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## AGTEHM: Documentation of Modifications to the Terrestrial Ecosystem Hydrology Model (TEHM) for Agricultural Applications

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ENVIRONMENTAL SCIENCES DIVISION  
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and

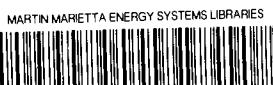
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## ABSTRACT

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terrestrial ecosystem hydrology model (TEHM) for  
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AGTEHM, an agricultural application version of TEHM, the Terrestrial Ecosystem Hydrology Model (Huff et al., 1977), is the outgrowth of over a decade of effort to realize a model of the complex interrelations of air, water, land, and vegetation. TEHM combines mechanistic algorithms for climatic and hydrologic processes with vegetation properties to explicitly simulate interception, throughfall, infiltration, root zone evaporation, transpiration, drainage, plant and soil water potential, unsaturated and saturated subsurface flow, surface runoff, and open channel flow. AGTEHM was developed from TEHM and several innovations have been added for agricultural applications. These include changes in the input data options, algorithms for sprinkler and flood irrigation, an alternative surface resistance-water potential relationship, a variable-contributing-area function, and the coupling of a model for soil macropore effects on water flow. Several internal changes to the original code have been made to increase calculation efficiency. This report is intended as a companion to the TEHM report and describes those features not previously documented.



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## I. Introduction and Rationale

The Terrestrial Ecosystem Hydrology Model (TEHM) documented by Huff et al. (1977) is a simulation code for the hydrologic processes of vegetated land in which the physical processes and physiological mechanisms of water and vapor transport are represented by deterministic equations. TEHM has been chiefly applied to forest watershed studies; however, it can also be applied to agricultural watersheds. In extending the range of TEHM applications to more diverse agricultural situations, a series of modifications have been introduced that are documented in this report as a model called AGTEHM. These changes involve (1) additional input data options, (2) irrigation algorithms, (3) an alternative leaf physiological algorithm, (4) a variable-contributing-area algorithm, and, (5) algorithms for water flow in soil macropores.

The TEHM code has an hourly time step (15 minute step during periods with rainfall or rapid soil water flow). Computation of hourly meteorological conditions from daily input data is conducted with simple algorithms for diurnal changes. In recent years some experiments have been performed for selected periods to measure plant variables while simultaneously measuring meteorological conditions at intervals of approximately an hour. Data with this detailed time resolution has become more common with the development of automated data sampling equipment. Provision needs to be made for entering such hourly data for detailed simulation of these experiments. While simulation for a period of one year may require as many as 8784 hourly values of each variable, the measured values are rarely available for such extensive

periods. Facility has been provided in AGTEHM for combining periods with hourly records with the standard daily data inputs of the TEHM code. In addition, algorithms have been added to AGTEHM to simulate daily averages for applications where daily data are incomplete or missing entirely. These changes in input data options greatly expand the types of applications that can be attempted, although care must be taken in the interpretation of simulations generated with default meteorological data.

Irrigation is an ancient agricultural practice that continues as a well established and important technology in current times. Sprinkler and flood irrigation systems have greatly improved agricultural productivity. Some problems in irrigation practice remain, however, especially water-borne pollutants originating from agricultural ecosystems. Incorporation of irrigation algorithms into the hydrology model will be useful for addressing these problems.

One of the most important relationships in the hydrologic model is between stomatal resistance and leaf-water potential. This function determines the partitioning of water between the liquid and vapor phases. An exponential function is used in TEHM and is not suitable for some agricultural crops. A hyperbolic function has been shown to be more appropriate in some cases (Reicosky and Lambert, 1978) and AGTEHM provides this function as an alternative to the original exponential form.

