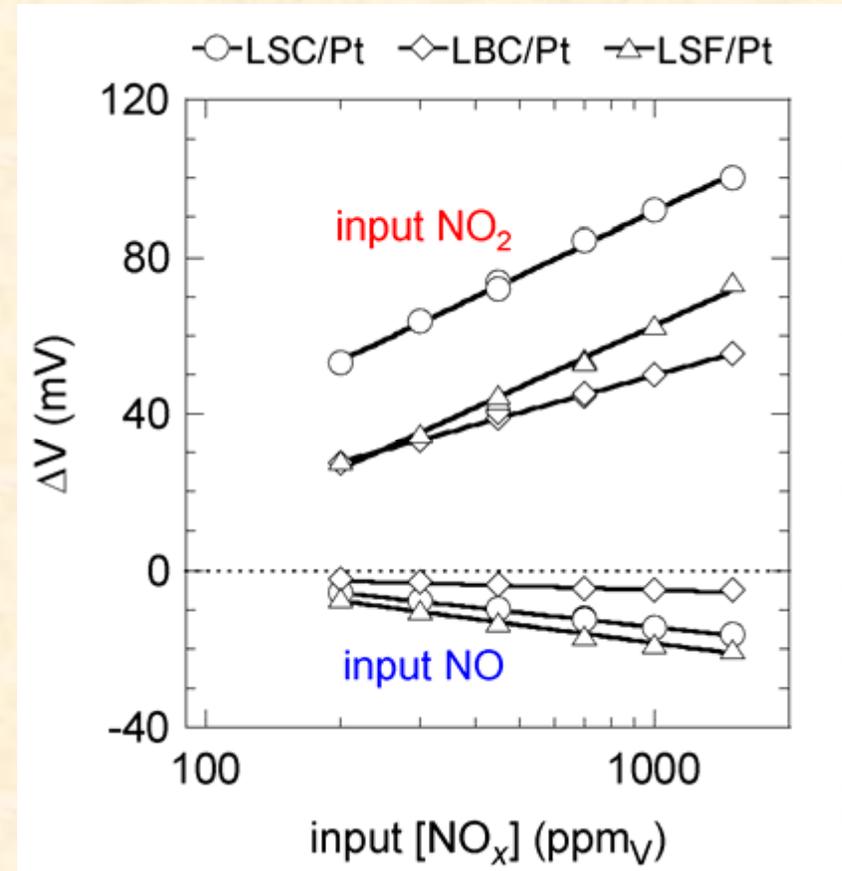
LSF

No bias: Strong NO₂ response

$$V_{\text{meas}} = f(t) \text{ (LSF/Pt, 13 vol\% O}_2\text{)}$$



$$V_{\text{meas}} = f([\text{NO}_x]) \text{ (600 °C, 7 vol\% O}_2\text{)}$$



⇒ Semicircular (SC) geometries.

⇒ Mechanism for *in situ* NO_x → NO₂[†] required, focus on NO₂ response.

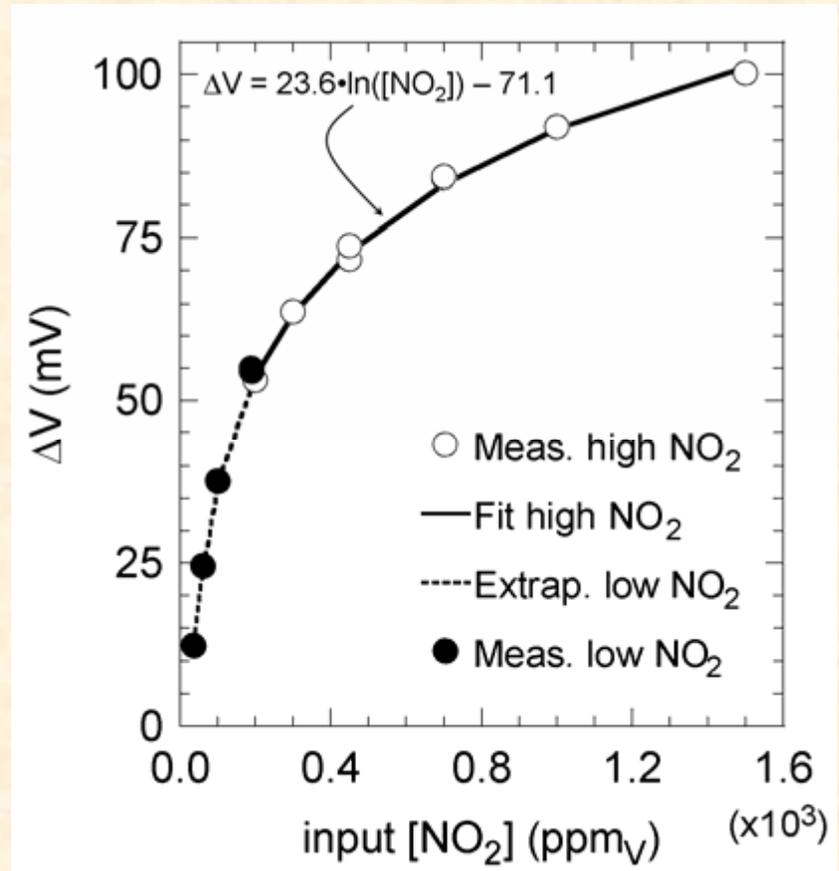
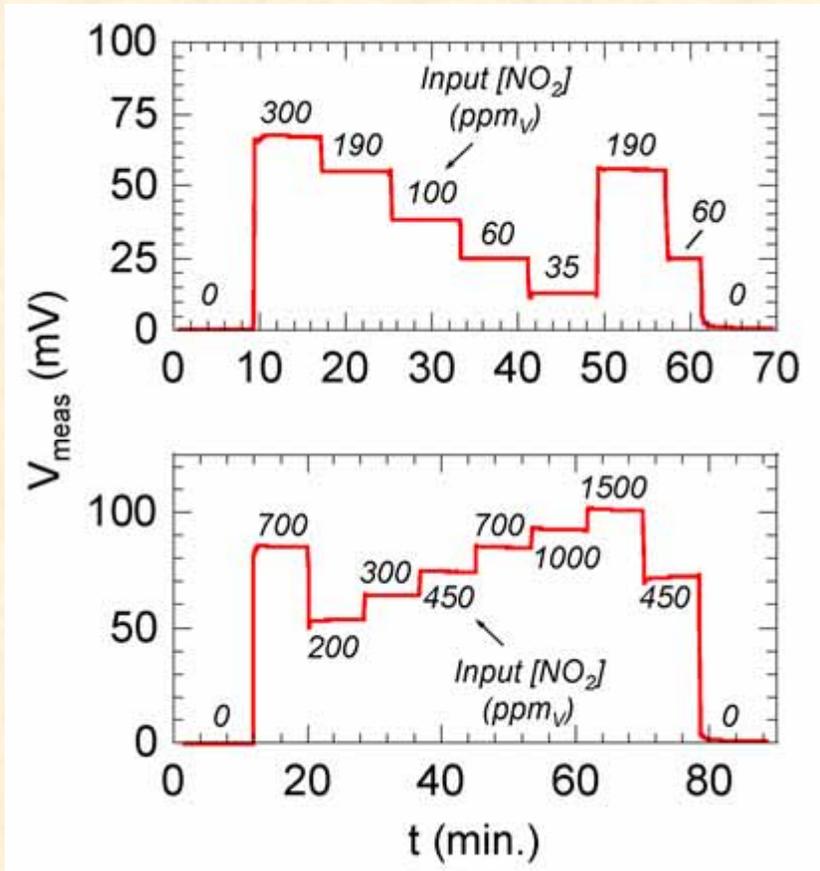
[†]Szabo and Dutta, *Sens. Actuators B; Chem.*, **88**, pp. 168-77 (2002);

