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Scintillation Light Transport and Detection

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Engineering Physics and Mathematics Division

Scintillation Light Transport and Detection*

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Abstract

The MORSE neutron gamma-ray transport code has been modified to allow for the transport of scintillation light. This modified code is used to analyze the light collection characteristics of a large liquid scintillator module ($18 \times 18 \times 350 \text{ cm}^3$).

I. Introduction and Method of Calculation

Efficient collection of scintillation light produced by the energy deposition of a charged particle is important in the overall performance of a scintillator detector system. The detection efficiency is determined by many factors including the geometry of the modular section, the index of refraction of the scintillator material and external material (usually air)* which determines the internal reflection characteristics, the absorption length of scintillation light, the photoelectron conversion efficiency of the phototubes, and the size of the phototubes. The MORSE¹ Monte Carlo code was modified to include all of the above factors so that accurate scintillation light transport could be carried out.

The wavelength distribution of the isotropically distributed scintillation light is shown in the upper graph of Fig. 1. The wavelength distribution was used by employing standard sampling techniques to define the source wavelength for the transport calculation. As implied by the histogram in Fig. 1, the calculation was carried out using 15 scintillation light wavelength groups, each group being 10 nm wide.

The absorption length for all wavelengths of light considered was assumed to be 75, 150, or 225 cm. Three sets of 15-group cross sections (reflecting the above absorption lengths) with no downscatter were generated. During the transport, scintillation light which traveled the sampled flight path before reaching the phototube was assumed to be absorbed and therefore would not contribute to the detector response.

Scintillation photons which reached the sides of the modules were allowed to either escape or undergo specular reflection. Any photon whose angle of incidence was greater than the critical angle was internally reflected. Any photon whose angle of incidence was less than the critical angle was allowed to escape from the system and therefore would not contribute to the detector response.[†] The critical angle is defined from the following expression: $\sin \theta = 1/n$, where θ = angle of photon relative to the normal at the surface and n = the index of refraction of the scintillator material which for these calculations has been taken to be 1.5.

Scintillation photons which are not absorbed or do not leak from the system reach the phototubes (represented by the 2 cylindrical holes in the geometry) and can produce a detectable photoelectron. The probability of this occurring is given by the bottom graph in Fig. 1. Analytically, these data can be represented by the following expression: $\epsilon = 0.26 e^{-5.2 \times 10^{-3}(\lambda - 400)^2}$. Generally speaking, most phototubes are approximately 20-25% efficient, requiring 4 to 5 scintillation gamma rays to produce one photoelectron.

*Generally for liquid scintillator systems, the box, usually lucite, containing the liquid has an index of refraction very similar to that of the scintillator. Internal reflection will then occur at the box/air interface and not at the scintillator/box interface.

[†]Some reflection is possible due to surface irregularity contamination for angles less than the critical angle. However, this effect is neglected in these calculations.

