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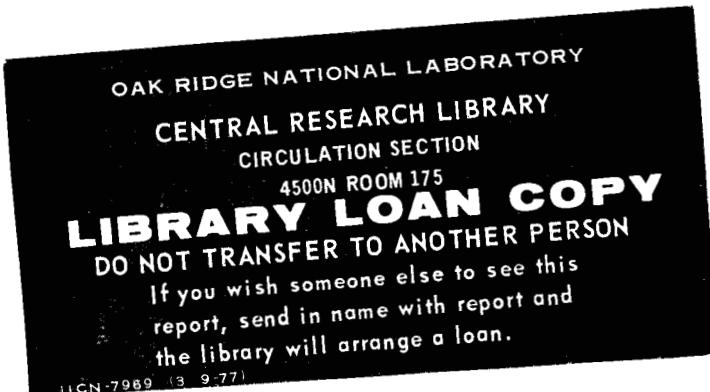


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ORNL/TM-7176/R1

LMFBR Models for the ORIGEN2 Computer Code

A. G. Croff
J. W. McAdoo
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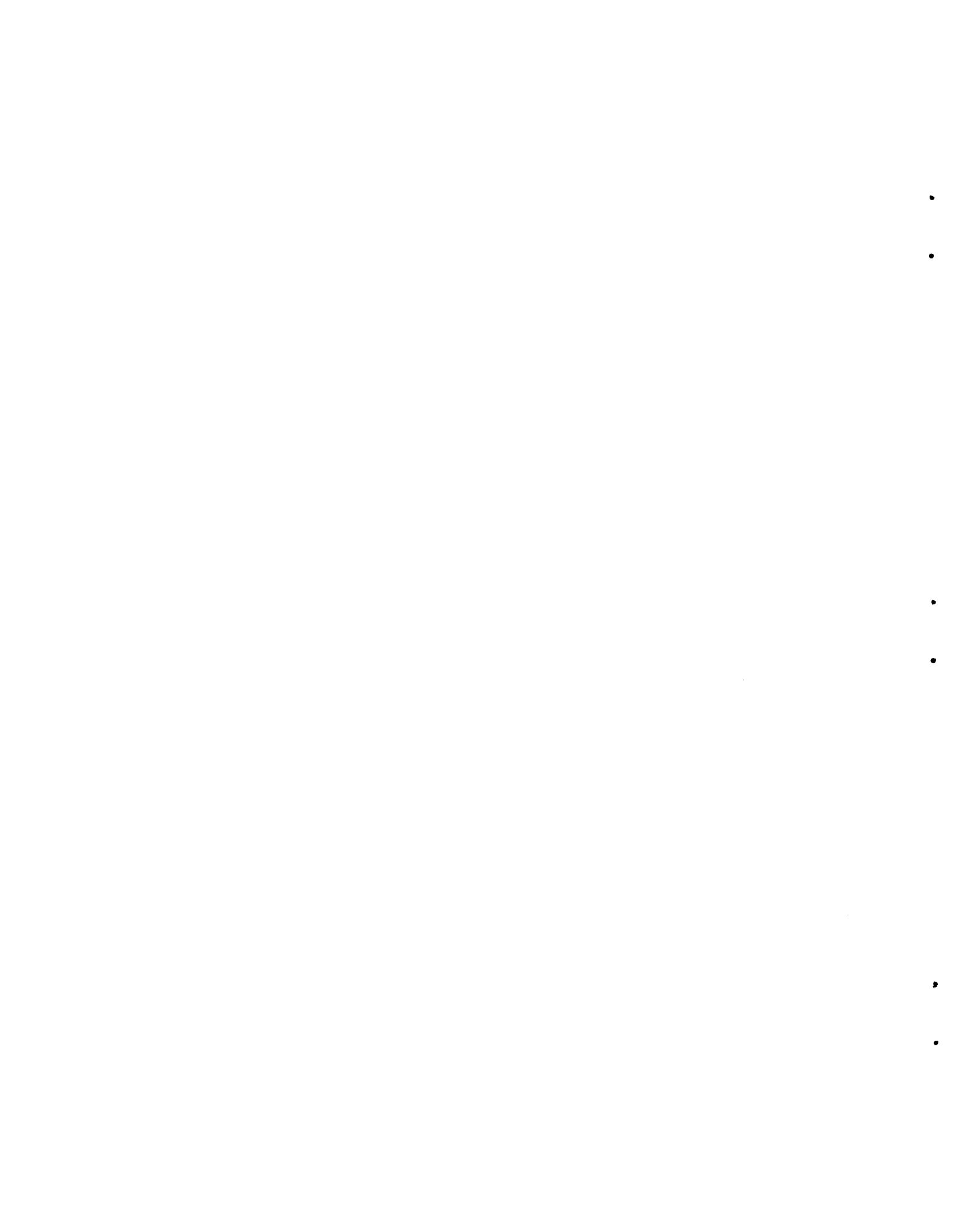
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GLOSSARY

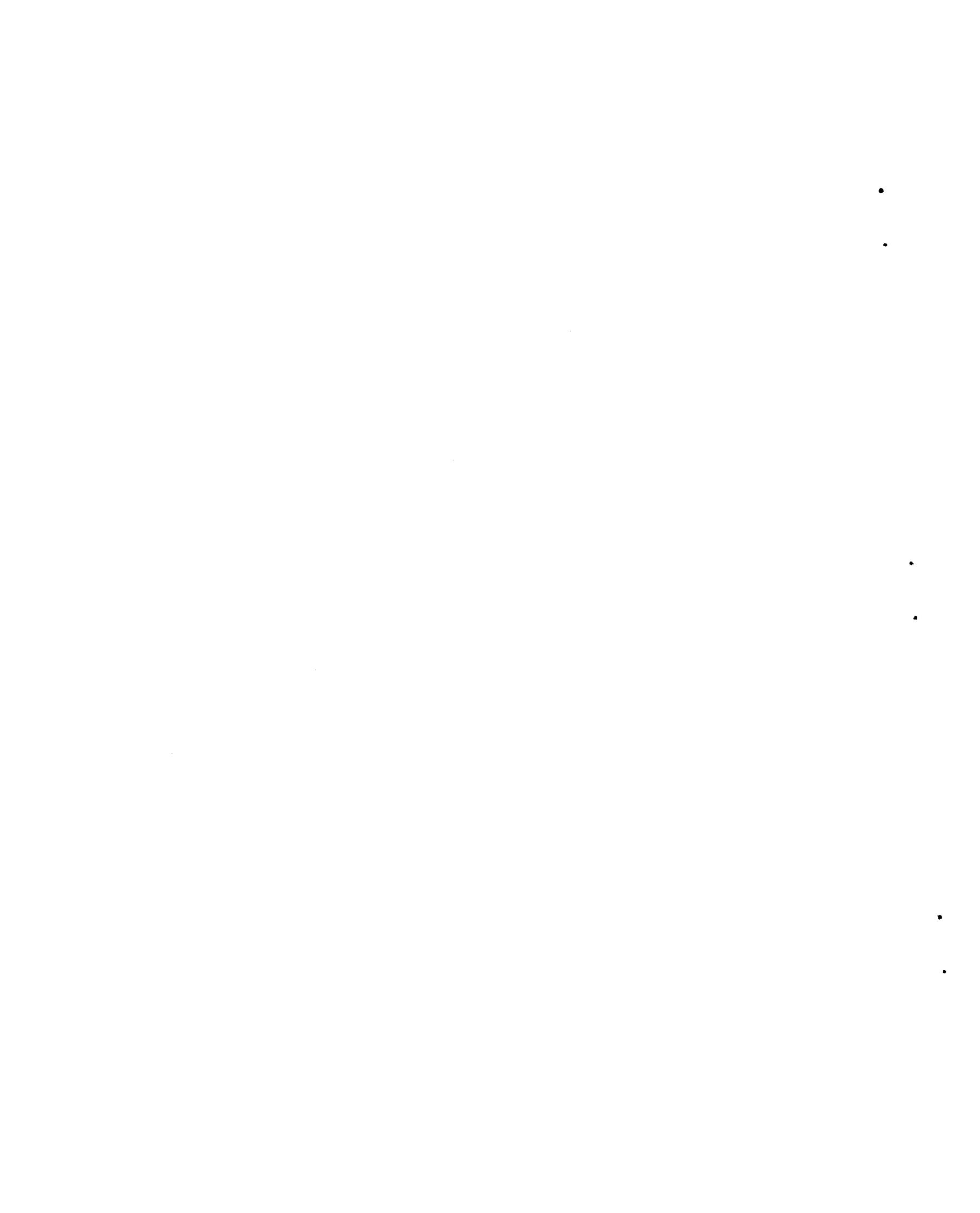
GWd	Gigawatt-days = 10^9 watt-days
MWd	Megawatt-days = 10^6 watt-days
MTIHM	Metric tons (10^6 g) of initial heavy metal
Depletion calculation	Calculation of the fresh reactor fuel irradiation that predicts the discharged fuel composition
Fuel element	The smallest structurally discrete part of a fuel assembly that has nuclear fuel as the principal constituent; also called a fuel pin or a fuel rod
Fuel assembly	A grouping of fuel elements that remains intact during the charging and discharging of a reactor core
Pin cell	A cylindrical model of a fuel element used in a reactor physics calculation
Assembly cell	A cylindrical model of a fuel assembly used in a reactor physics calculation
Fuel channel	Hexagonal, sheet-metal can surrounding each fuel assembly to prevent cross-flow of coolant between assemblies
LMFBR	Liquid metal (cooled), fast-breeder reactor. "Fast" refers to the fact that the neutron spectrum is high-energy, i.e., not thermal.
FFTF	Fast-Flux Test Facility in Richland, Washington



PREFACE

This revision is being issued to correct a significant error that occurred in generating the cross sections for the ORIGEN2 LMFBR reactor models described in the original report. Specifically, the weighting of the multigroup cross section library with a multigroup neutron energy spectrum to yield a one-group cross-section library was done improperly because the nuclide concentrations were not correct. This error was propagated throughout much of the data presented in the appendixes, thus necessitating a completely new version of this portion of the report. In addition, some minor changes have been made based on information obtained after the original report had been issued. The most notable of these are: (1) the FFTF irradiation parameters have been updated; (2) Table B.1, in which the values in the first column were shifted, has been corrected; and (3) an error in the specific power for the radial blanket in the AMORUUUX and EMOPUUUX reactor models has been eliminated.

The impact of these changes on the principal actinide nuclides (e.g., uranium, plutonium) is negligible since they are dependent on variable cross sections which were not affected by the multigroup cross-section processing errors. However, the changes in the one-group cross sections will affect virtually all other nuclides to varying degrees. It should be noted that the cross-section processing errors described above do not affect the FFTF model in this report or the CRBRP model described in NUREG/CR-2762.



LMFBR MODELS FOR THE ORIGEN2 COMPUTER CODE

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ABSTRACT

Reactor physics calculations have led to the development of nine liquid-metal fast breeder reactor (LMFBR) models for the ORIGEN2 computer code. Four of the models are based on the U-Pu fuel cycle, two are based on the Th-U-Pu fuel cycle, and three are based on the Th- ^{233}U fuel cycle. The reactor models are based on cross sections taken directly from the reactor physics codes. Descriptions of the reactor models as well as values for the ORIGEN2 flux parameters THERM, RES, and FAST are given.

1. INTRODUCTION AND SUMMARY

1.1 Introduction

1.1.1 Background

The ORIGEN¹ computer code is a versatile tool used for calculating the buildup and depletion of isotopes in nuclear materials. This computer code was written in the late 1960s and early 1970s by the ORNL Chemical Technology Division. At that time, the required nuclear data libraries (half-lives, cross sections, fission product yields, etc.) and reactor models (PWR-U, PWR-Pu, LMFBR, HTGR, and MSBR) were also developed. The code was principally intended for use in generating spent fuel and waste characteristics (composition, thermal power, etc.) that would form the basis for the study and design of fuel reprocessing plants, spent fuel shipping casks, waste treatment and disposal facilities, and waste shipping casks. Since fuel cycle operations were being examined generically in order to accommodate a wide range of fuel

characteristics, it was only necessary that the ORIGEN results be representative of this range. A satisfactory result was obtained by simply adjusting the resonance integrals of the major fissile and fertile species to obtain agreement with a spent fuel composition from an exogenous source.

Soon after the ORIGEN computer code was documented, it was made available to other users through the Radiation Shielding Information Center at ORNL. Because of the relative simplicity of ORIGEN and its convenient and detailed output, many organizations acquired it; some began using ORIGEN for applications that were more specific and that required greater precision in the calculated results than the generic fuel cycle studies for which the code was originally developed. (For example, environmental impact studies required relatively precise calculations of minor isotopes such as ^3H , ^{14}C , ^{232}U , and $^{242,244}\text{Cm}$.) In response to these requirements, attempts were made to update specific aspects of ORIGEN and its data bases;^{2,3} however, inconsistencies and numerous data bases resulted from these efforts.