Kunimoto *et al.*, *SAE Tech. Pap. Ser. 1999-01-1280* (1999)

No bias: Logarithmic signal over a wide [NO₂]

$$V_{\text{meas}} = f(t)$$

$$\Delta V = f([\text{NO}_2])$$

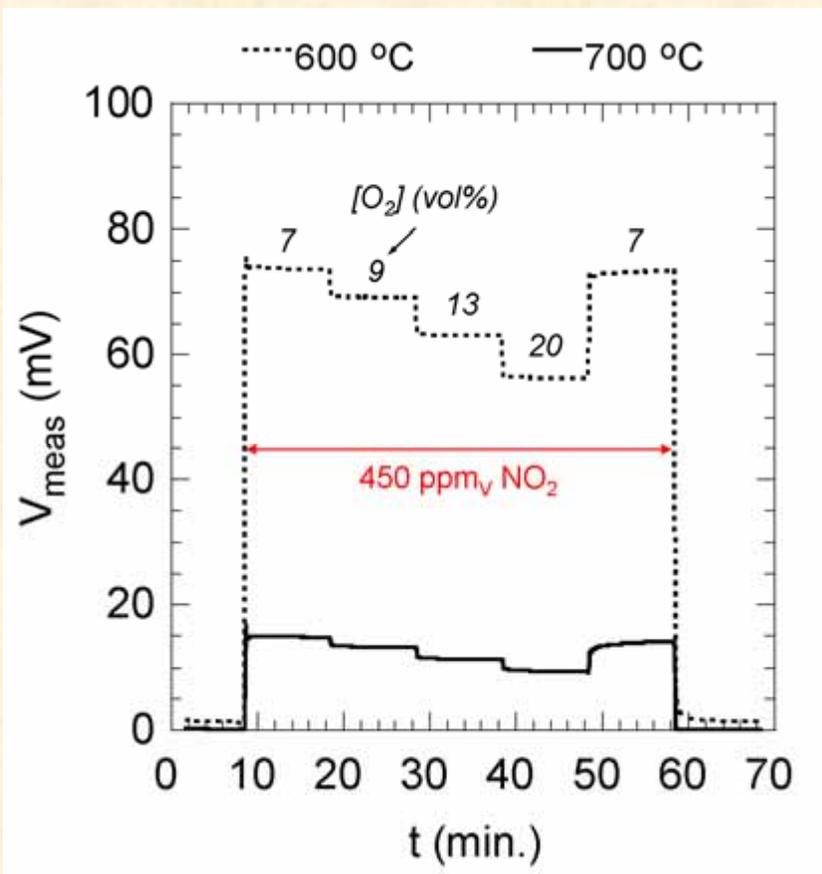


⇒ Data collected at 600 °C, 7 vol% O₂.