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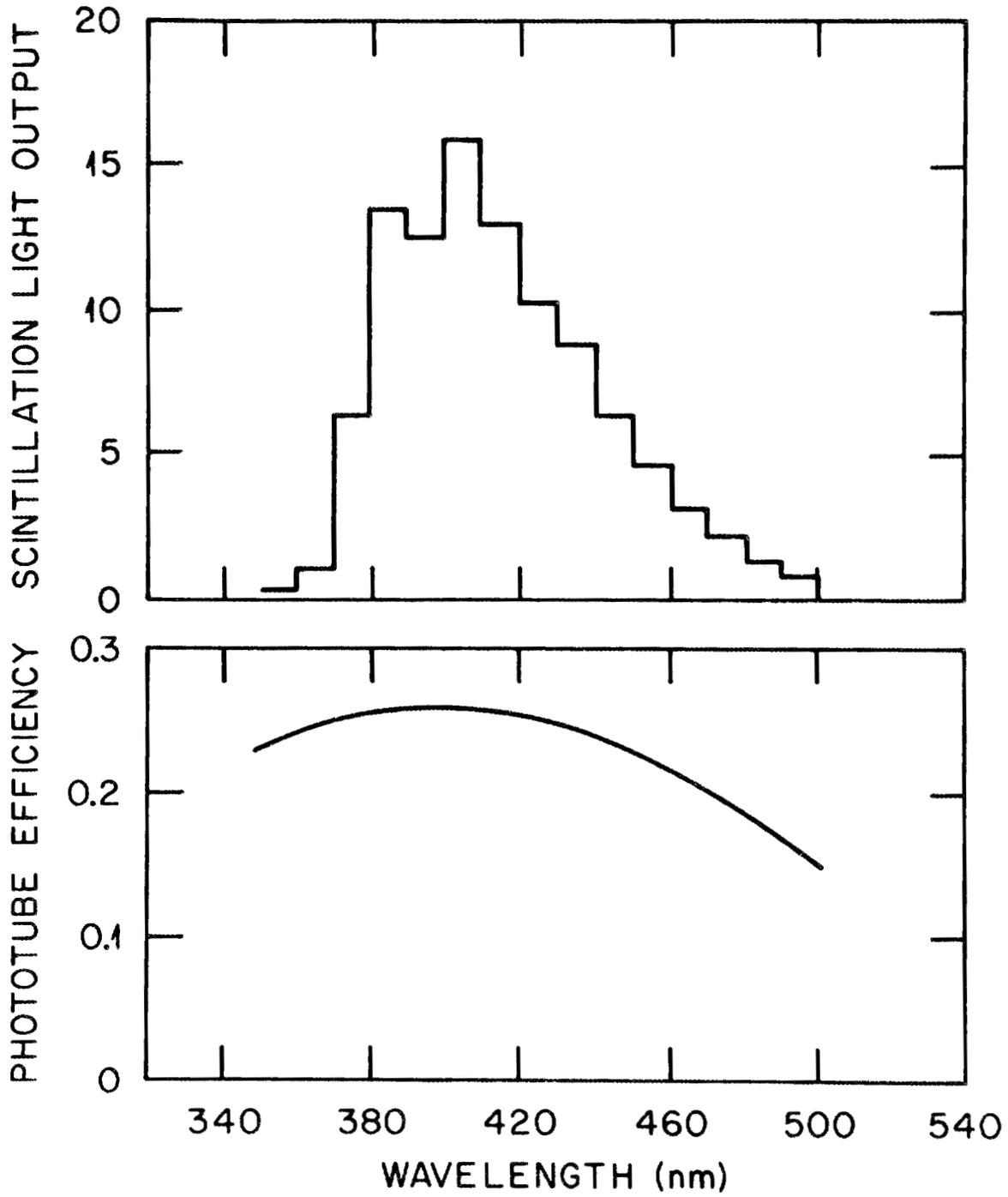


Fig. 1. Scintillation light output and phototube efficiency versus wave length.

No statistical weighting was used in any of these calculations. A source particle which started with a weight of one had a statistical weight of one when or if it finally produced a photoelectron at the phototube. Statistical weighting would have yielded the same average results, but with these calculations analog fluctuations are also necessary if the detector efficiency with respect to light collection is to be properly determined.

The detector module size considered for these calculations is $18.3 \times 18.3 \times 300.3 \text{ cm}^3$ (x, y, z coordinates were chosen such that $0, 0, 0$ represented the center of the module).^{*} The wall thickness of the container is 0.15 cm which yields an active scintillator volume of $18. \times 18. \times 300. \text{ cm}^3$. Attached at each end of the detector is a 7.62 cm diameter phototube. The geometry of the detector module was set up using the combinatorial geometry package in MORSE. The phototubes were represented by a cylindrical hole cut into each end ($z = \pm 150.$) of the module.

II. Results

The number of photoelectrons produced in both phototubes as a function of the number of source scintillation photons and as a function of scintillation photo absorption length is given in Fig. 2. These results are for a source of photons located in the center of the detector module. As can be seen, only a small number of photoelectrons are produced relative to the number of initial scintillation photons. A fit to these curves yields the following expressions:

$$PE = \begin{cases} 1.125 \times 10^{-3} S & \text{for } \lambda = 75 \text{ cm} \\ 4.113 \times 10^{-3} S & \text{for } \lambda = 150 \text{ cm} \\ 6.688 \times 10^{-3} S & \text{for } \lambda = 225 \text{ cm} \end{cases}$$

where S is the number of scintillation photons and PE is the number of produced photoelectrons.