To remedy these problems, a concerted program was initiated in 1975 to update the ORIGEN computer code and its associated data bases and reactor models. This is one of several reports describing the various aspects of the ORIGEN update effort. Previously issued reports describe (1) a revised version of the ORIGEN computer code,^{4,5} designated ORIGEN2, (2) updated decay and photon data libraries,⁶ (3) updated U-Pu cycle PWR and BWR models,⁷ and (4) alternative-fuel-cycle (thorium cycles and extended burnup) PWR models,⁸ and CANDU reactor models.⁹

1.1.2 Scope

This report describes nine model LMFBRs. Eight of these are commercial designs based on the Prototype Large Breeder Reactor study¹⁰ and the ninth is based on the currently operating FFTF reactor¹¹ in the Richland, Washington area. A characteristic description of the fuel cycles considered in these reactor models is given in Table 1.

Table 1. Fuel cycles considered for ORIGEN2 LMFBR models

Core fissile material	Fertile material			Core burnup (Gwd/MTHM)	MNEMONIC
	Core	Axial blanket	Radial blanket		
LWR PuO ₂	UO ₂	UO ₂	UO ₂	100	AMOPUUUX
LWR PuO ₂	UO ₂	UO ₂	UO ₂	68	EMOPUUUX
Recycle PuO ₂	UO ₂	UO ₂	UO ₂	100	AMORUUUX
LWR PuO ₂	UO ₂	UO ₂	ThO ₂	100	AMOPUUTX
LWR PuO ₂	ThO ₂	ThO ₂	ThO ₂	100	AMOPTTTX
Recycle ²³³ UO ₂	ThO ₂	ThO ₂	ThO ₂	100	AMOOTTTX
14% denatured ²³³ UO ₂	ThO ₂	ThO ₂	ThO ₂	100	AMO1TTTX
40% denatured ²³³ UO ₂	ThO ₂	ThO ₂	ThO ₂	100	AMO2TTTX
High-grade Pu	UO ₂			45	FFTF

The fundamental objective of this work was to develop LMFBR models based on existing cross section data^{12,13} rather than the arbitrary adjustment of cross sections that typified previous ORIGEN reactor models. The generation of the information required for these reactor models began with the gathering and initial processing of the existing cross section data into a library of 126 neutron energy groups that could be used by a modular system of reactor physics codes (AMPX)¹⁴ at ORNL (Sect. 2). Two separate libraries were created: (1) a smaller one containing nuclides whose presence in the reactor would have the greatest effects on the neutron spectrum and depletion characteristics, and (2) a larger library containing many nuclides of interest in ORIGEN2 with negligible effects on the neutron spectrum and depletion. Only the smaller library was considered in the subsequent multigroup fuel-depletion calculations.

Following these initial steps, composition-dependent cross sections that accounted for spatial and energy self-shielding effects were generated for each of the commercial reactors (Sect. 3). The libraries resulting from this procedure contained nine neutron energy groups, which were then used in a diffusion-theory depletion code to predict the spent fuel composition and to supply some of the cross sections required by ORIGEN2. The 126-group cross sections were then collapsed to 1-group cross sections, using a typical neutron spectrum that was derived from the depletion calculation. Fission product yields were obtained by spectrum-weighting energy-dependent yields, using this same neutron spectrum. Additional calculations were then performed that yielded new values of the ORIGEN2 flux parameters — THERM, RES, AND FAST.

Finally, an investigation was undertaken to determine appropriate input parameters for the reactor models. The parameters investigated included the actinide and impurity composition of the fresh fuel and the structural material type and composition of a fuel assembly.

2. THE GENERATION OF THE MASTER, MULTIGROUP CROSS-SECTION DATA BASE

This section describes the sources of the unprocessed cross-section data used to develop the LMFBR models and the initial processing of these cross sections into an AMPX master cross-section library. The 126-energy-group library structure (of which two groups were in the thermal energy range) is shown in Appendix A.

Cross sections that were used for the ORIGEN2 LMFBR models were collected into two groups. Group 1 contains all fission product isotopes having cross-section data available for processing. Data for the group 1 nuclides (listed in Table 2) were obtained from ENDF/B-IV and are documented in ref. 15. These data were processed with the AMPX modules NPTXS and XLACS2.

Nuclides in group 2, initially divided into subgroups 2A and 2B, include the activation products, actinides, coolant, and structural materials considered in this work. Subgroup 2A consists of nuclides that are important in the reactor physics calculations. Most of the cross-section data for subgroup 2A was derived from ENDF/B-IV¹² and its processing^{16,17} was accomplished with the MINX¹⁸ computer code. Data for a few of the nuclides in this subgroup were obtained from a preliminary version of ENDF/B-V¹³ and were processed into the master, multigroup format using the AMPX modules NPTXS and XLACS2 (or, in the case of ²³³U, the NJOY¹⁹ computer code). Data for the nuclides in subgroup 2A, which are summarized in Table 3, were used through the entire sequence of fuel depletion calculations.

Subgroup 2B contains nuclides for which data were obtained from ENDF/B-IV, through the processing sequence defined in refs. 16 and 17. Data for these nuclides (which include the light nuclides, such as ¹H, and the minor actinides, such as ²³³Pa) were not used in the physics calculations for the LMFBR models, but were intended for subsequent weighting with a representative spectrum. However, during the course of this study the more complete cross-section data from ENDF/B-V became available, superseding the ENDF/B-IV data. As a result, multigroup cross-section data were calculated for all of the individual nuclides

Table 2. ORIGEN2 group 1 (fission-product) nuclides^a

72Ge	73Ge	74Ge	75As	76Ge	76Se	77Se	78Se
79Br	80Se	80Kr	81Br	82Se	82Kr	83Kr	84Kr
85Kr	85Rb	86Kr	86Rb	86Sr	87Rb	87Sr	88Sr
89Sr	89Y	90Sr	90Y	90Zr	91Y	91Zr	92Zr
93Zr	93Nb	94Zr	94Nb	94Mo	95Zr	95Nb	95Mo
96Zr	96Mo	97Mo	98Mo	99Mo	99Tc	99Ru	100Mo
100Ru	101Ru	102Ru	103Ru	103Rh	104Ru	104Pd	105Ru
105Rh	105Pd	106Ru	106Pd	107Pd	107Ag	108Pd	108Cd
109Ag	110Pd	110Cd	111Ag	111Cd	112Cd	113Cd	113In
114Cd	115mCd	115In	115Sn	116Cd	116Sn	117Sn	118Sn
119Sn	120Sn	121Sb	122Sn	122Te	123Sn	123Sb	123Te
124Sn	124Sb	124Te	125Sn	125Sb	125Te	126Sn	126Sb
126Te	127mTe	127I	128Te	128Xe	129mTe	129I	129Xe
130Te	130I	130Xe	131I	131Xe	132Te	132Xe	133Xe
133Cs	134Xe	134Cs	134Ba	135I	135Xe	135Cs	135Ba
136Xe	136Cs	136Ba	137Cs	137Ba	138Ba	139La	140Ba
140La	140Ce	141Ce	141Pr	142Ce	142Pr	142Nd	143Ce
143Pr	143Nd	144Ce	144Nd	145Nd	146Nd	147Nd	147Pm
147Sm	148Nd	148Pm	148mPm	148Sm	149Pm	149Sm	150Nd
150Sm	151Pm	151Sm	151Eu	152Sm	152Eu	153Sm	153Eu
154Sm	154Eu	154Gd	155Eu	155Gd	156Eu	156Gd	157Eu
157Gd	158Gd	159Tb	160Gd	160Tb	160Dy	161Dy	162Dy
163Dy	164Dy	165Ho	166Er	167Er			

^aAll cross sections are taken from ref. 12 and documented in
ref. 15.

Table 3. ORIGEN2 subgroup 2A nuclides (included in reactor physics calculations)

Nuclide	Ref. Nos.	Nuclide	Ref. Nos.
^{160}O	12, 16, 17	^{238}Np	13
Na	12, 16, 17	^{238}Pu	12, 16, 17
Stainless steel	12, 16, 17	^{239}Pu	12, 16, 17
Control rod	12, 16, 17	^{240}Pu	12, 16, 17
Lumped fission product	12, 16, 17	^{241}Pu	12, 16, 17
^{232}Th	12, 16, 17	^{242}Pu	12, 16, 17
^{233}Pa	12, 16, 17	^{241}Am	13
^{233}U	13	^{242}Am	13
^{234}U	12, 16, 17	^{242m}Am	13
^{235}U	12, 16, 17	^{243}Am	13
^{236}U	12, 16, 17	^{242}Cm	13
^{238}U	12, 16, 17	^{243}Cm	13
^{237}Np	12, 16, 17	^{244}Cm	13

in group 2, and for some additional actinides, using ENDF/B-V as the data source. Cross sections for this new grouping of nuclides (designated as group 3 and listed in Table 4) were introduced into the sequence of reactor physics codes after the depletion calculation had been performed using the ENDF/B-IV cross sections. The collapse of these cross sections to 1-group values is discussed further in Sect. 3.1.4.

3. MULTIGROUP NEUTRON SPECTRUM AND DEPLETION CALCULATIONS

The 126-energy-group AMPX master cross-section library, described in Sect. 2 of this report, contains cross-section information of a general nature for solving LMFBR neutronics problems. This section describes the processing of this general multigroup library into problem-dependent, multigroup libraries used in the sophisticated reactor physics codes and then into a problem-dependent, 1-group library for use in ORIGEN2. Section 3.1 describes the approach used for the eight commercial LMFBR models, and Sect. 3.2 describes the somewhat simplified procedure used for the FFTF.

3.1 Spectrum and Depletion Calculations for ORIGEN2 Commercial LMFBR Models

3.1.1 Energy self-shielding

The first step in the sequence of calculations leading to the desired ORIGEN2 cross-section library is to account for the energy self-shielding effects in the resonances of various nuclides. In effect, the master library is transformed into a 126-energy group problem-dependent library via the BONAMI module of the AMPX system. This module accesses problem-independent master cross-section data that contain Bondarenko factors (from MINX), performs a resonance self-shielding calculation based on the iterative Bondarenko method,²⁰ and produces problem-dependent master cross-section data. A BONAMI calculation is performed for each of the five zones (i.e., inner core, outer core, inner axial blanket, outer axial blanket, and radial blanket) in each of the eight commercial LMFBR models considered in this work. The input to this calculation includes a simplified system geometry and approximate composition for each zone.

Table 4. ORIGEN2 group 3 nuclides (non-fission-product
and ENDF/B-V Nuclides)^a

¹ H	²³⁴ U	^{242m} Am
¹⁰ B	²³⁵ U	²⁴³ Am
¹¹ B	²³⁶ U	²⁴¹ Cm
¹² C	²³⁷ U	²⁴² Cm
¹⁴ N	²³⁸ U	²⁴³ Cm
¹⁵ N	²³⁷ Np	²⁴⁴ Cm
¹⁶ O	²³⁸ Np	²⁴⁵ Cm
¹⁷ O	²³⁶ Pu	²⁴⁶ Cm
²³ Na	²³⁸ Pu	²⁴⁷ Cm
⁵⁵ Mn	²³⁹ Pu	²⁴⁸ Cm
⁵⁹ Co	²⁴⁰ Pu	²⁴⁹ Bk
²³⁰ Th	²⁴¹ Pu	²⁴⁹ Cf
²³² Th	²⁴² Pu	²⁵⁰ Cf
²³¹ Pa	²⁴³ Pu	²⁵¹ Cf
²³³ Pa	²⁴⁴ Pu	²⁵² Cf
²³² U	²⁴¹ Am	²⁵³ Cf
²³³ U	²⁴² Am	²⁵³ Es

^aAll data from ref. 13.

3.1.2 Spatial self-shielding and collapse to a few groups

The five 126-energy-group, problem-dependent libraries from the BONAMI code are then employed in one-dimensional calculations using the XSDRNPM module of the AMPX system. The purpose of this calculation is (1) to account for the spatial self-shielding effects in each of the zones and (2) to collapse the cross-section library from 126 energy groups to a 9-energy-group structure that will be used in subsequent depletion calculations. Three XSDRNPM calculations are required: one in the radial direction along the core midplane and two in the axial direction (one for the inner core/axial blanket and one for the outer core/axial blanket). The radial calculation is performed using cylindrical geometry with outer radii as follows: inner core, 101.6 cm; outer core, 142.0 cm; radial blanket, 180.6 cm; radial shield, 195.0 cm. The axial calculations are performed using slab geometry with distances from the core midplane as follows: core, 53.9 cm; axial blanket, 87.2 cm; axial shield, 100.0 cm. Other input data required include the approximate composition of each zone, based on prior experience. A 9-energy-group cross-section library, containing all of the nuclides in Table 3, is output for each zone of each reactor.