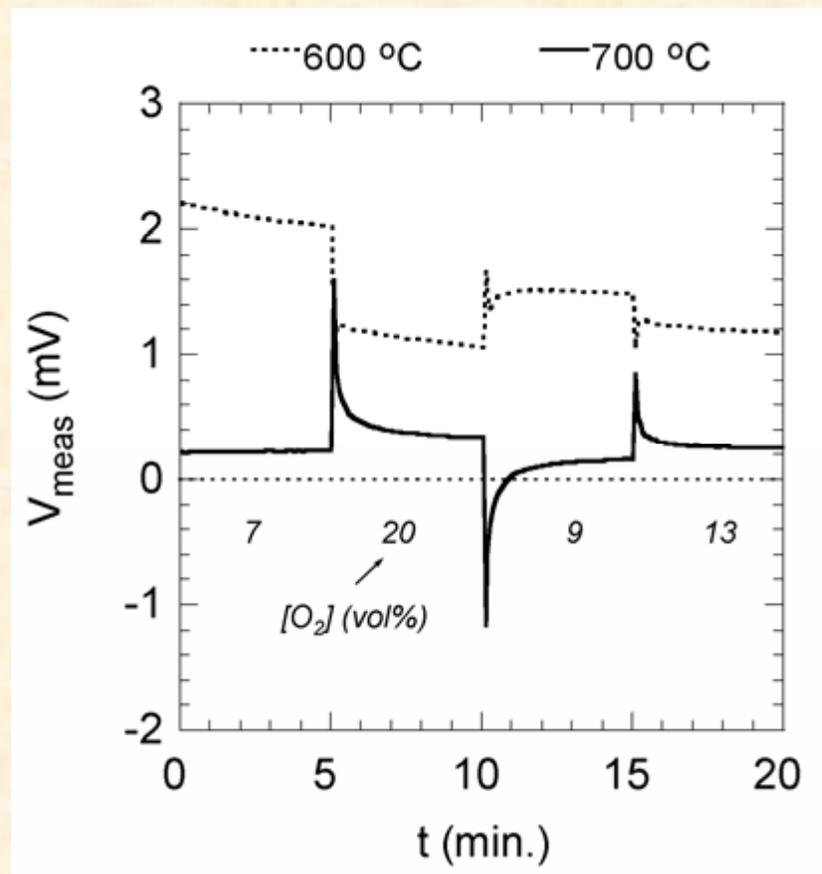
⇒ LSC/Pt sensing element, semicircular (SC) geometry.