For liquid or plastic scintillator approximately $100\text{-}125 \text{ eV}$ of energy deposition is required to produce one scintillation photon. Therefore, 4000 photons correspond to $0.4\text{-}0.5 \text{ MeV}$ in energy deposition. Figure 2 defines the energy normalization for the detector module. Over the range covered by these calculations, the response is very linear with respect to energy deposition.

The energy resolution of the detector module was determined not by the average number of photoelectrons produced, but by the fluctuations in the number produced. An example of these fluctuations is illustrated in Fig. 3 for 2000 source scintillation photons located in the center of the module. The solid curve was obtained directly from the calculated data and the dashed curve was obtained from a Gaussian ($\alpha e^{-(x-x_0)^2/2\sigma^2}$) fit to the data. The data are very well fitted by a Gaussian curve. The fluctuation as measured by the standard deviation σ as a function of scintillation gammas is given in Fig. 4. As

^{*}This detector module is being constructed for use at the KfK/SNS neutrino experiment.

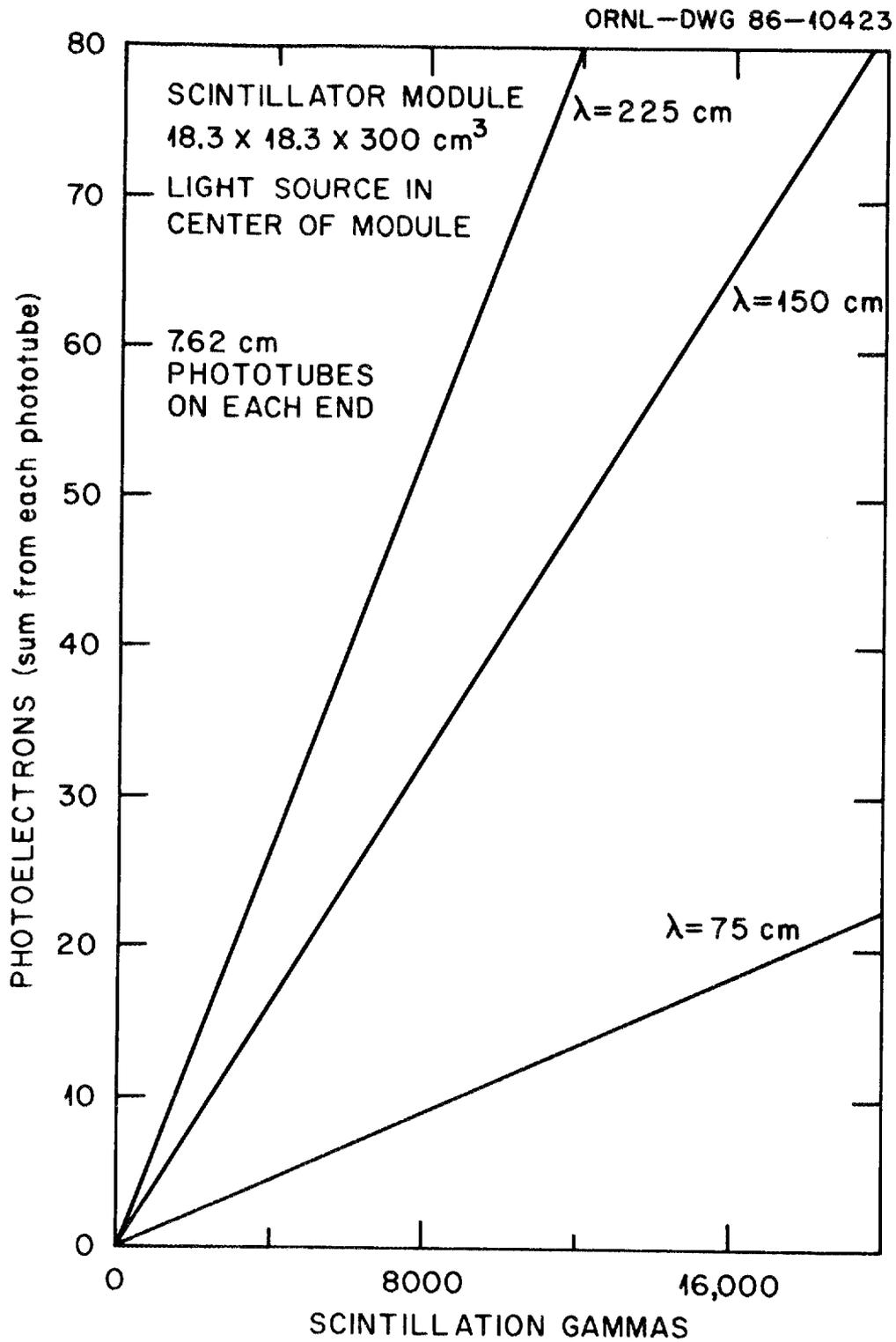


Fig. 2. The number of photoelectrons produced versus the number of source scintillation photons.