3.1.3 Fuel depletion calculation

The fuel depletion calculation was performed with the CITATION²¹ computer code, using a two-dimensional R-Z geometry model and the 9-energy-group cross sections from the previous step. Each CITATION calculation was begun with approximate compositions and was continued until equilibrium discharge concentrations were reached. The middle-of-cycle equilibrium compositions were then volume-averaged over the CITATION model zones for use in XSDRNPM. Also produced in this step were burnup-dependent cross sections for some of the major actinides in Table 3.

3.1.4 Determination of neutron-spectrum-averaged parameters

The final step is to use a characteristic neutron energy spectrum as a weighting function to yield average parameters for use in ORIGEN2. This is done by calculating a 126-energy-group neutron spectrum for each zone of the reactor using the XSDRNPM module of AMPX and the exact equilibrium fuel composition from the previous step. The resulting neutron spectra, which are determined using the ENDF/B-V cross sections in Table 4, are used to collapse the 126-energy-group cross sections in Tables 2 and 4 to 1-energy-group cross sections that can be used directly in ORIGEN2. The spectra are also used to collapse energy-dependent fission product yields from ENDF/B-IV¹² to give average yields that can be used in ORIGEN2. Finally, the spectra are cast into two 2-energy-group structures which yield values for the ORIGEN2 flux parameters THERM, RES, and FAST when the methods described in ref. 4 are applied.

3.2 Spectrum Calculation for the FFTF

Because the FFTF is a test reactor rather than a commercial power reactor, it has several unusual properties:

1. It has no axial or radial blankets.
2. It has many test positions, as well as loops that can contain a wide variety of materials that are unknowable at the present time.
3. The fissile and/or fertile materials in the reactor (currently high-grade plutonium in UO₂) may be changed to other materials in the future.
4. The fuel management and longevity in the reactor are subject to change, depending on performance and other requirements.

These considerations make it very difficult to do a generic depletion calculation; its value is vanishingly small, since the variability in items 2-4 above can change the neutron spectrum drastically. The lack of blankets also eliminates much of the value of the depletion calculation. Therefore, the approach taken here was to perform the energy-self-shielding calculations as described previously (i.e., using BONAMI) and then to use XSDRNPM to (1) account for the spatial self-shielding effects, (2) calculate the characteristic 126-energy-group neutron spectrum, (3) calculate effective, 1-energy-group cross sections for ORIGEN2, and (4) calculate the ORIGEN2 flux parameters. The depletion calculation using CITATION was not performed for the FFTF.

3.3 Summary of Relevant Calculated Results

The relevant results of the foregoing sophisticated reactor physics calculations are summarized below.

3.3.1 Characteristic 126-energy-group neutron spectra

A listing of the energy-group structures and the neutron spectra is given in Appendix A for all reactors considered. A graphical representation is also given in Appendix A for the core, axial blanket, and radial blanket regions of the AMOPUUUX and AMO2TTTX, and for the core of the FFTF.

3.3.2 1-energy-group, effective cross sections

The collapse of the multigroup cross sections for the nuclides in Tables 2 and 4, using the 126-energy-group neutron spectrum as a weighting function, yielded 1-group, effective cross sections for these nuclides. A listing of these 1-group cross sections for the core, axial blanket, and radial blanket regions of the AMOPUUUX and the AMO2TTTX, and for the FFTF core is given in Appendix B.

3.3.3 Burnup-dependent cross sections for major actinides

The depletion calculations performed with CITATION yielded the 1-energy-group, effective cross sections (from ENDF/B-IV) for about a dozen actinides (depending on the reactor) at several different

sequential burnups during fuel irradiation. These are output and are incorporated into ORIGEN2 to improve the accuracy of the actinide buildup and depletion calculation. Tables containing these burnup-dependent cross sections for the core, axial blanket, and radial blanket of the AMOPUUUX and the AMO2TTTX and for the core of the FFTF are given in Appendix C.

3.3.4 ORIGEN2 flux parameters THERM, RES, and FAST

The XSDRNPM module of AMPX is used to perform two 2-energy-group calculations for each region of each reactor. When properly manipulated, these yield the ORIGEN2 flux parameters THERM, RES, and FAST. A list of these parameters for the nine LMFBRs considered in this work is given in Table 5.

4. DESCRIPTION OF REACTOR MODELS

This section summarizes the input and output information for the nine LMFBR models that comprise this work. Specifically, the following four aspects of the models are addressed:

1. a description of the fuel assemblies, including the composition of structural materials,
2. the composition of the oxide fuel in each region of each reactor,
3. a summary description of each reactor, and
4. the composition of the discharged fuel from selected regions and reactors.

4.1 LMFBR Fuel Assembly Description and Composition

The eight commercial LMFBRs considered in this work have the same fuel assembly design, although the designs of the radial blanket assembly and the core/axial blanket assembly within each reactor are different (the radial blanket assembly has fewer fuel elements, with a larger diameter). The FFTF assembly design differs from that of the commercial reactors and, of course, has no blankets. A physical description of these assemblies is given in Table 6.

Table 5. ORIGEN2 flux parameters for LMFBR models

Reactor MNEMONIC ^a	Reactor region	THERM	RES	FAST	Neutron flux (neutrons cm ⁻² sec ⁻¹)
AMOPUUUX	Core	2.888E-11	1.533E-03	0.1508	5.11E + 15
	Ax.Blan.	3.126E-08	2.253E-03	0.0702	1.33E + 15
	Rad.Blan.	6.647E-08	2.328E-03	0.0866	7.27E + 14
EMOPUUUX	Core	3.924E-11	1.615E-03	0.1444	5.37E + 15
	Ax.Blan.	3.287E-08	2.601E-03	0.0681	1.39E + 15
	Rad.Blan.	6.903E-08	2.383E-03	0.0848	6.81E + 14
AMORUUUX	Core	2.679E-11	1.543E-03	0.1481	5.15E + 15
	Ax.Blan.	3.315E-08	2.569E-03	0.0687	1.37E + 15
	Rad.Blan.	8.222E-08	2.335E-03	0.0855	7.17E + 14
AMOPUUTX	Core	8.746E-11	1.577E-03	0.1459	5.25E + 15
	Ax.Blan.	3.242E-08	2.532E-03	0.0688	1.36E + 15
	Rad.Blan.	1.099E-06	2.479E-03	0.0693	1.17E + 15
AMOPTTTX	Core	2.847E-11	1.521E-03	0.1406	6.51E + 15
	Ax.Blan.	5.413E-08	2.456E-03	0.0646	2.28E + 15
	Rad.Blan.	3.524E-07	2.325E-03	0.0759	1.22E + 15
AMO0TTTX	Core	1.168E-10	1.272E-03	0.1705	4.01E + 15
	Ax.Blan.	4.674E-08	2.264E-03	0.0711	1.03E + 15
	Rad.Blan.	4.362E-07	2.157E-03	0.0809	5.10E + 14
AM01TTTX	Core	9.134E-11	1.448E-03	0.1546	4.59E + 15
	Ax.Blan.	4.630E-08	2.369E-03	0.0703	1.19E + 15
	Rad.Blan.	4.581E-07	2.267E-03	0.0764	5.73E + 15
AM02TTTX	Core	1.044E-10	1.266E-03	0.1706	4.17E + 15
	Ax.Blan.	4.978E-08	2.311E-03	0.0687	1.07E + 15
	Rad.Blan.	4.185E-07	2.131E-03	0.0815	5.42E + 15
FFTF	Core	7.301E-11	1.300E-03	0.1737	5.00E + 15

^aSee Table 1 of this document for a description.

Table 6. Physical characteristics of LMFBR fuel assemblies

	Commercial LMFBR ^a		
	Core/axial blanket	Radial blanket	FFTF ^b
Assembly component lengths, cm			
Upper end hardware	91	91	30
Gas plenum	191	191	107
Upper axial blanket	33		17 ^c
Core or radial blanket	122	188	91
Lower axial blanket	33		27 ^c
Lower end hardware	102	102	94
Overall total	572	572	366
Fuel element total	379	379	242
Assembly shape	hexagonal	hexagonal	hexagonal
Assembly flats, cm	13.78	13.78	11.62
Fuel element arrangement	triangular	triangular	triangular
Fuel elements per assembly	271	91	217
Fuel element OD, cm	0.650	1.270	0.584
Fuel pellet OD, cm	0.573	1.180	0.508
Fuel element pitch, cm	0.795	1.369	0.726
Cladding thickness, cm	0.030	0.038	0.038
Channel thickness, cm	0.221	0.221	0.305
Channel height, cm	495	495	~300
Circumscribed volume/assembly, m ³	0.114	0.114	0.052
Heavy metal/assembly, kg	117.7	172.7	33.2
M0 ₂ assembly, kg ^d	133.4	195.9	37.6
Stainless steel/assembly, kg	115.1	97.5	125.7
Inconel 600/assembly, kg			8.9
Assembly total weight, kg	257.7	300.3	172.2

^aBased on data in ref. 10.^bBased on data in refs. 11 and 22.^cUO₂ insulator pellet and Inconel 600 reflector.^d(Pu,U)O₂ in the core/axial blanket and UO₂ in the radial blanket.

Virtually the entire construction of all of the fuel assemblies is stainless steel 316, with the exception of the FFTF assembly, which contains some Inconel 600. The compositions of these metals, including the anticipated trace impurities, are given in Table 7.

4.2 LMFBR Fuel Composition

The LMFBR fuel pellets contain two groups of elements: the actinides and the nonactinides, which include oxygen and impurities. The initial actinide compositions of the LMFBR core fuels are given in Table 8. These fuel compositions are based on the CITATION calculations described in Sect. 3. The initial composition of the FFTF fuel is based on data in refs. 11, 26, and 27.

The initial actinide compositions of the fuel blankets is as follows: uranium blankets - 2000 g $^{235}\text{U}/\text{MTIHM}$ and 998,000 g $^{238}\text{U}/\text{MTIHM}$; thorium blankets - 100 g $^{230}\text{Th}/\text{MTIHM}$ and 999,900 g $^{232}\text{Th}/\text{MTIHM}$. The ^{230}Th in the thorium blankets is an important precursor of ^{232}U , which is the parent of a highly gamma-active decay chain.

The assumed nonactinide composition of the oxide reactor fuels is given in Table 9. Since specific data are not yet available for the fuels considered in this work, the values in Table 9 are the same as those for light water reactor (LWR) oxide fuels.

4.3 Summary Description of the ORIGEN2 LMFBR Models

Fuel depletion calculations were performed for the nine LMFBRs considered in this work with ORIGEN2, using the input compositions given in Sects. 4.1 and 4.2. Results of these calculations, including irradiation conditions and measurements of the uranium, plutonium, and thorium contents of the fresh and spent fuels, are presented in Tables 10-18. All values have been normalized so that the total reactor power is 3956 MW(t). This corresponds to a net electrical power of 1250 MW(e), using the 31.6% thermal efficiency given in ref. 10. These tables can be readily applied to more advanced designs involving higher thermal efficiencies (assuming the fuel assembly design remains unchanged) by simply

Table 7. Typical compositions of stainless steel 316 and Inconel 600

Element	Atomic number	Amount, g/ 10^6 g metal	
		Stainless steel 316 ^a	Inconel 600 ^b
B	5	5	5
C	6	610	400
N	7	320	45
Al	13	165	0
Si	14	5,700	2,000
P	15	204	0
S	16	150	70
Ti	22	150	0
Cr	24	170,500	158,000
Mn	25	18,500	2,000
Fe	26	643,726	72,000
Co	27	150	500
Ni	28	135,500	763,870
Cu	29	900	1,000
Nb	41	100	100
Mo	42	23,400	0
Sn	50	40	0
Pb	82	30	0
Density, g/cm ³		8.02	8.33

^aData from ref. 23.^bData from refs. 24 and 25.