[O₂] affects response to NO₂

Varying [O₂] with 450 ppm_v NO₂



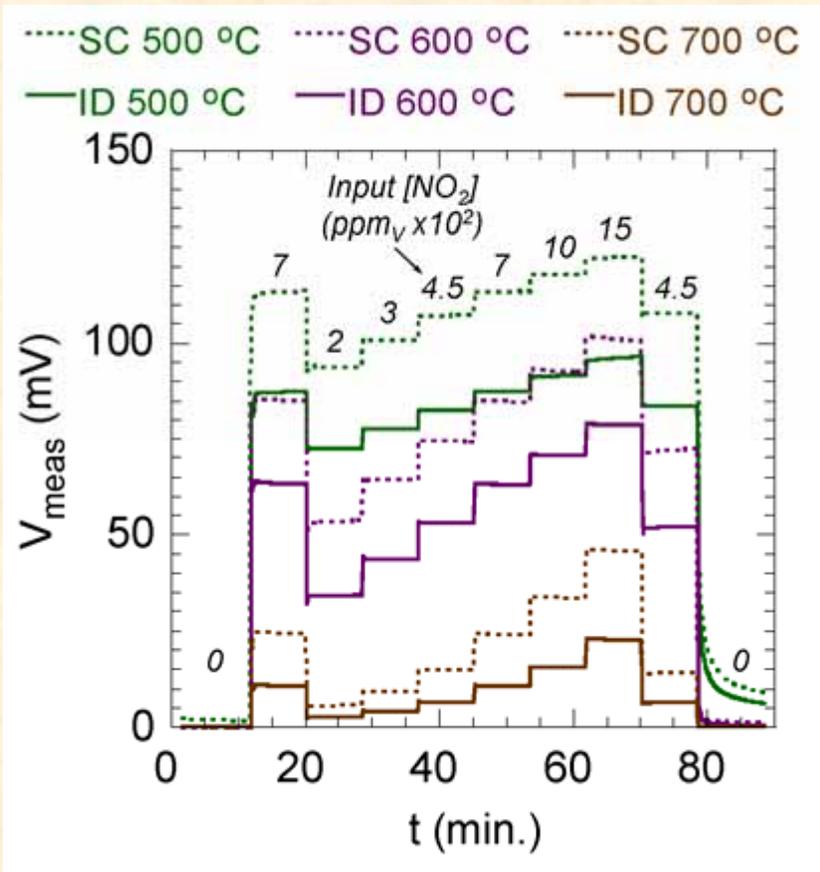
Varying [O₂] with 0 ppm_v NO₂



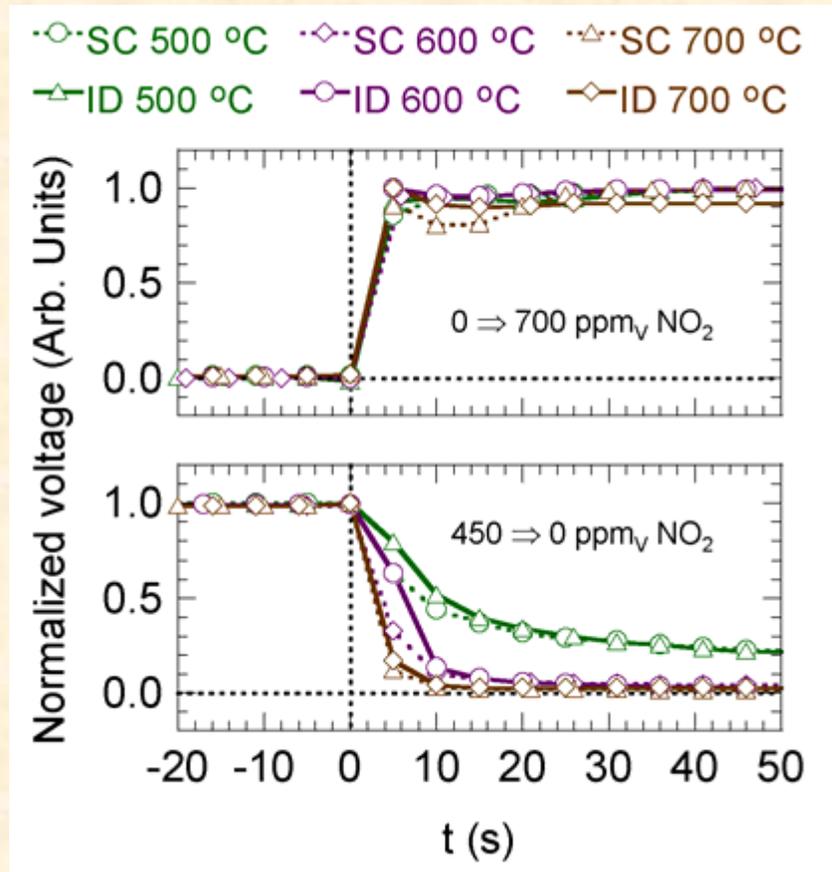
⇒ LSC/Pt sensing element, semicircular (SC) geometry.

T controls signal magnitude, recovery time

Varying $[\text{NO}_2]$



Step response / recovery



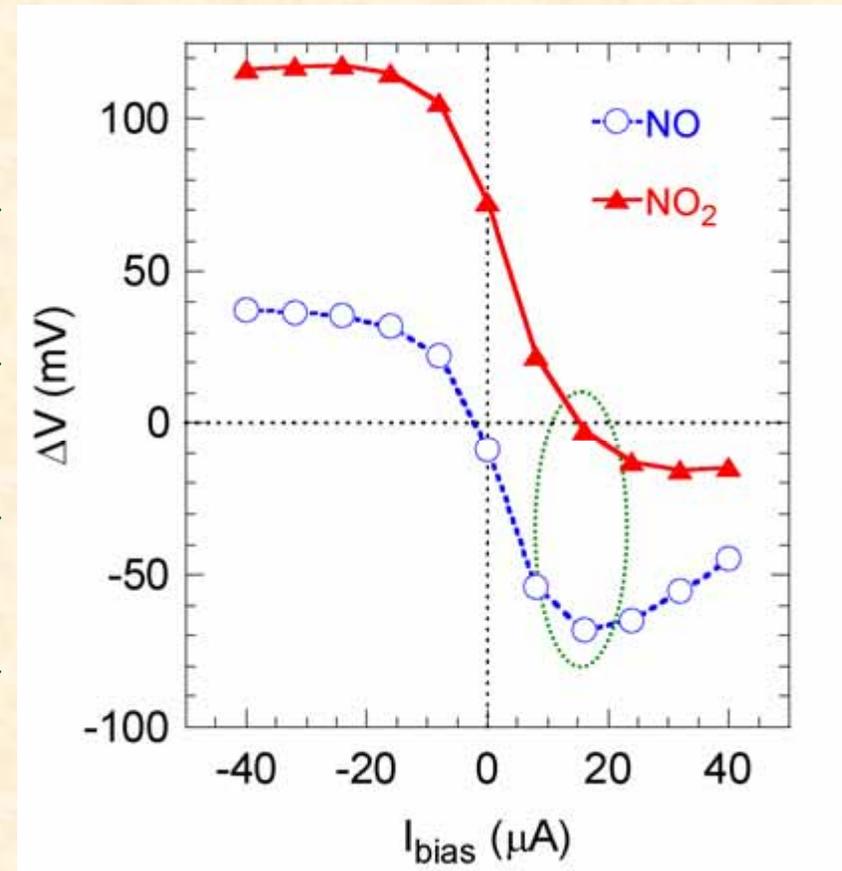
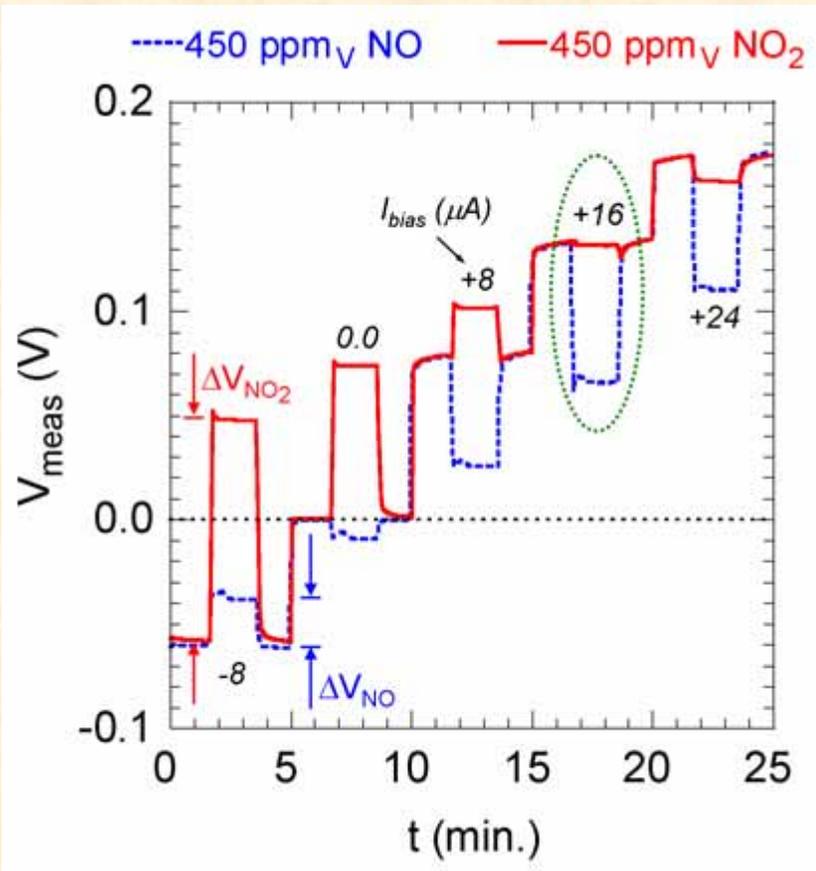
⇒ SC = "semicircular", ID = "interdigitated".