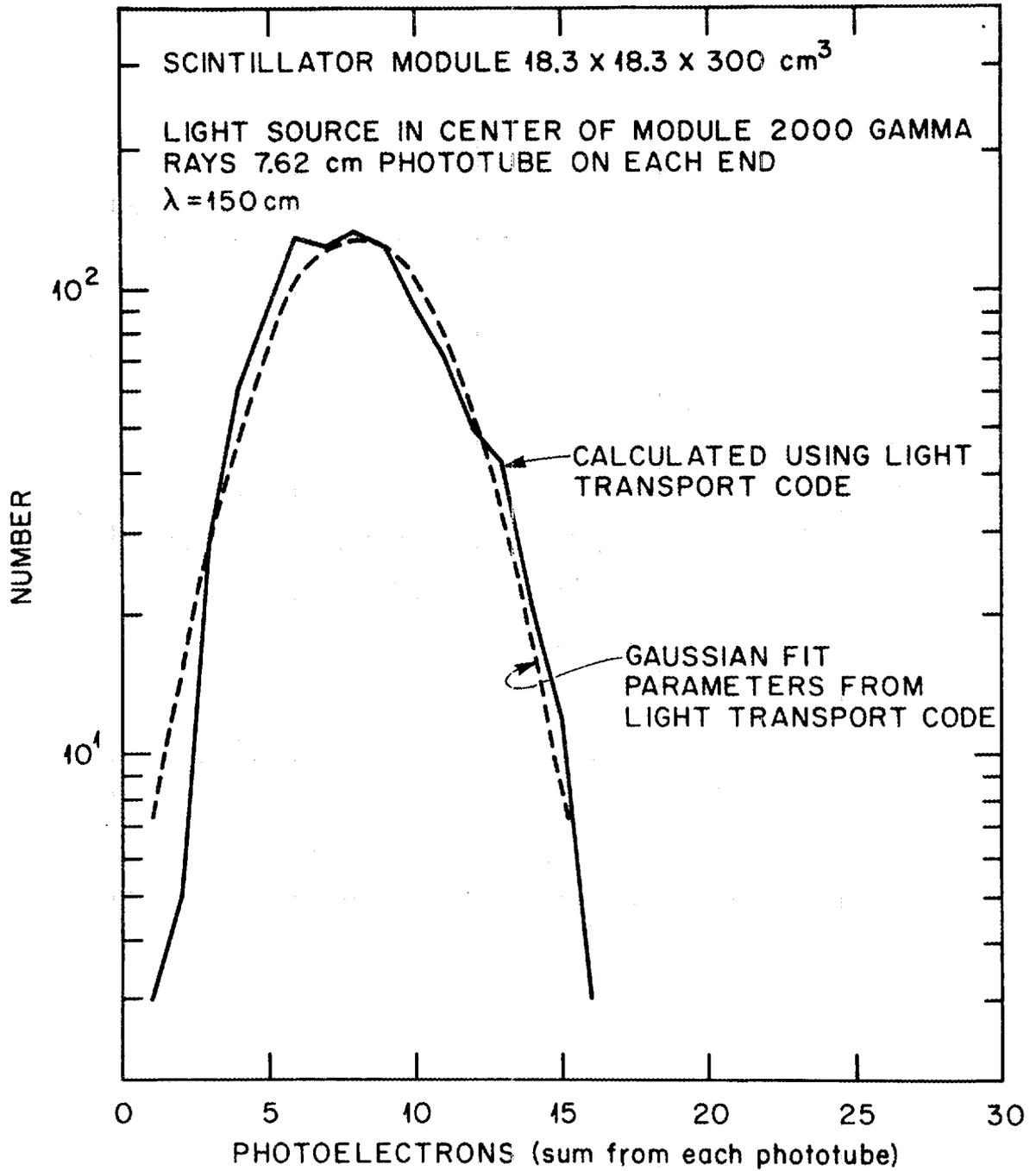


Fig. 3. Comparison between calculated fluctuation data and a Gaussian fit to these data.