Table 8. Heavy metal composition of 1000 kg of LMFBR core fuel

	Reactor type ^a								FFTF ^b		
	AMOPUUUX	EMOPUUUX	AMORUUUX	AMOPUUTX	AMOPTTX	AMOOTTX	AMO1TTX	AMO2TTX	Inner core	Outer core	Weighted average
²³⁰ Th, g					81	79		60			
²³² Th, g					809,377	793,036		603,293			
Total thorium, g					809,458	793,115		603,353			
²³² U, g						402	315	375			
²³³ U, g						172,227	134,816	160,665			
²³⁴ U, g						29,800	23,323	27,795	43	40	41
²³⁵ U, g	1,676	2,054	1,674	1,675		4,455	3,492	4,161	5,503	5,142	5,283
²³⁶ U, g						1	1	1			
²³⁸ U, g	813,656	831,650	821,912	821,470			838,053	203,650	769,523	719,044	738,827
Total uranium, g	815,332	833,704	823,586	823,145		206,885	1,000,000	396,647	775,069	724,226	744,151
²³⁶ Pu, g	0.023	0.021	0.0029	0.022	0.024				0.003	0.074	0.004
²³⁸ Pu, g	2,586	2,317	324	2,476	2,668				337	413	383
²³⁹ Pu, g	101,567	91,159	128,592	97,275	104,803				192,407	235,787	218,787
²⁴⁰ Pu, g	46,738	41,944	39,793	44,755	48,218				25,777	31,715	29,388
²⁴¹ Pu, g	24,557	22,593	5,209	23,511	25,331				5,623	6,894	6,396
²⁴² Pu, g	9,220	8,283	2,496	8,838	9,522				787	965	895
Total plutonium, g	184,668	166,296	176,414	176,855	190,542				224,931	275,774	255,849
Total heavy metal, g	1,000,000	1,000,000	1,000,000	1,000,000	1,000,000	1,000,000	1,000,000	1,000,000	1,000,000	1,000,000	1,000,000

^aSee Table 1 of this document for mnemonic identification.^bFuel should be decayed from 1/71 before irradiation.

Table 9. Assumed nonactinide composition of LMFBR oxide fuels^a

Element	Atomic number	Concentration (g/MTIHM) ^b	Element	Atomic number	Concentration (g/MTIHM) ^a
Li	3	1.0	Mn	25	1.7
B	5	1.0	Fe	26	18.0
C	6	89.4	Co	27	1.0
N	7	25.0	Ni	28	24.0
O	8	134,454 ^c	Cu	29	1.0
F	9	10.7	Zn	30	40.3
Na	11	15.0	Mo	42	10.0
Mg	12	2.0	Ag	47	0.1
Al	13	16.7	Cd	48	25.0
Si	14	12.1	In	49	2.0
P	15	35.0	Sn	50	4.0
Cl	17	5.3	Gd	64	2.5
Ca	20	2.0	W	74	2.0
Ti	22	1.0	Pb	82	1.0
V	23	3.0	Bi	83	0.4
Cr	24	4.0			

^aData obtained from refs. 28 to 32.^bParts of element per million parts of heavy metal.^cStoichiometric quantity for (Pu,U)O₂ fuel; use 137,931 g/MTIHM for thorium-based fuels.

Table 10. Summary characteristics for an AMOPUUUX^a

Parameter	Fuel region(s) ^b				
	CO	AB	RB	CO + AB	CO + AB + RB
Electric power, MW(e)	1154	34	62	1188	1250
Thermal power, MW(t)	3652	108	197	3760	3957
Average specific power, ^c MW(t)/MTIHM	123.25	6.89	3.59	83.10	39.56
Average fuel burnup, MWd/MTIHM	101,289	5660	5900	68,280	44,758
Irradiation duration, full-power days	821.8	821.8	1643.6	821.8	
Refueling cycle length, full-power days	273.9	273.9	273.9	273.9	273.9
Charge, kg/refueling cycle					
Thorium	0	0	0	0	0
Fissile uranium ^d	16.5	10.4	18.2	26.9	45.1
Total uranium	8052	5207	9130	13,259	22,389
Fissile plutonium ^e	1246	0	0	1246	1246
Total plutonium	1824	0	0	1824	1824
Total (Th + U + Pu)	9876	5207	9130	15,083	24,213
Discharge, kg/refueling cycle					
Thorium	0	0	0	0	0
Fissile uranium ^d	6.9	7.6	13.2	14.5	27.7
Total uranium	7125	5010	8776	12,135	20,911
Fissile plutonium ^e	1102	160	287	1262	1549
Total plutonium	1695	167	298	1862	2160
Total (Th + U + Pu)	8820	5177	9074	13,997	23,071

^aSee Table 1 for mnemonic definition.^bCO = core, AB = axial blanket, RB = radial blanket.^cBased on full power and fuel charged.^d ^{233}U + ^{235}U + ^{233}Pa .^e ^{239}Pu + ^{241}Pu + ^{239}Np .

Table 11. Summary characteristics for an EMOPUUUX^a

Parameter	Fuel region(s) ^b				
	CO	AB	RB	CO + AB	CO + AB + RB
Electric power, MW(e)	1165	30	55	1195	1250
Thermal power, MW(t)	3689	94	173	3783	3956
Average specific power, ^c MW(t)/MTIHM	124.1	6.03	3.15	83.37	39.46
Average fuel burnup, MWd/MTIHM	67,992	3300	5180	45,677	34,041
Irradiation duration, full-power days	547.9	547.9	1643.6	547.9	
Refueling cycle length, full-power days	273.9	273.9	273.9	273.9	273.9
Charge, kg/refueling cycle					
Thorium	0	0	0	0	0
Fissile uranium ^d	30.6	15.6	18.3	46.2	64.5
Total uranium	12,386	7826	9147	20,212	29,359
Fissile plutonium ^e	1694	0	0	1694	1694
Total plutonium	2476	0	0	2476	2476
Total (Th + U + Pu)	14,862	7826	9147	22,688	31,835
Discharge, kg/refueling cycle					
Thorium	0	0	0	0	0
Fissile uranium ^d	16.3	12.5	13.6	28.8	42.4
Total uranium	11,358	7615	8820	18,973	27,793
Fissile plutonium ^e	1628	179	267	1807	2074
Total plutonium	2433	183	277	2616	2893
Total (Th + U + Pu)	13,791	7798	9097	21,589	30,686

^aSee Table 1 for mnemonic definition.^bCO = core, AB = axial blanket, RB = radial blanket.^cBased on full power and fuel charged.^d ^{233}U + ^{235}U + ^{233}Pa .^e ^{239}Pu + ^{241}Pu + ^{239}Np .

Table 12. Summary characteristics for an AMORUUUX^a

Parameter	Fuel region(s) ^b				
	CO	AB	RB	CO + AB	CO + AB + RB
Electric power, MW(e)	1154	35	61	1189	1250
Thermal power, MW(t)	3652	112	192	3764	3956
Average specific power, ^c MW(t)/MTIHM	123.25	7.18	3.51	83.21	39.57
Average fuel burnup, MWd/MTIHM	101,289	5900	5770	68,385	44,783
Irradiation duration, full-power days	821.8	821.8	1643.6	821.8	
Refueling cycle length, full-power days	273.9	273.9	273.9	273.9	273.9
Charge, kg/refueling cycle					
Thorium	0	0	0	0	0
Fissile uranium ^d	16.5	10.4	18.2	26.9	45.1
Total uranium	8133	5202	9122	13,335	22,457
Fissile plutonium ^e	1321	0	0	1321	1321
Total plutonium	1743	0	0	1743	1743
Total (Th + U + Pu)	9876	5202	9122	15,078	24,200
Discharge, kg/refueling cycle					
Thorium	0	0	0	0	0
Fissile uranium ^d	6.8	7.5	13.2	14.3	27.5
Total uranium	7194	4999	8772	12,193	20,965
Fissile plutonium ^e	1158	164	284	1322	1606
Total plutonium	1648	171	295	1819	2114
Total (Th + U + Pu)	8842	5170	9067	14,012	23,079

^aSee Table 1 for mnemonic definition.^bCO = core, AB + axial blanket, RB = radial blanket.^cBased on full power and fuel charged.^d ^{233}U + ^{235}U + ^{233}Pa .^e ^{239}Pu + ^{241}Pu + ^{239}Np .

Table 13. Summary characteristics for an AMOPUUTX^a

Parameter	Fuel region(s) ^b				
	CO	AB	RB	CO + AB	CO + AB + RB
Electric power, MW(e)	1144	33	73	1177	1250
Thermal power, MW(t)	3620	105	231	3725	3956
Average specific power, ^c MW(t)/MTIHM	122.52	6.75	4.43	82.53	40.71
Average fuel burnup, MWd/MTIHM	100,689	5550	7280	67,825	45,693
Irradiation duration, full-power days	821.8	821.8	1643.6	821.8	
Refueling cycle length, full-power days	273.9	273.9	273.9	273.9	273.9
Charge, kg/refueling cycle					
Thorium	0	0	8670	0	8670
Fissile uranium ^d	16.5	10.4	0	26.9	26.9
Total uranium	8108	5198	0	13,306	13,306
Fissile plutonium ^e	1190	0	0	1190	1190
Total plutonium	1742	0	0	1742	1742
Total (Th + U + Pu)	9850	5198	8670	15,048	23,718
Discharge, kg/refueling cycle					
Thorium	0	0	8301	0	8301
Fissile uranium ^d	6.7	7.7	296	14.4	310
Total uranium	7154	5010	304	12,164	12,468
Fissile plutonium ^e	1079	154	0	1233	1233
Total plutonium	1652	161	0	1813	1813
Total (Th + U + Pu)	8841	5171	8606	14,012	22,618

^aSee Table 1 for mnemonic definition.^bCO = core, AB = axial blanket, RB = radial blanket.^cBased on full power and fuel charged.^d $^{233}\text{U} + ^{235}\text{U} + ^{233}\text{Pa}$.^e $^{239}\text{Pu} + ^{241}\text{Pu} + ^{239}\text{Np}$.

Table 14. Summary characteristics for an AMOPTTTX^a

Parameter	Fuel region(s) ^b				
	CO	AB	RB	CO + AB	CO + AB + RB
Electric power, MW(e)	1145	34	71	1179	1250
Thermal power, MW(t)	3624	107	225	3731	3956
Average specific power, ^c MW(t)/MTIHM	129.55	7.28	4.37	87.38	41.97
Average fuel burnup, MWd/MTIHM	106,467	5980	7180	71,806	47,478
Irradiation duration, full-power days	821.8	821.8	1643.6	821.8	
Refueling cycle length, full-power days	273.9	273.9	273.9	273.9	273.9
Charge, kg/refueling cycle					
Thorium	7547	4909	8592	12,456	21,048
Fissile uranium ^d	0	0	0	0	0
Total uranium	0	0	0	0	0
Fissile plutonium ^e	1213	0	0	1213	1213
Total plutonium	1776	0	0	1776	1776
Total (Th + U + Pu)	932.3	4909	8592	14,232	22,824
Discharge, kg/refueling cycle					
Thorium	6795	4729	8237	11,524	19,761
Fissile uranium ^d	414	148	283	562	845
Total uranium	479	153	291	632	923
Fissile plutonium ^e	535	0	0	535	535
Total plutonium	1021	0	0	1021	1021
Total (Th + U + Pu)	8319	4882	8529	13,201	21,730

^aSee Table 1 for mnemonic definition.^bCO = core, AB = axial blanket, RB = radial blanket.^cBased on full power and fuel charged.^d ^{233}U + ^{235}U + ^{233}Pa .^e ^{239}Pu + ^{241}Pu + ^{239}Np .

Table 15. Summary characteristics for an AMOOTTX^a

Parameter	Fuel region(s) ^b				
	CO	AB	RB	CO + AB	CO + AB + RB
Electric power, MW(e)	1194	20	36	1214	1250
Thermal power, MW(t)	3780	62	114	3842	3956
Average specific power, ^c MW(t)/MTIHM	135.28	4.15	2.18	89.57	41.51
Average fuel burnup, MWd/MTIHM	111,176	3410	3583	73,608	47,049
Irradiation duration, full-power days	821.8	821.8	1643.6	821.8	
Refueling cycle length, full-power days	273.9	273.9	273.9	273.9	273.9
Charge, kg/refueling cycle					
Thorium	7386	4984	8736	12,370	21,106
Fissile uranium ^d	1645	0	0	1645	1645
Total uranium	1927	0	0	1927	1927
Fissile plutonium ^e	0	0	0	0	0
Total plutonium	0	0	0	0	0
Total (Th + U + Pu)	9313	4984	8736	14,297	23,033
Discharge, kg/refueling cycle					
Thorium	6706	4829	8456	11,535	19,991
Fissile uranium ^d	1226	136	242	1362	1604
Total uranium	1537	138	246	1675	1921
Fissile plutonium ^e	0	0	0	0	0
Total plutonium	0	0	0	0	0
Total (Th + U + Pu)	8246	4968	8702	13,214	21,916

^aSee Table 1 for mnemonic definition.^bCO = core, AB + axial blanket, RB = radial blanket.^cBased on full power and fuel charged.^d $^{233}\text{U} + ^{235}\text{U} + ^{233}\text{Pa}$.^e $^{239}\text{Pu} + ^{241}\text{Pu} + ^{239}\text{Np}$.