⇒ LSC / Pt sense elements, data collected in 7 vol% O_2 .

Effect of varying I_{bias} on NO_x responses

Pulses of 450 ppm_v NO_x at varying I_{bias}

$$\Delta V = f([I_{bias}])$$

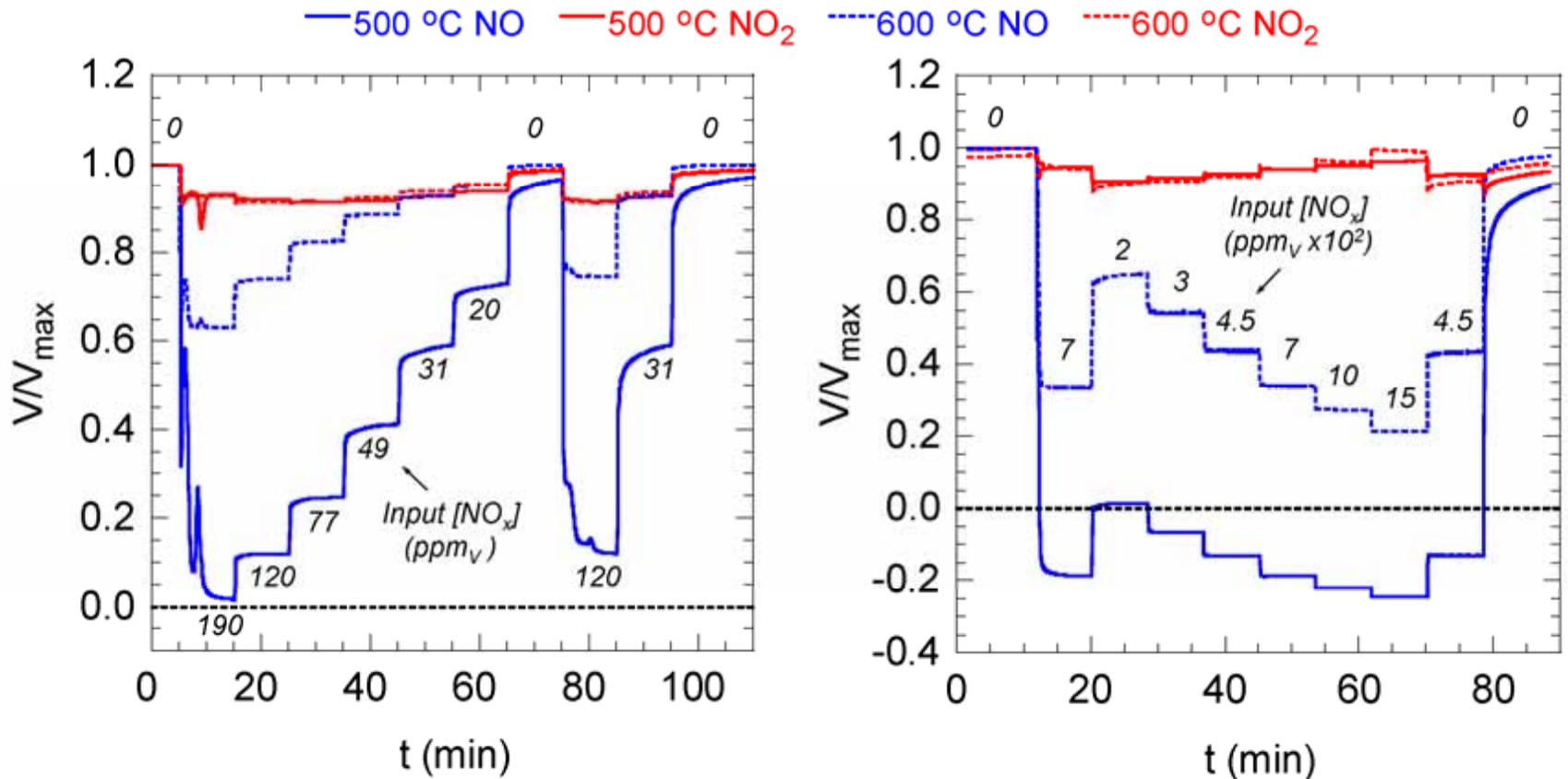


⇒ Data collected at 600 °C, 7 vol% O₂. LSC/Pt, semicircular (SC) geometry.

⇒ "Positive bias": Oxide electrode +, Pt electrode -.