Two additional developments in the model concerning variable-contributing areas and soil macropores have been undertaken to simulate two hydrologic processes that are important during storm events or

excessive irrigation. Hewlett and Nutter (1970), Freeze (1972), and Bevan and Kirby (1979), among others, have investigated the role of variable-contributing areas through which the majority of watershed runoff passes during storm events. Soil macropores due to root channels, wormholes, and cracks between aggregates also have an important role in channeling water downslope during and after storm events. Thomas and Phillips (1979) have reviewed the hydrologic role of macropores, and simple algorithms have been included in AGTEHM for representation of channel-water flow through soil profiles. These various changes greatly extend the range of applications. Both the TEHM and AGTEHM are designed to be coupled with soil chemistry models. The improved treatment of soil-water-flow behavior will greatly improve the analysis of pollutant transport in forestry and agricultural ecosystems. The alternative input data options, irrigation algorithms, and the other code developments are documented in the following sections.

## II. Documentation of Modifications to TEHM

This section describes ten sets of programming changes that have been introduced in AGTEHM. Other minor modifications are discussed in the subroutine descriptions of Section III.

### A. Hourly Data Input and Default Algorithms

The format for the input of daily meteorological data is described in the documentation of TEHM (Huff et al., 1977; see pp. 85-91). Included here is a brief review and a description of the format for entering hourly data.

As in TEHM, each set of meteorological data (air temperature, dew point, solar radiation, and wind speed) is preceded by a data card which has an integer specifying a data type and a title or name of the type of data. This latter identification is used to make the listing of the data more readable and serves no other purpose. This data-type card is followed by an arbitrary number of data cards. The last data card is followed by a card with a dollar sign (\$) in column 1 which signals the end of this set of data.

Each data card begins with a seven-column field (see field F1 on hypothetical card given on page 6) which may be used to identify the data. Any descriptor not beginning with a dollar sign (\$) in column 1 may be used. The descriptor is not used internally in TEHM or AGTEHM. The descriptor is followed in columns 8-11 by two-digits signifying the year and two digits signifying the month of the subsequent data items (F2). Column 12 contains a single digit (F3) which, if 1, 2, or 3, indicates that the data items are for the first, second, or third 11 d

of the month. In AGTEHM an additional option is provided. If the digit is 4 it signals that hourly data follows.

Each string of hourly data is preceded by a two-digit integer day, two-digit integer starting hour, and a two-digit integer indicating the number of consecutive hourly data items to follow (F4, F6, F8). If the number of data items is zero the remainder of the card is ignored. If the number is nonzero, the string of data (F5, F7) may be followed by additional day-hour-number designators and data. A string of data cannot be continued from one data card to the next. The items in the data string are entered in groups of six columns (two groups of three columns in the case of temperature data) in FORTRAN F6.0 (or 2F3.0) format.

For example, to input hourly solar radiation data, the format would be as follows (see p. 90 of Huff et al., 1977):

For NBZ, BZ = 3 SOLAR RADIATION, the cards required for hourly data are:

| <u>Subroutine</u>                                    | <u>Card number</u> | <u>Columns</u> | <u>Description of Input Data</u>  |
|--|--------------------|----------------|---|
| ENTRY DAYIN<br>(alternate entry to subroutine BIMON) | 3.38 to ...        |                | FORMAT (A1, 6X, 2I2, I1, 11F6.0)  |
|  | 3.38               | 1-7            | X. May be used for identification purposes. The character \$ in column 1 signals that all daily radiation data have been read and control should return to subroutine GETSET. |
|  | 8-9                |                | Y, a two-digit integer signifying the year of input.  |
|  | 10-11              |                | M, a two-digit integer signifying the month of input.   |
|  | 12                 |                | K, = 4, signifying hourly input.  |

- 13-14      A two-digit integer signifying the day of month M.
- 15-16      A two-digit integer signifying the starting hour of the day that hourly input is available (the ordinal number of the hour - see below).
- 17-18      IN, a two-digit integer signifying the number of data items to follow (must be  $\leq 10$ ).
- 19-24      Hourly radiation for the first hour ( $\text{cal cm}^{-2}\text{h}^{-1}$ ).
- 25-30      Hourly radiation for the second hour if  $IN > 1$  ( $\text{cal cm}^{-2}\text{h}^{-1}$ ). There will be IN data items. For example, if  $IN = 3$ , then input the third data item in columns 31-36. The user can input another string of data as follows.
- ⋮
- 37-38      See columns 13-14 above.
- 39-40      See columns 15-16 above.
- 41-42      See columns 17-18 above, but now  $IN \leq 6$  (if  $IN = 3$  the first time).
- ⋮
- etc.