Table 16. Summary characteristics for an AM01TTTX^a

Parameter	Fuel region(s) ^b				
	CO	AB	RB	CO + AB	CO + AB + RB
Electric power, MW(e)	1168	38	44	1206	1250
Thermal power, MW(t)	3698	119	139	3817	3956
Average specific power, ^c MW(t)/MTIHM	125.38	7.64	2.54	84.65	39.65
Average fuel burnup, MWd/MTIHM	103,040	6270	4175	69,566	44,880
Irradiation duration, full-power days	821.8	821.8	1643.6	821.8	
Refueling cycle length, full-power days	273.9	273.9	273.9	273.9	273.9
Charge, kg/refueling cycle					
Thorium	0	5199	9115	5199	14,314
Fissile uranium ^d	1360	0	0	1360	1360
Total uranium	9831	0	0	9831	9831
Fissile plutonium ^e	0	0	0	0	0
Total plutonium	0	0	0	0	0
Total (Th + U + Pu)	9831	5199	9115	15,030	24,145
Discharge, kg/refueling cycle					
Thorium	0	4945	8806	4945	13,751
Fissile uranium ^d	575	220	265	795	1060
Total uranium	8270	224	270	8494	8767
Fissile plutonium ^e	478	0	0	478	478
Total plutonium	512	0	0	512	512
Total (Th + U + Pu)	8785	5169	9077	13,954	23,031

^aSee Table 1 for mnemonic definition.^bCO = core, AB + axial blanket, RB = radial blanket.^cBased on full power and fuel charged.^d ^{233}U + ^{235}U + ^{233}Pa .^e ^{239}Pu + ^{241}Pu + ^{239}Np .

Table 17. Summary characteristics for an AM02TTTX^a

Parameter	Fuel region(s) ^b				
	CO	AB	RB	CO + AB	CO + AB + RB
Electric power, MW(e)	1191	20	39	1211	1250
Thermal power, MW(t)	3768	64	124	3832	3956
Average specific power, ^c MW(t)/MTIHM	131.60	4.26	2.36	87.95	41.23
Average fuel burnup, MWD/MTIHM	108,151	3500	3879	72,278	46,603
Irradiation duration, full-power days	821.8	821.8	1643.6	821.8	
Refueling cycle length, full-power days	273.9	273.9	273.9	273.9	273.9
Charge, kg/refueling cycle					
Thorium	5760	4979	8729	10,739	19,468
Fissile uranium ^d	1573	0	0	1573	1573
Total uranium	3786	0	0	3786	3786
Fissile plutonium ^e	0	0	0	0	0
Total plutonium	0	0	0	0	0
Total (Th + U + Pu)	9546	4979	8729	14,525	23,254
Discharge, kg/refueling cycle					
Thorium	5218	4827	8446	10,045	18,491
Fissile uranium ^d	1083	134	244	1217	1461
Total uranium	3149	136	249	3285	3534
Fissile plutonium ^e	106	0	0	106	106
Total plutonium	113	0	0	113	113
Total (Th + U + Pu)	8482	4963	8695	13,445	22,140

^aSee Table 1 for mnemonic definition.^bCO = core, AB + axial blanket, RB = radial blanket.^cBased on full power and fuel charged.^d ^{233}U + ^{235}U + ^{233}Pa .^e ^{239}Pu + ^{241}Pu + ^{239}Np .

Table 18. Summary characteristics for an FFTF^a

Parameter	Fuel region(s)		
	Inner core	Outer core	Total
Electric power, MW(e)	0	0	0
Thermal power, MW(t)	138	214	352
Average specific power, ^b MW(t)/MTIHM	143	143	143
Average fuel burnup, MWd/MTIHM	45,000	45,000	45,000
Irradiation duration, full-power days	315	315	315
Refueling cycle length, full-power days	105	105	105
Charge, kg/refueling cycle			
Thorium	0	0	0
Fissile uranium ^c	1.8	2.6	4.4
Total uranium	249	361	610
Fissile plutonium ^d	64	121	185
Total plutonium	72	137	209
Total (Th + U + Pu)	321	498	819
Discharge, kg/refueling cycle			
Thorium		0	
Fissile uranium ^c		3.5	
Total uranium		587	
Fissile plutonium ^d		163	
Total plutonium		193	
Total (Th + U + Pu)		780	

^aSee Table 1 for mnemonic definition.^bBased on full power and fuel charged.^c ^{233}U + ^{235}U + ^{233}Pa .^d ^{239}Pu + ^{241}Pu + ^{239}Np .

increasing the amount of electricity produced to a value greater than the 3956 MW(t) that forms the basis of the reactor models. Thus, the fuel being charged and discharged to the reactor and its irradiation conditions would be essentially unchanged, but increased temperatures would allow more electricity to be produced from the fuel.

4.4 Discharge Compositions of Selected LMFBR Fuels

The actinide discharge composition of the three U-Pu cycle commercial LMFBR core fuels and the average FFTF fuel are given in Table 19. The effect of recycling plutonium in the LMFBR may be seen by comparison of the AMOPUUUX and AMORUUUX discharge compositions, which indicate that the production of the heavier plutonium and transplutonium nuclides is substantially reduced in the latter. The discharge compositions for all of the blankets are somewhat similar.

The discharge compositions for typical U-Pu cycle axial and radial blankets, as represented by the AMOPUUUX, are given in Table 20.

Table 19. Discharge fuel composition for 1000 kg (one tonne)
of selected core fuels^a

Nuclide	Discharge fuel composition (g/MTIHM)			FFTF average
	AMOPUUUX ^b	AMORUUUX ^b	EMOPUUUX ^b	
²³⁵ U	696	692	1096	4277
²³⁶ U	210	208	210	251
²³⁸ U	720,400	727,400	762,800	712,000
Total uranium	721,400	728,400	764,200	716,600
²³⁷ Np	389	382	293	209
²³⁸ Pu	1553	308	1538	407
²³⁹ Pu (+ ²³⁹ Np)	98,748	110,929	95,811	194,843
²⁴⁰ Pu	49,410	46,970	44,420	34,600
²⁴¹ Pu	12,840	6374	13,760	4170
²⁴² Pu	9335	2696	8569	1027
Total plutonium	171,886	167,277	164,098	235,047
²⁴¹ Am	1304	450	974	2159
²⁴³ Am	1511	409	1052	35.4
²⁴² Cm	127	40	84	120
²⁴⁴ Cm	248	67	134	1.43
Total heavy metal	896,900	897,000	930,800	954,200
Burnup, GWd/MTIHM	100	100	68	45

^aSee Table 8 for initial compositions.

^bSee Table 1 for mnemonic definitions.

Table 20. Charge and discharge composition of AMOPUUUX^a blankets

Nuclide	Charge composition (g/MTIHM)	Discharge composition (g/MTIHM)	
		Axial blanket	Radial blanket
²³⁵ U	2000	1460	1446
²³⁶ U		134	139
²³⁸ U	998,000	960,500	959,600
Total uranium	1,000,000	962,100	961,200
²³⁷ Np		68.8	86.9
²³⁸ Pu		8.0	9.4
²³⁹ Pu (+ ²³⁹ Np)		30,782	31,404
²⁴⁰ Pu		1336	1347
²⁴¹ Pu		35.7	36.6
²⁴² Pu		0.6	0.7
Total plutonium		32,162	32,798
²⁴¹ Am		0.98	1.1
²⁴³ Am		0.012	0.013
²⁴² Cm		0.02	0.03
²⁴⁴ Cm		0.00037	0.00044
Total heavy metal	1,000,000	994,300	994,100
Burnup, GWd/MTIHM	0	5.7	5.9

^aSee Table 1 for mnemonic definition.

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APPENDIX A:

126-ENERGY-GROUP NEUTRON SPECTRA
GRAPHS AND LISTINGS

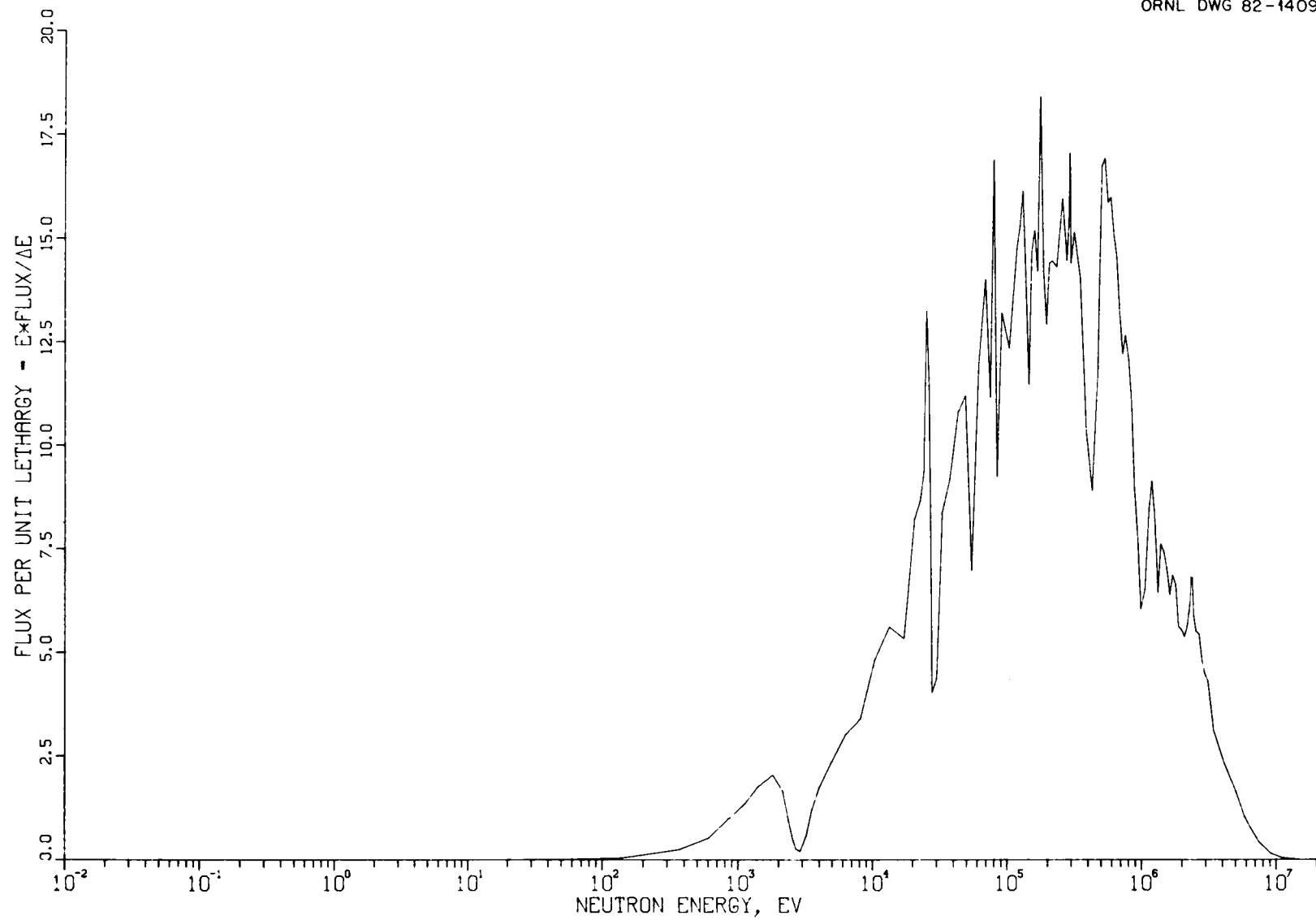


Fig. A.1. Neutron energy spectrum in AMOPUUUX core fuel.