Asymmetry in biased response over wide [NO_x]

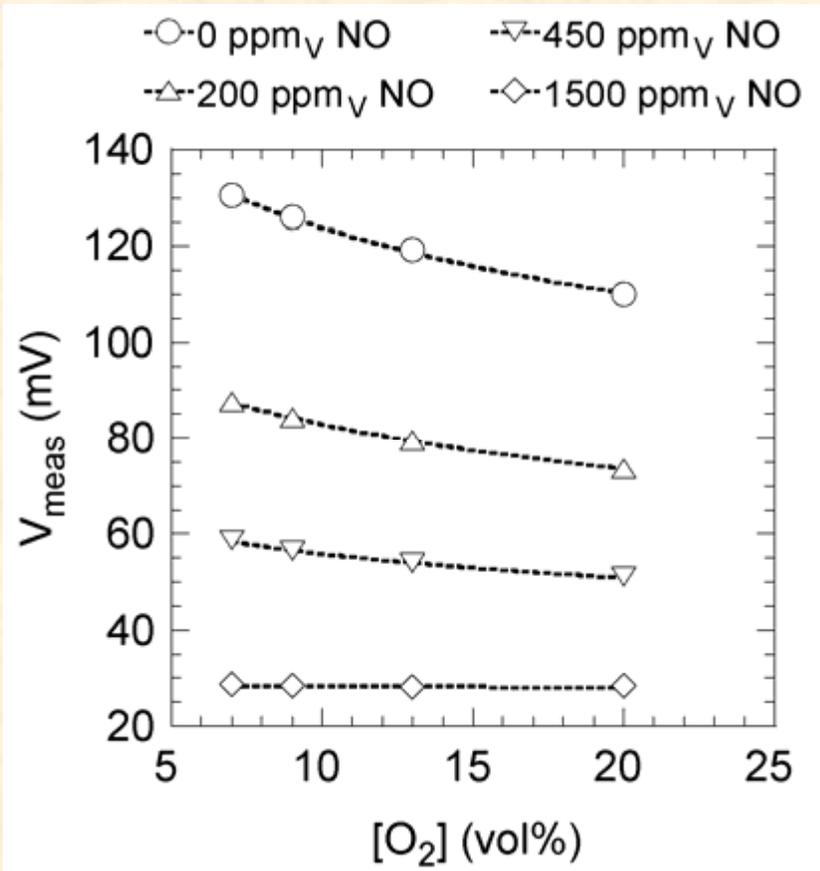
$$V_{\text{meas}} = f(t) \text{ (LSC/Pt SC sensing element, 7 vol\% O}_2\text{)}$$



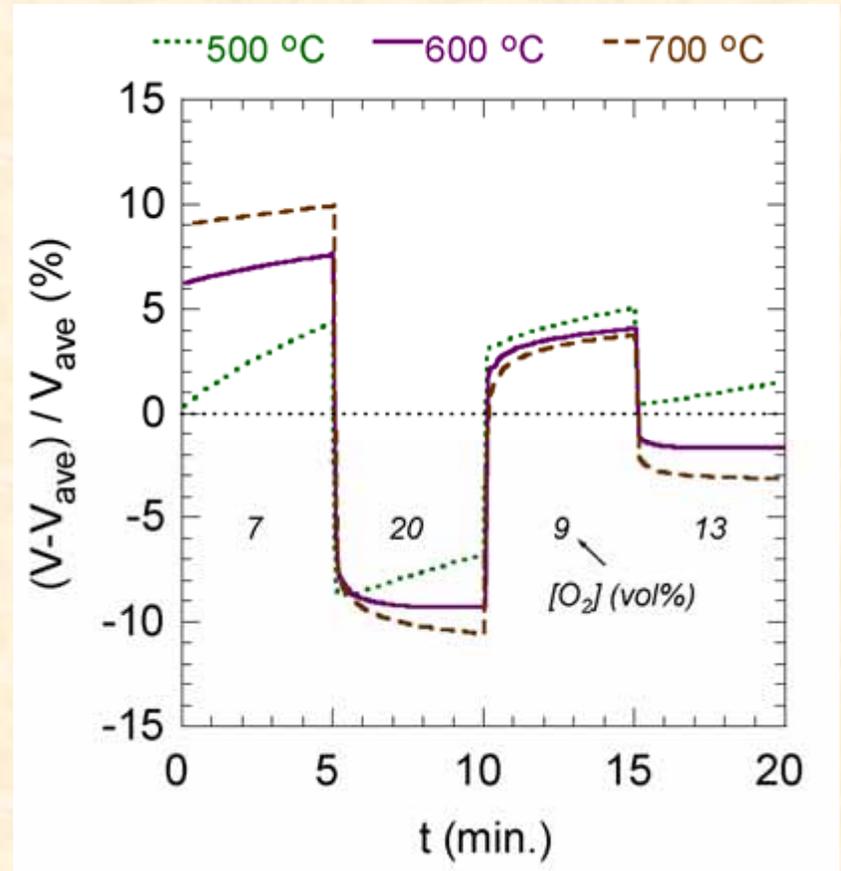
- ⇒ +1.5 (500 °C) and +14 (600 °C) μA biases.
- ⇒ Focus on NO response with biased elements.