Additional data cards 3.39, 3.40, etc. have the same format as card 3.38. The last card in this section of data will have a \$ in column 1.

To illustrate further, consider the card (^ signifies blank),

|  |      |    |        |                                |                                |                                |                                |        |                           |      |  |
|--|------|----|--------|--------------------------------|--------------------------------|--------------------------------|--------------------------------|--------|---------------------------|------|--|
| <sup>^</sup> OR <sup>^</sup> TN <sup>^</sup> | 7807 | 4  | 130704 | <sup>^</sup> <sup>^</sup> 1.02 | <sup>^</sup> <sup>^</sup> 0.76 | <sup>^</sup> <sup>^</sup> 1.15 | <sup>^</sup> <sup>^</sup> 1.09 | 131401 | <sup>^</sup> <sup>^</sup> | 2.45 |  |
| F1   | F2   | F3 | F4     | F5                             | F6                             | F7                             | F8                             |        |                           |      |  |

The fields on the card signify as follows: F1 - Oak Ridge, Tennessee, F2 - July 1978; F3 - hourly data follows; F4 - July 13, begin with the hour ending at 7:00 AM, find 4 h of data; F5 - four data items; F6 - continue July 13 at 1:00 PM (14th h) find one data item; F7 - data item; F8 - end of data (number of following data items is zero). Observe that the number of the starting hour is the ordinal number of the hour.

To avoid the necessity of providing complete hourly data, or even hourly data for a full day, a hierarchical set of algorithms is used to enter data not otherwise specified. It is not necessary that daily data be chronologically ordered. However, for each set of meteorological data (i.e., air temperature, dew point, solar radiation, and wind speed), all daily data must be entered before any hourly data. These daily quantities are used to compute hourly values. The computed hourly values are then overwritten by the subsequent hourly data input. In other words, the code will not function properly if only hourly data are read.

It is stressed here that the daily data are read or computed for 11-d intervals. That is, if available, the daily data for the first 11 d of a month are read in on one card, the second 11 d on a second card, and the data for the remaining days of the month on a third card (Huff et al., 1977; see pp. 89-90). Therefore, daily data cannot be read in for only part of an 11-d interval; the code assumes the data for this interval are complete and will not calculate the missing data. Hence, if the data for any interval are incomplete, do not read any data at all for that interval, and AGTEHM will compute the data for

the 11 d (or less if the last third of the month) using the appropriate internal algorithm (see below). AGTEHM calculates the hourly values from the computed daily values during simulation.

#### B. Algorithm for Average Daily Temperature

The average daily temperature at a site varies with the slope of the land, soil type, vegetation, nearness to bodies of water, and air drainage as well as with season, latitude, and altitude. The equation used includes only the three latter effects.

The equation was developed from charts of normal average daily temperature by month in North America published in the "Weather Atlas of the United States" (1968). Use of the function should be limited to the range from 25° to 55° North latitude on the North American continent. The mean daily temperature T (in Fahrenheit degrees) is given by

$$T = 117 - 1.60L + (12.2 - .925L) \cos (.0172(D-20)) - .0015A , \quad (1)$$

where L is the North latitude in degrees, D is the Julian date, and A is the altitude above mean sea level in feet. Of the constants, ".0015" is the average lapse rate in °F/foot, ".0172" is  $2\pi/365.25$  and "20" represents a lag of about one month from the winter solstice. The remaining constants are empirical, derived from an analysis of the weather charts. The mean daily temperature variation has a small seasonal variation and varies with terrain slope and elevation as well

as other factors mentioned previously. Away from bodies of water the mean daily temperature variation ( $^{\circ}$ F) can be taken to be

$$\Delta T = 20 + .0013 A \ ^{\circ}\text{F} , \quad (2)$$

where A is again the altitude in feet. This estimate also came from an analysis of the weather maps. The mean temperature and its variation allows calculation of the maximum and minimum temperatures which are actually needed in AGTEHM.