ORNL DWG 82-1407

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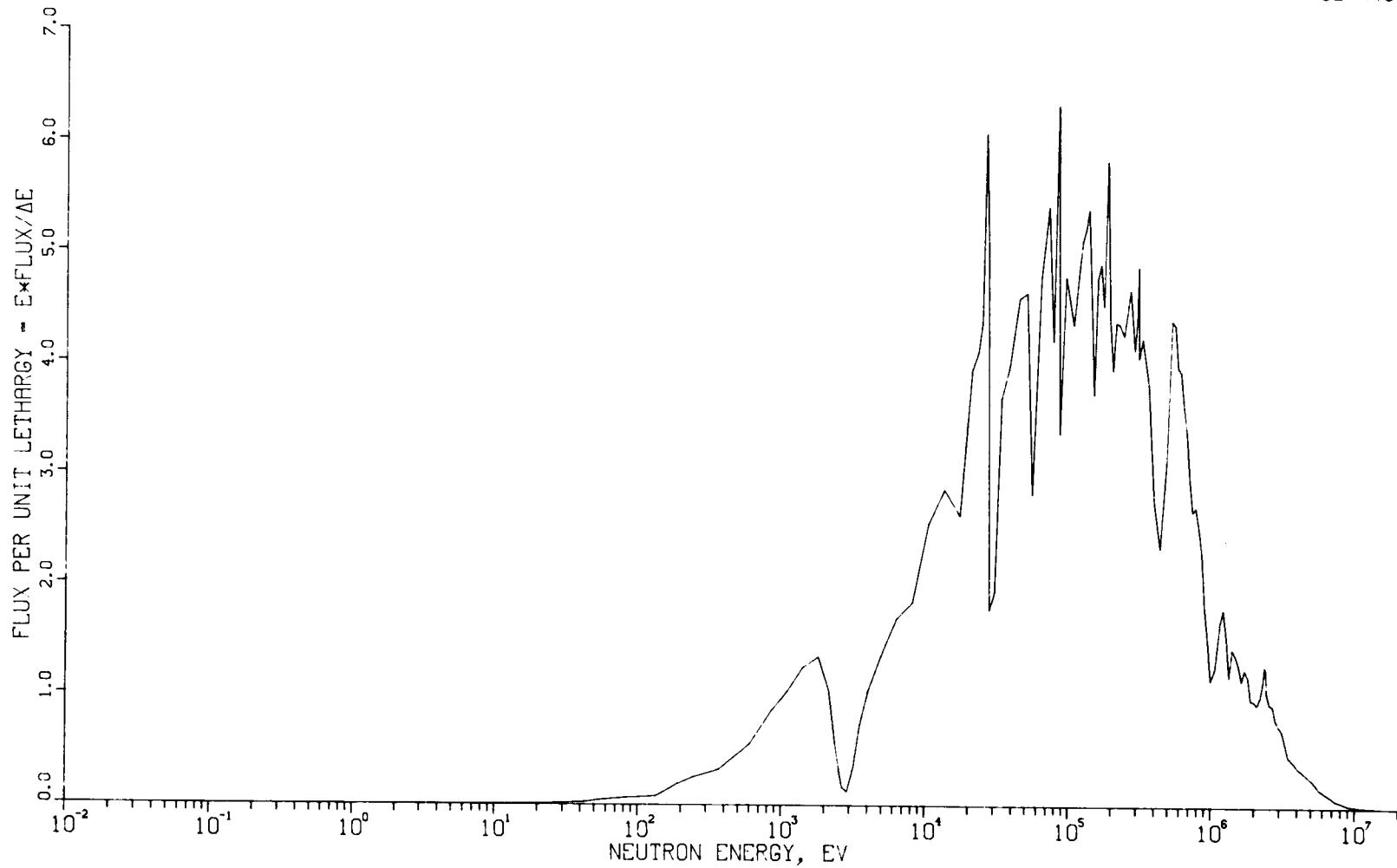


Fig. A. 2. Neutron energy spectrum in AMOPUUUX axial blanket fuel.

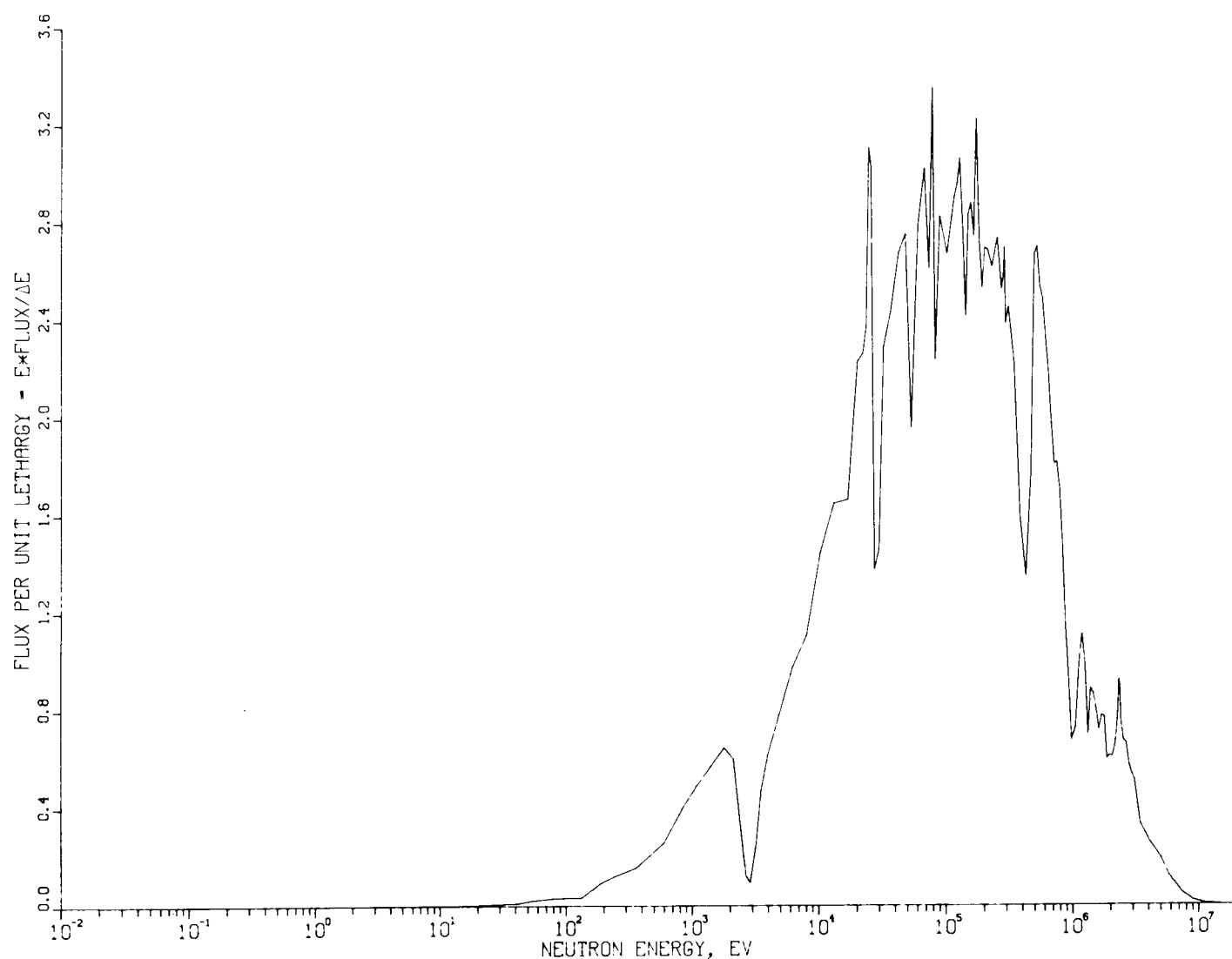


Fig. A. 3. Neutron energy spectrum in AMOPUUUX radial blanket fuel.

ORNL DWG 82-1413

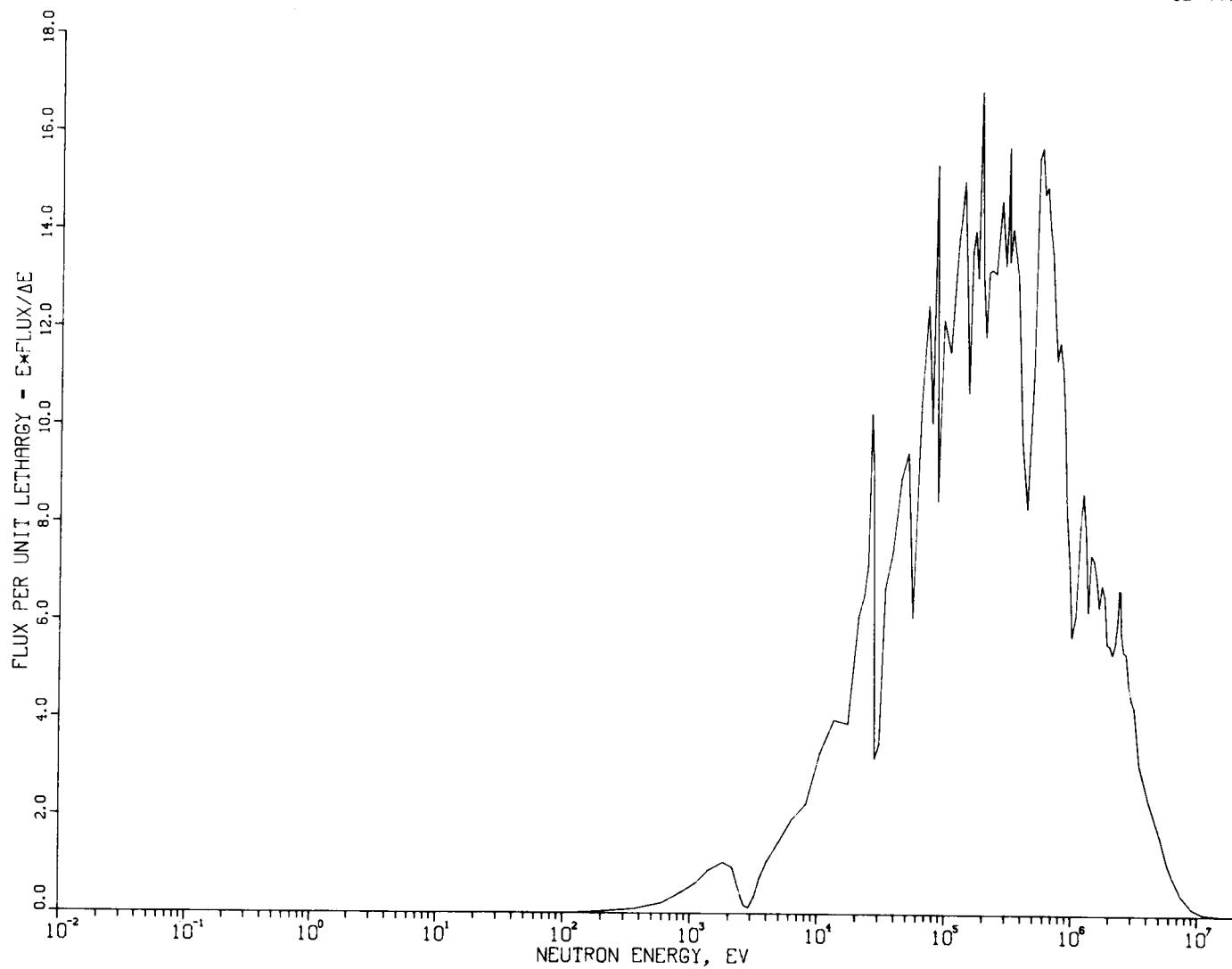


Fig. A.4. Neutron energy spectrum in AM0ZTTX core fuel.

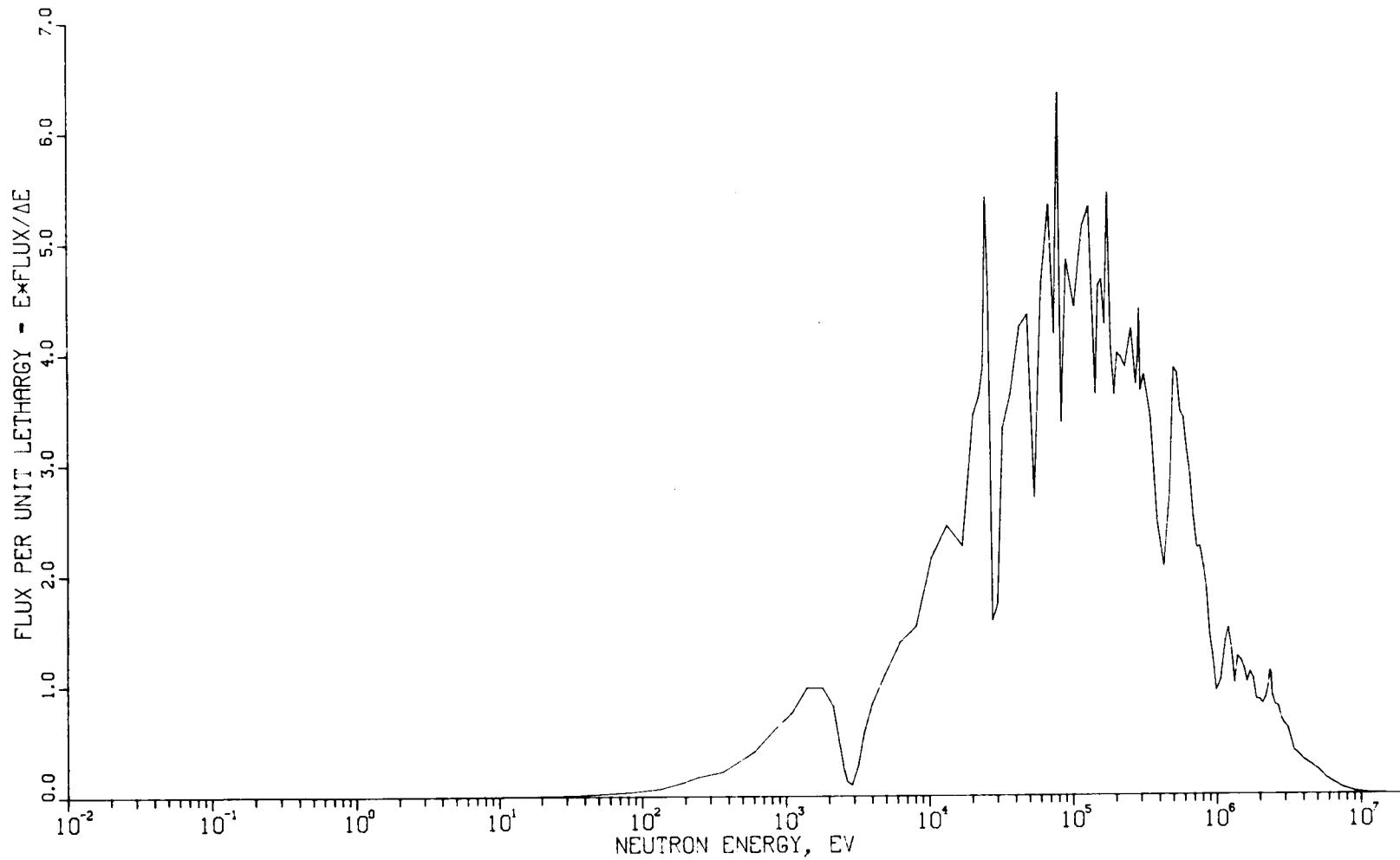


Fig. A.5. Neutron energy spectrum in AMO2TTX axial blanket fuel.