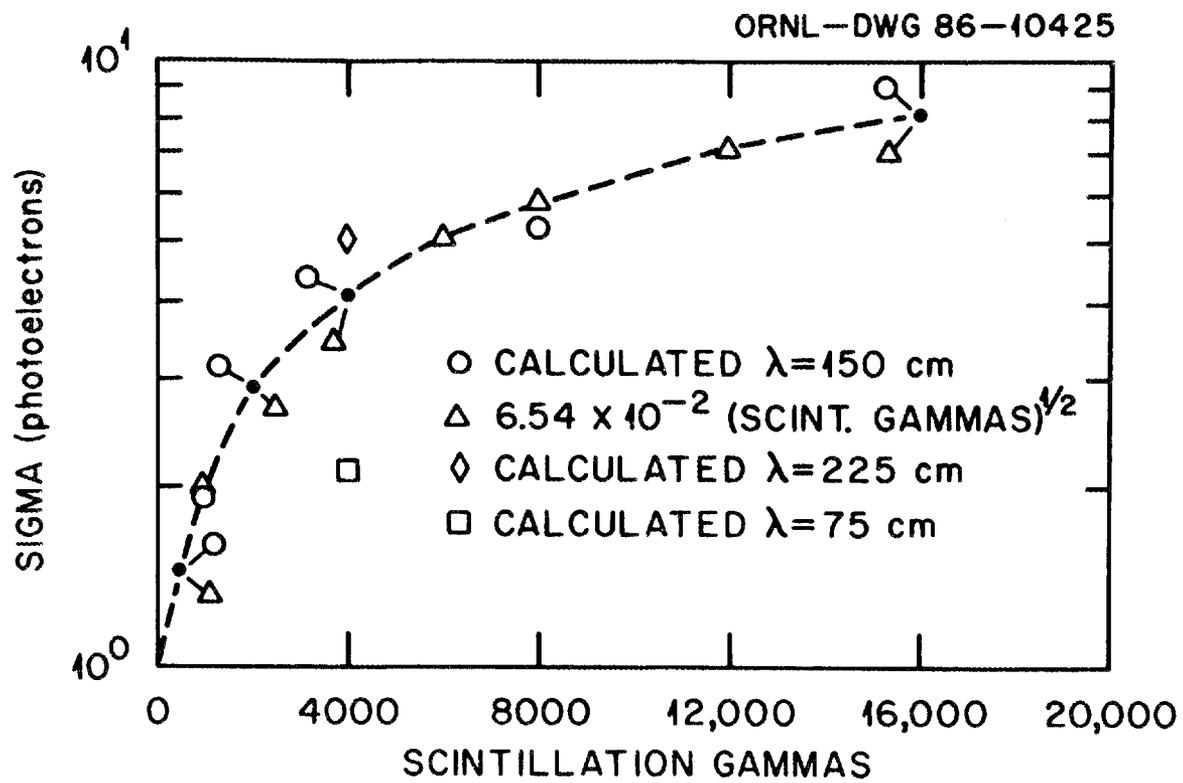


Fig. 4. Standard deviation in the number of photoelectrons produced versus the number of scintillation photons.

one would expect from statistical theory, the curve in Fig. 4 is proportional to the square root of the number of photons. A best fit to the data yields the following expression: $\sigma = 6.54 \times 10^{-2} S^{1/2}$ for $\lambda = 150$ cm and S is the number of scintillation photons. Data points for $\lambda = 75$ and 225 cm are also given. However, by using the data in Fig. 2, the data for $\lambda = 150$ cm can be used to obtain σ 's for $\lambda = 75$ and 225 cm. For example, 4000 photons for $\lambda = 75$ cm correspond to approximately 1200 photons for the $\lambda = 150$ -cm case relative to the number of photoelectrons produced. Comparing these values in Fig. 4 yields the same σ .

The data presented so far have been for an isotopic source located in the center of the module. The spatial variation of the average number of photoelectrons detected as a function of distance from the center of the detector module toward one of the phototubes is given in Fig. 5. The coordinates (x,y) remain on axis. A strong variation in the average number is evident for all absorption lengths especially as the edge of the module is approached. Ideally, these curves should be as flat as possible. By using timing differences between the two phototubes to locate the energy deposition site and the above curves, the spatial variation of light collection as it influences energy resolution can be partially minimized.