Biased: $[O_2]$ dependence a decreasing function of $[NO]$

Varying $[O_2]$ at 600 °C



$V = f(t)$ with 0 [NO]

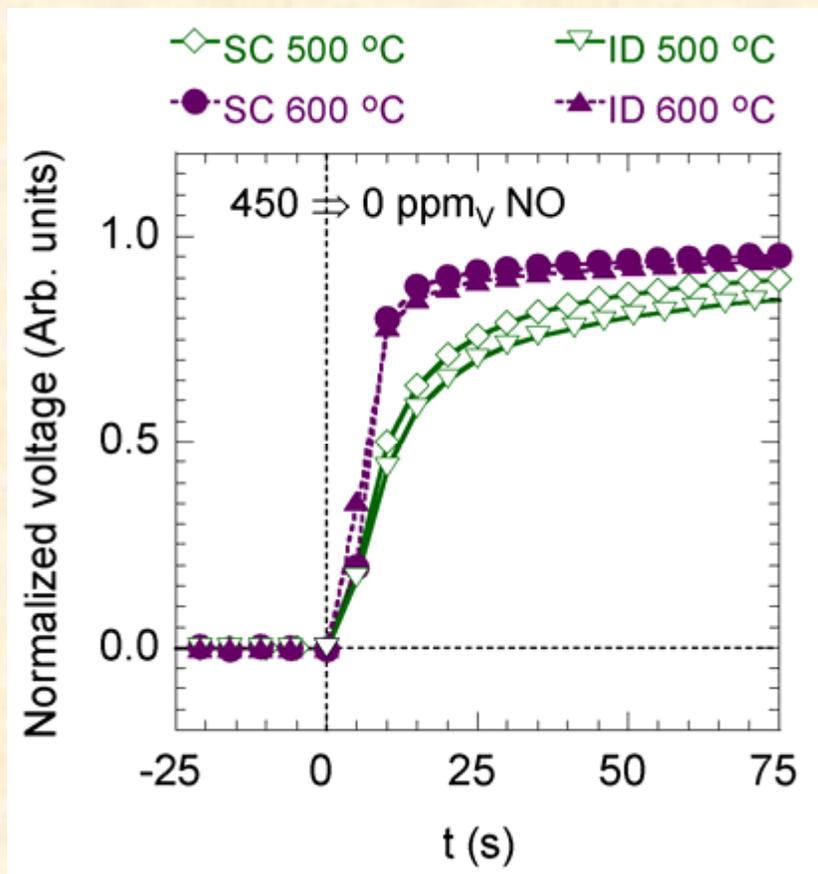
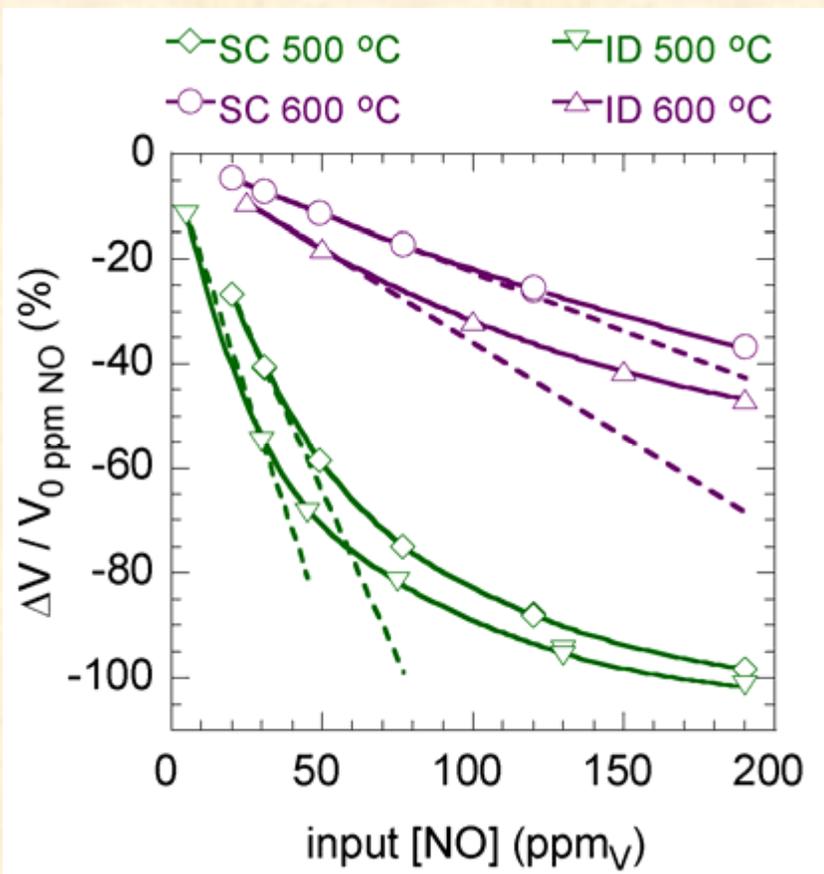


⇒ LSC /Pt semicircular (SC) sensing element. 700 °C bias = 60 μ A.