ORNL DWG 82-1414

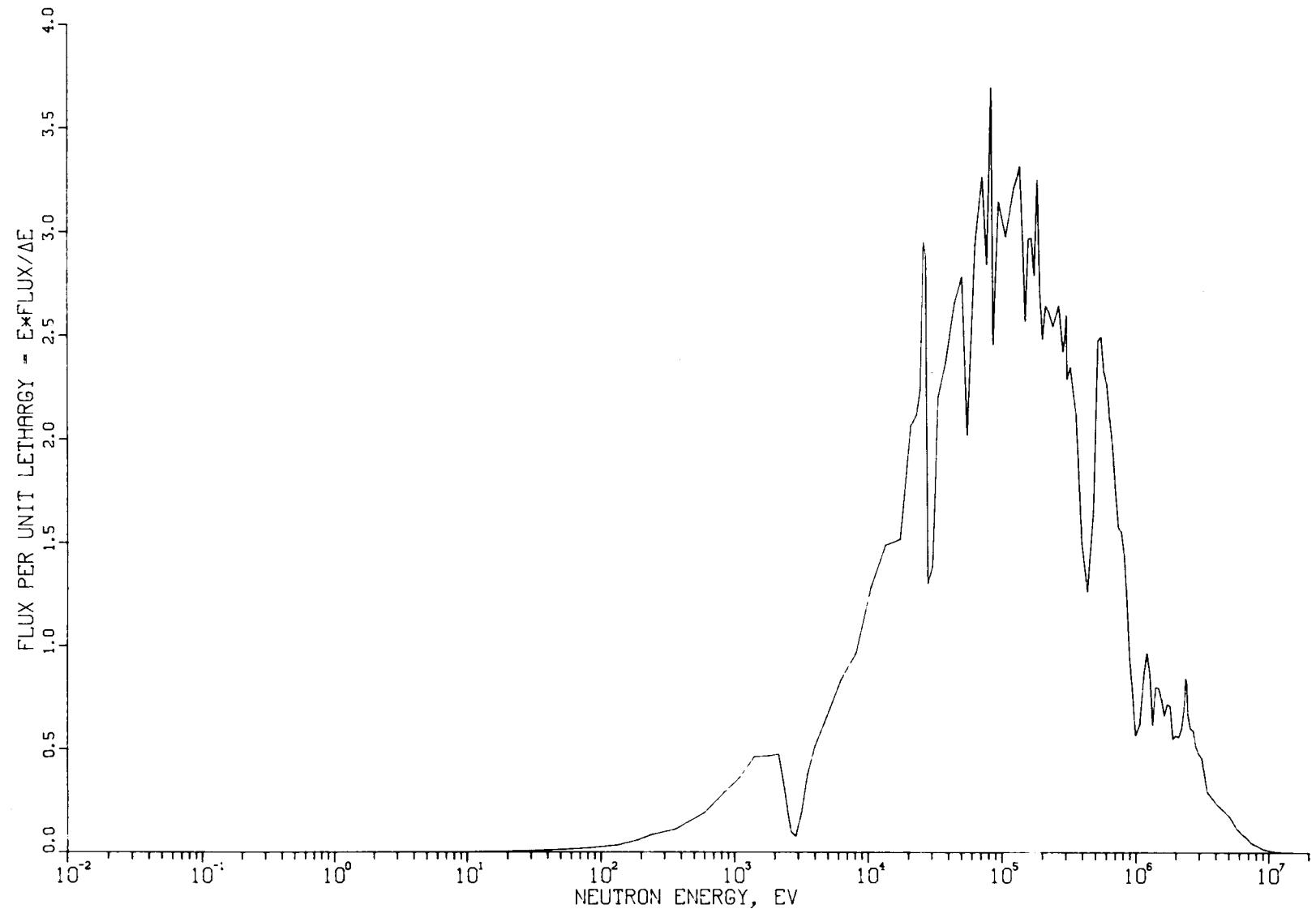


Fig. A.6. Neutron energy spectrum in AMO2TTX radial blanket fuel.

FFTF

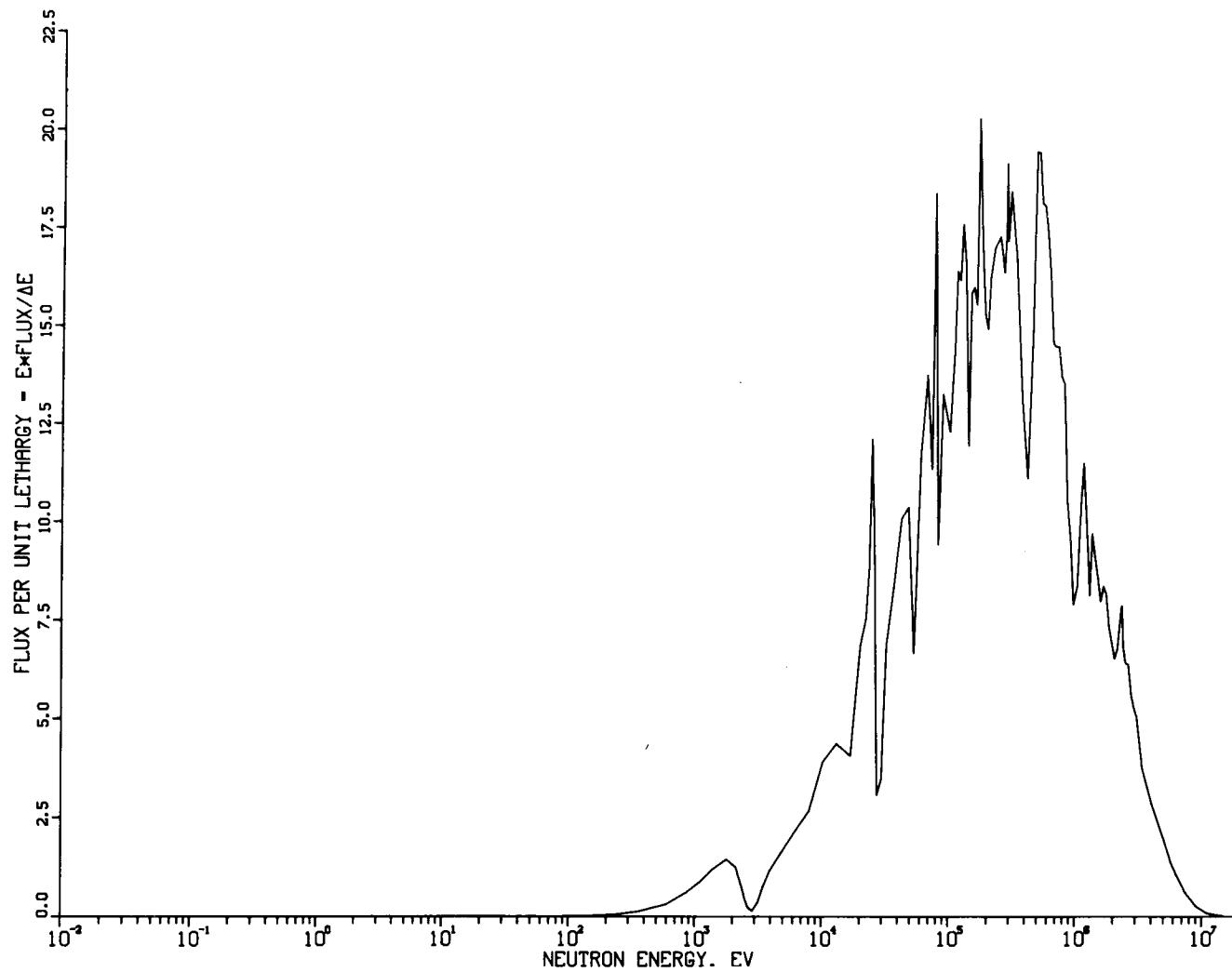


Fig. A.7. Neutron energy spectrum in FFTF core fuel.

Table A.1 (continued)

Energy group	Group energy boundaries, eV		AMOPUUUX			AMORUUUX		
	Upper	Lower	Core	Axial blanket	Radial blanket	Core	Axial blanket	Radial blanket
111	7.48520E 02	4.54000E 02	4.67506E-01	2.54360E-01	2.46547E-01	5.59344E-01	5.97069E-01	5.34122E-01
112	4.54000E 02	2.75360E 02	1.78188E-01	1.01228E-01	1.25418E-01	2.21331E-01	3.00563E-01	3.08593E-01
113	2.75360E 02	2.14450E 02	8.22562E-02	5.56226E-02	7.31495E-02	1.04253E-01	1.78497E-01	1.92581E-01
114	2.14450E 02	1.67020E 02	4.88294E-02	3.95727E-02	5.59457E-02	6.41051E-02	1.34193E-01	1.53882E-01
115	1.67020E 02	1.01300E 02	1.40265E-02	1.39749E-02	2.06076E-02	1.93180E-02	5.58819E-02	7.29467E-02
116	1.01300E 02	6.14420E 01	4.81099E-03	1.03744E-02	1.61157E-02	7.11362E-03	3.72439E-02	5.22446E-02
117	6.14420E 01	4.78510E 01	1.53046E-03	5.53413E-03	9.25742E-03	2.36602E-03	1.98305E-02	2.92727E-02
118	4.78510E 01	3.72670E 01	4.71289E-04	2.51574E-03	4.42579E-03	7.97763E-04	9.87112E-03	1.64031E-02
119	3.72670E 01	2.26030E 01	2.35558E-04	2.26684E-03	3.28905E-03	4.81942E-04	6.89249E-03	1.31978E-02
120	2.26030E 01	1.06770E 01	2.17422E-05	6.76891E-04	6.92569E-04	5.03084E-05	1.72679E-03	3.36179E-03
121	1.06770E 01	5.04350E 00	1.62274E-06	2.03979E-04	1.15550E-04	4.20095E-06	3.94864E-04	6.69724E-04
122	5.04350E 00	2.37239E 00	6.81776E-07	1.37041E-04	1.33257E-04	2.25029E-06	2.18699E-04	6.11413E-04
123	2.37239E 00	1.12540E 00	2.18815E-07	4.14767E-05	6.20329E-05	6.42351E-07	6.90882E-05	3.31814E-04
124	1.12540E 00	4.13990E-01	1.77656E-08	5.87450E-06	1.25199E-05	2.97420E-08	9.96113E-06	4.72489E-05
125	4.13990E-01	1.00000E-01	7.40016E-09	1.91692E-07	3.49671E-07	7.42229E-09	3.47840E-07	1.22207E-06
126	1.00000E-01	1.00000E-05	5.43688E-10	8.38406E-09	1.24730E-08	5.68503E-10	1.44885E-08	6.89637E-08

Table A.2 (continued)