Calculations have also been carried out to determine the variation in signal when the source is moved along the x-axis and the y and z coordinates are fixed. This variation in source location leads to very small changes, except at the very edge of the active scintillator region and should not lead to any serious resolution degradation. Fluctuations in the data presented in Fig. 5 can be obtained from the the data given in Figs. 2 and 4. Similar data are presented in Fig. 6 as were given in Fig. 5 except that only one phototube has been considered.

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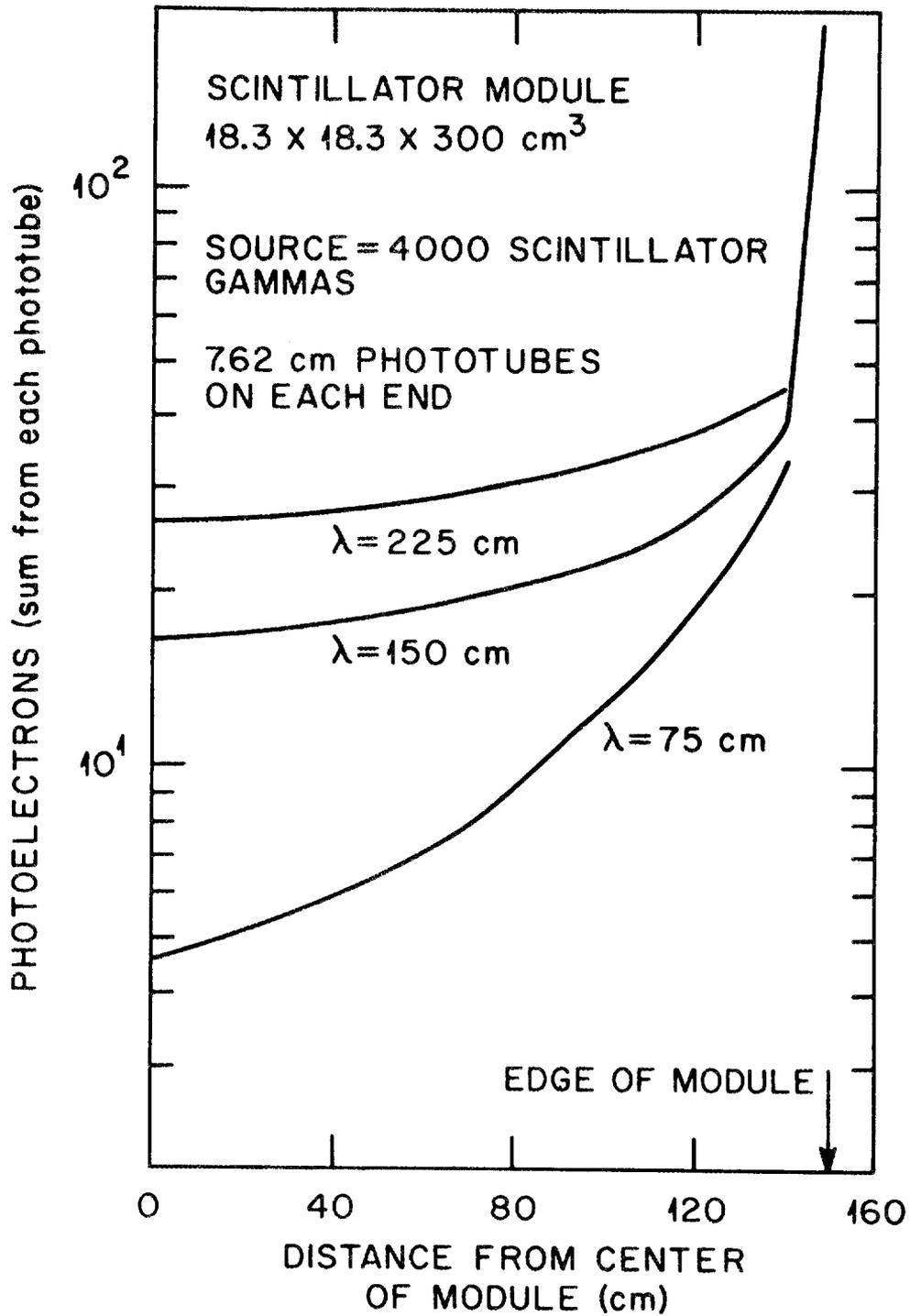


Fig. 5. Spatial variation in the number of photoelectrons produced as a function of distance from the center of the module.