T still controls response magnitude, recovery time

$$\Delta V = f([\text{NO}])$$

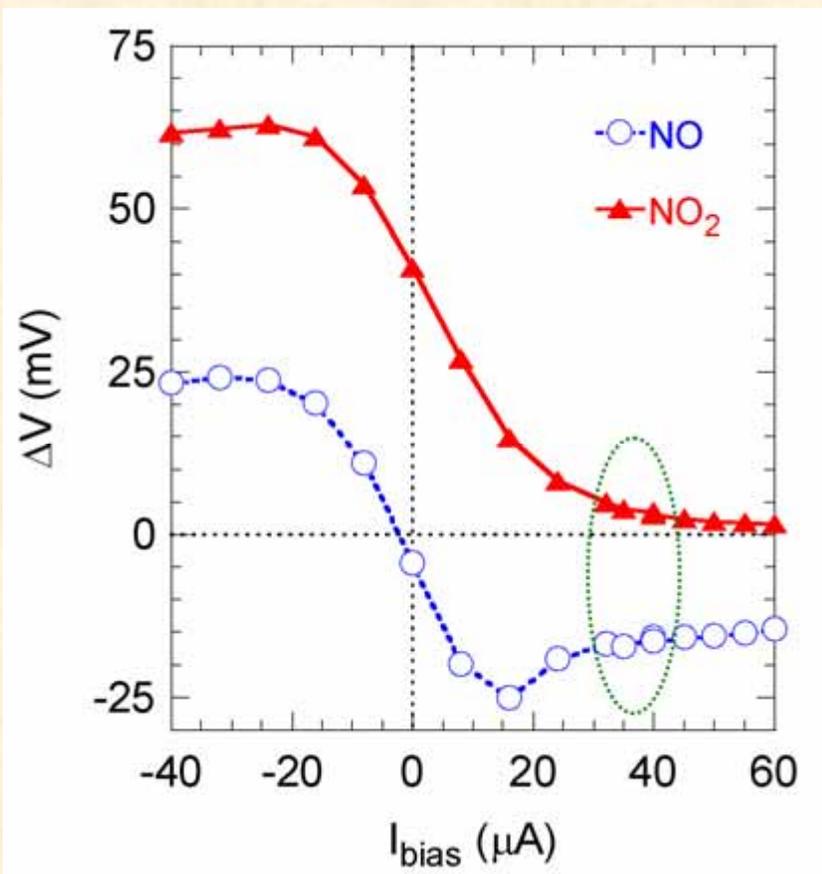
Recovery from 450 ppm_v NO



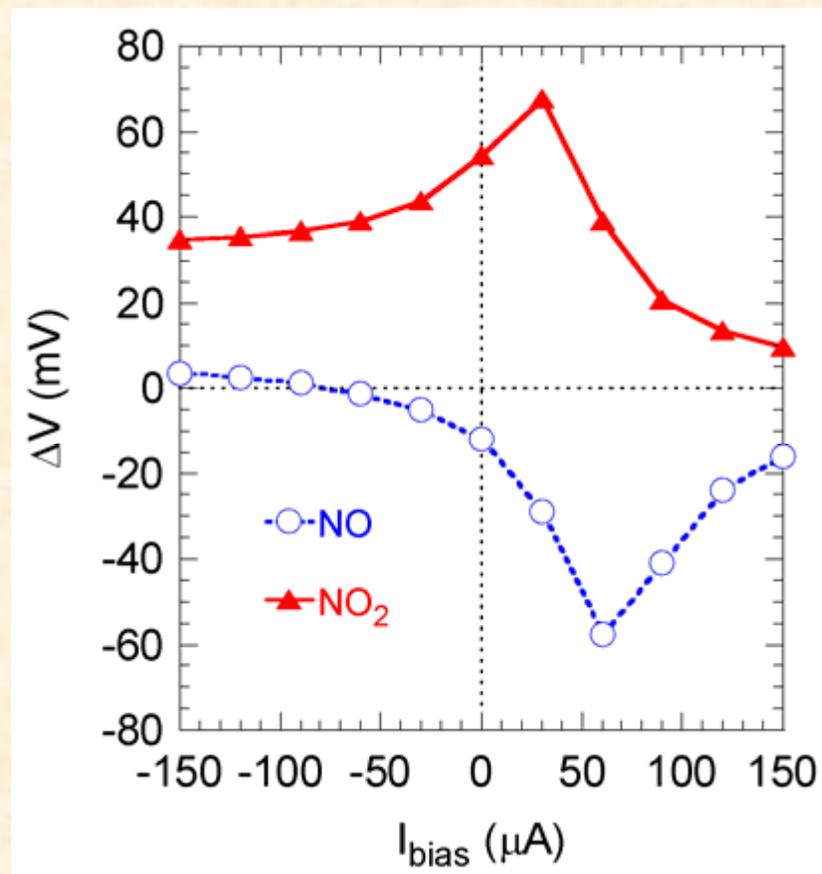
- ⇒ LSC /Pt sensing elements.
- ⇒ Biased to "NO-selective" condition.

Ferrite behaved differently than chromites with bias

$\text{La}_{0.85}\text{Ba}_{0.15}\text{CrO}_3$ (LBC)



$\text{La}_{0.8}\text{Sr}_{0.2}\text{FeO}_3$ (LSF)



- ⇒ Data collected at 600 °C in 7 vol% O_2 .
- ⇒ LSC /Pt semicircular (SC) sensing elements.

Summary and conclusions

⇒ Experimental approach

- ◆ Sensing elements with co-planar electrodes (oxide /Pt).

⇒ Observations

- ◆ Strong NO₂ response without bias.

- ⇒ Response logarithmic 20 – 1500 ppm [NO₂].

- ⇒ Function of [O₂] only in presence of [NO₂].

- ⇒ Magnitude, recovery time decrease with T.

- ◆ Enhanced NO response possible with DC biasing.

- ⇒ Response linear at low [NO].

- ⇒ [O₂] sensitivity inversely proportional to [NO].

- ⇒ Magnitude, recovery time decrease with T.

- ⇒ Not all oxides behave similarly.

⇒ Conclusion and future outlook

- ◆ Use of biasing enables sensing of NO as opposed to NO₂.
- ◆ Characterization of stability and selectivity still required.

Acknowledgements

- ⇒ B. L. Armstrong and C. A. Walls (ORNL).
 - ◆ YSZ substrate fabrication.
 - ◆ Screen printing ink formulation and production.
- ⇒ L. C. Maxey and B. E. Evans (ORNL).
 - ◆ Electronics and automation.
- ⇒ D. Kubinski, R. Soltis, and J. Visser (Ford SRL).
 - ◆ Consultation in mobile power sensing requirements and technologies.

Oak Ridge National Laboratory is operated by UT-Battelle for the
United States Department of Energy under contract
DE-AC05-00OR22725.

Thank you for your attention!