Energy group	Group energy boundaries, eV		EMOPUUUX			AMOPUUTX		
	Upper	Lower	Core	Axial blanket	Radial blanket	Core	Axial blanket	Radial blanket
111	7.48520E 02	4.54000E 02	5.33556E-01	5.99915E-01	2.45377E-01	3.46331E-01	3.24522E-01	1.20877E-01
112	4.54000E 02	2.75360E 02	2.06714E-01	3.04490E-01	1.24038E-01	1.15251E-01	1.32917E-01	4.55186E-02
113	2.75360E 02	2.14450E 02	9.67394E-02	1.82339E-01	7.20402E-02	4.25985E-02	5.80801E-02	1.72327E-02
114	2.14450E 02	1.67020E 02	5.83979E-02	1.37952E-01	5.49641E-02	1.45051E-02	2.04367E-02	4.90727E-03
115	1.67020E 02	1.01300E 02	1.67797E-02	5.77863E-02	2.00570E-02	1.82325E-03	3.34969E-03	6.17284E-04
116	1.01300E 02	6.18420E 01	6.11315E-03	3.93840E-02	1.54472E-02	6.76103E-04	2.47394E-03	4.89105E-04
117	6.18420E 01	4.78510E 01	1.98559E-03	2.13586E-02	8.80126E-03	2.10423E-04	2.55219E-03	6.70353E-04
118	4.78510E 01	3.72670E 01	6.24572E-04	1.07137E-02	4.11005E-03	6.25722E-05	1.56643E-03	4.08154E-04
119	3.72670E 01	2.26030E 01	3.28503E-04	7.37896E-03	2.98056E-03	5.38756E-06	1.71795E-04	3.56672E-05
120	2.26030E 01	1.06770E 01	3.04748E-05	1.84914E-03	6.10861E-04	2.97898E-07	5.05563E-05	1.06416E-05
121	1.06770E 01	5.04350E 00	2.25081E-06	4.05556E-04	9.85423E-05	7.44319E-08	1.53827E-05	3.40147E-06
122	5.04350E 00	2.37239E 00	8.74558E-07	2.16036E-04	1.15602E-04	4.33862E-07	8.99087E-05	6.85708E-05
123	2.37239E 00	1.12540E 00	2.75266E-07	6.93178E-05	4.97106E-05	2.16895E-07	3.61037E-05	5.29815E-05
124	1.12540E 00	4.13990E-01	1.95156E-08	1.08581E-05	1.03157E-05	1.95701E-08	6.41352E-06	1.53613E-05
125	4.13990E-01	1.00000E-01	8.09937E-09	3.83479E-07	2.73171E-07	7.26768E-09	2.08648E-07	5.17688E-07
126	1.00000E-01	1.00000E-05	6.77840E-10	1.53388E-08	8.55605E-09	6.18153E-10	9.96479E-09	3.59488E-08

Table A.3 (continued)

Energy group	Group energy boundaries, eV		AMOPTTX			AMOOTTX		
	Upper	Lower	Core	Axial blanket	Radial blanket	Core	Axial blanket	Radial blanket
111	7.48520E 02	4.54000E 02	5.00147E-01	6.30390E-01	3.67070E-01	1.81155E-01	3.46919E-01	1.99483E-01
112	4.54000E 02	2.75360E 02	1.75335E-01	2.94732E-01	1.86202E-01	5.45948E-02	1.56562E-01	1.02437E-01
113	2.75360E 02	2.14450E 02	7.64116E-02	1.70549E-01	1.11007E-01	2.11102E-02	8.79230E-02	6.22247E-02
114	2.14450E 02	1.67020E 02	3.89724E-02	1.11151E-01	7.45277E-02	9.55794E-03	5.59919E-02	4.25604E-02
115	1.67020E 02	1.01300E 02	1.33205E-02	6.44120E-02	4.63411E-02	3.87980E-03	3.24521E-02	2.71010E-02
116	1.01300E 02	6.14420E 01	3.23418E-03	3.55945E-02	2.79276E-02	1.19190E-03	1.83711E-02	1.67181E-02
117	6.14420E 01	4.78510E 01	9.23892E-04	1.79717E-02	1.48557E-02	3.56574E-04	9.33076E-03	9.05561E-03
118	4.78510E 01	3.72670E 01	4.13009E-04	1.27967E-02	1.18645E-02	2.05735E-04	6.87099E-03	7.15062E-03
119	3.72670E 01	2.26030E 01	1.63394E-04	6.60791E-03	6.49493E-03	5.23413E-05	3.60914E-03	4.02001E-03
120	2.26030E 01	1.06770E 01	1.99823E-05	2.32967E-03	2.21237E-03	7.91751E-06	1.34594E-03	1.41431E-03
121	1.06770E 01	5.04350E 00	3.81981E-06	9.51581E-04	8.73399E-04	1.49728E-06	5.88515E-04	5.61173E-04
122	5.04350E 00	2.37239E 00	1.66148E-06	3.34236E-04	5.20840E-04	8.37496E-07	2.09541E-04	3.23809E-04
123	2.37239E 00	1.12540E 00	2.85225E-07	7.06009E-05	1.17850E-04	9.08648E-08	4.51807E-05	8.28441E-05
124	1.12540E 00	4.13990E-01	3.00916E-08	1.45544E-05	3.89583E-05	8.62851E-08	9.23348E-06	2.63940E-05
125	4.13990E-01	1.00000E-01	8.06679E-09	7.20799E-07	2.40349E-06	1.70814E-08	4.53837E-07	1.69416E-06
126	1.00000E-01	1.00000E-05	5.72139E-10	2.35823E-08	9.37007E-08	6.04996E-10	1.46544E-08	7.06901E-08

Table A.4 (continued)

Energy group	Group energy boundaries, eV		AM01TTX			AM02TTX			FFTF
	Upper	Lower	Core	Axial blanket	Radial blanket	Core	Axial blanket	Radial blanket	
111	7.48520E 02	4.54000E 02	3.19340E-01	2.68915E-01	2.12913E-01	1.99558E-01	4.08576E-01	2.15957E-01	3.07685E-01
112	5.54000E 02	2.75360E 02	1.21361E-01	1.11413E-01	1.07911E-01	6.48102E-02	1.90405E-01	1.09012E-01	1.20691E-01
113	2.75360E 02	2.18450E 02	5.84086E-02	4.94097E-02	6.44040E-02	2.75699E-02	1.10152E-01	6.49291E-02	4.93779E-02
114	2.18450E 02	1.67020E 02	3.42831E-02	1.77798E-02	4.33093E-02	1.31416E-02	7.18386E-02	4.35686E-02	2.78573E-02
115	1.67020E 02	1.01300E 02	1.02740E-02	3.01249E-03	2.67765E-02	4.09943E-03	4.18347E-02	2.71862E-02	8.24889E-03
116	1.01300E 02	6.18420E 01	4.15999E-03	2.21683E-03	1.62537E-02	1.24906E-03	2.34746E-02	1.66535E-02	2.33709E-03
117	6.18420E 01	4.78510E 01	1.50119E-03	2.25116E-03	8.65924E-03	4.08375E-04	1.19488E-02	8.92884E-03	5.87919E-04
118	4.78510E 01	3.72670E 01	6.02553E-04	1.36736E-03	6.90654E-03	2.16358E-04	8.56439E-03	7.18967E-03	2.01945E-04
119	3.72670E 01	2.26030E 01	1.99748E-04	1.47544E-04	3.78834E-03	5.69945E-05	4.46830E-03	3.99596E-03	1.21854E-04
120	2.26030E 01	1.06770E 01	1.94001E-05	4.24033E-05	1.30925E-03	7.31025E-06	1.60463E-03	1.41750E-03	1.45234E-05
121	1.06770E 01	5.04350E 00	1.83439E-06	1.28431E-05	5.17834E-04	1.41263E-06	6.69292E-04	5.88470E-04	7.04249E-06
122	5.04350E 00	2.37239E 00	9.14399E-07	7.48579E-05	3.10709E-04	8.08493E-07	2.33503E-04	3.57272E-04	1.00392E-05
123	2.37239E 00	1.12540E 00	1.10007E-07	3.00548E-05	7.78112E-05	8.85669E-08	5.06734E-05	9.16377E-05	2.41081E-06
124	1.12540E 00	4.13990E-01	8.10654E-08	5.37057E-06	2.53803E-05	8.26383E-08	1.01821E-05	3.00933E-05	6.48793E-08
125	4.13990E-01	1.00000E-01	1.40312E-08	2.09827E-07	1.58314E-06	1.63569E-08	5.02846E-07	1.92663E-06	7.59713E-09
126	1.00000E-01	1.00000E-05	6.24785E-10	8.37382E-09	6.28890E-08	6.25750E-10	1.64719E-08	7.90473E-08	7.73024E-10

APPENDIX B:

ONE-GROUP, SPECTRUM-AVERAGED CROSS SECTIONS FOR THE
AMOPUUUX, AM02TTX, AND FFTF LMFBRs

Table B.1 (continued)

Isotope	Cross section type ^a	Cross section (barns)						
		AMOPUUUC	AMOPUUUA	AMOPUUUR	AMO2TTTC	AMO2TTTA	AMO2TTTR	FFTFC
CM-243	N,F	2.60E 00	3.65E 00	3.42E 00	2.33E 00	3.38E 00	3.17E 00	2.42E 00
CM-244	N,G	7.94E-01	1.29E 00	1.20E 00	6.69E-01	1.19E 00	1.12E 00	6.85E-01
CM-244	N,F	4.87E-01	3.09E-01	3.30E-01	5.25E-01	2.98E-01	3.10E-01	5.42E-01
CM-245	N,G	2.98E-01	4.48E-01	4.24E-01	2.56E-01	4.21E-01	4.00E-01	2.56E-01
CM-245	N,F	2.59E 00	3.28E 00	3.14E 00	2.42E 00	3.13E 00	3.00E 00	2.45E 00
CM-246	N,G	2.21E-01	3.99E-01	3.61E-01	1.77E-01	3.56E-01	3.21E-01	1.86E-01
CM-246	N,F	3.20E-01	1.73E-01	1.91E-01	3.52E-01	1.66E-01	1.77E-01	3.65E-01
CM-247	N,G	2.92E-01	4.53E-01	4.28E-01	2.50E-01	4.23E-01	4.01E-01	2.52E-01
CM-247	N,F	1.93E 00	1.95E 00	1.95E 00	1.94E 00	1.94E 00	1.94E 00	1.95E 00
CM-248	N,G	2.32E-01	4.70E-01	4.34E-01	1.84E-01	4.12E-01	3.87E-01	1.99E-01
CM-248	N,F	3.56E-01	2.14E-01	2.30E-01	3.87E-01	2.05E-01	2.16E-01	4.01E-01
BK-249	N,G	8.76E-01	2.27E 00	1.96E 00	5.58E-01	1.91E 00	1.65E 00	6.69E-01
BK-249	N,F	1.90E-01	1.03E-01	1.14E-01	2.09E-01	1.01E-01	1.08E-01	2.15E-01
CF-249	N,G	3.43E-01	5.98E-01	5.48E-01	2.77E-01	5.40E-01	4.94E-01	2.88E-01
CF-249	N,F	2.57E 00	3.49E 00	3.29E 00	2.33E 00	3.29E 00	3.11E 00	2.37E 00
CF-250	N,G	3.90E-01	8.22E-01	7.44E-01	2.97E-01	7.21E-01	6.63E-01	3.21E-01
CF-250	N,F	1.13E 00	8.45E-01	8.75E-01	1.21E 00	8.57E-01	8.80E-01	1.23E 00
CF-251	N,G	2.97E-01	4.86E-01	4.53E-01	2.50E-01	4.46E-01	4.19E-01	2.57E-01
CF-251	N,F	2.27E 00	2.76E 00	2.68E 00	2.16E 00	2.67E 00	2.62E 00	2.17E 00
CF-252	N,G	2.77E-01	4.43E-01	4.12E-01	2.34E-01	4.10E-01	3.83E-01	2.36E-01
CF-252	N,F	7.59E-01	8.29E-01	7.89E-01	7.40E-01	7.47E-01	7.03E-01	7.75E-01
CF-253	N,G	1.75E-01	4.78E-01	4.05E-01	9.66E-02	3.96E-01	3.28E-01	1.21E-01
CF-253	N,F	6.26E-01	1.53E 00	1.34E 00	3.81E-01	1.30E 00	1.11E 00	4.47E-01
ES-253	N,G	1.32E-01	4.46E-01	3.82E-01	6.82E-02	3.65E-01	3.18E-01	9.69E-02
ES-253	N,GX	9.18E-02	3.10E-01	2.66E-01	4.74E-02	2.54E-01	2.21E-01	6.73E-02
I/V	N,G	6.90E-04	1.13E-03	1.05E-03	5.70E-04	1.04E-03	9.59E-04	5.85E-04

^aN,G = (n,gamma) to a ground state.

N,F = (n,fission).

N,GX = (n,gamma) to an excited state.

N,A = (n,alpha).

N,P = (n,proton).



APPENDIX C:

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