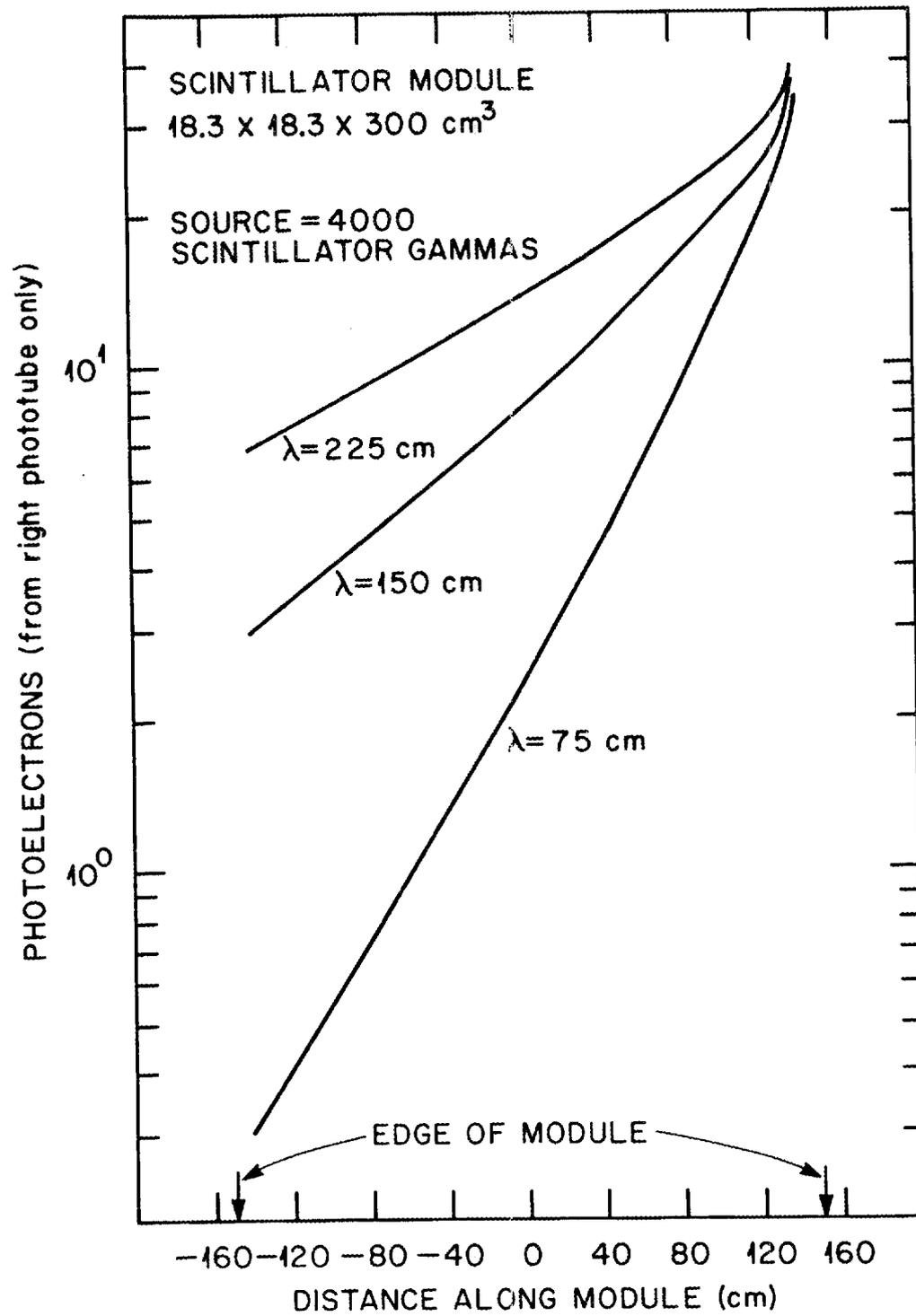


Fig. 6. Spatial variation in the number of photoelectrons produced in one phototube only as a function of distance from the center of the module.

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