The hourly variation of temperature is described in TEHM (Huff et al., 1977; see pp. 8-9), and follows an empirical curve. In qualitative terms, the temperature rises sinusoidally from a minimum at sunrise with a 1-h lag behind that of incident solar radiation. The deviation from sinusoidal behavior increases in the afternoon, and after sunset the temperature decays approximately exponentially to the minimum value of the following morning.

### C. Algorithm for Humidity

While the relative humidity may vary considerably during a typical day, the absolute humidity expressed as a dew point temperature is relatively constant. Daily average dew point temperature is approximately equal to the minimum daily temperature with a daily variation of about  $3^{\circ}\text{F}$ . In the absence of any humidity data, the average dew point is taken to be equal to the minimum temperature for the day.

When the average dew point is  $3^{\circ}\text{F}$  or more below the minimum temperature for the day, an hourly dew point equal to the average is

assigned. When the average dew point is higher than this a different procedure is used. If the temperature falls below the dew point, moisture will ordinarily condense as fog or dew lowering the dew point. Thus, the hourly dew point is assigned a value lower than the hourly temperature. To preserve the definition of the average, a "dew-point-hour" total is defined for the day equal to the average dew point times 24 h. Starting with the hour with minimum temperature, a dew point is assigned equal to the smaller of (1) the air temperature values less 3°F or (2) the number of dew point hours divided by the number of hours with as yet unassigned dew points. This dew point times 1 h is subtracted from the total number of dew point hours, and the remaining hour with the lowest temperature is chosen to repeat the process.

#### D. Algorithm for Incident Solar Radiation

From purely geometric considerations, one can calculate the potential solar radiation incident on an area above the earth's surface as in the algorithm of Swift (1973) used in TEHM. A simplified model of the transmission of the earth's atmosphere in the absence of clouds uses the transmission factor  $T = e^{\alpha\ell}$ , where  $\alpha$  is an attenuation coefficient and  $\ell$  is an appropriate optical path length. The attenuation coefficient  $\alpha$  is determined from the relation,

$$\alpha h = \log T_0, \quad (3)$$

where  $T_0$  is the fraction of the direct potential solar radiation reaching the earth's surface on a clear day when the sun is at the

zenith with an optical path length (or atmospheric thickness)  $h$ . The value  $T_0 \approx 0.90$  was found for one set of measured data from which  $\alpha h \approx -0.106$ . Assuming a flat earth with the sun at an angle  $\Psi$  (radians) from the zenith, then  $\ell = h \sec \Psi$ . Including the earth's curvature,

$$\frac{\ell}{h} = \frac{2 + h/R}{\cos \Psi + \sqrt{\cos^2 \Psi + (h/R)(2+h/R)}} , \quad (4)$$

where the law of cosines was applied to the triangle as seen in Fig. 1 ( $\ell/h$  is dimensionless).  $R$  is the earth radius and  $h$  the atmospheric thickness; variation of density of the air with altitude can be neglected when  $h \ll R$ .

The mean daily atmospheric transmission is approximated by

$$I = I_0 e^{\alpha \ell} = I_0 e^{(\alpha h \ell / h)} = I_0 T_0 (\ell/h) \quad (5)$$

using the previous expression for  $\ell/h$  and approximating  $\Psi$  by the angle of the sun from the zenith at local solar noon. Here,  $I_0$  is the daily potential radiation above the atmosphere.

The effects of cloud cover are calculated by the expression

$$S = S_i [(1 - C) + kC] \quad (6)$$

from Sikov (1971) using sky cover estimates from local climatological data.  $S_i$  is the solar radiation incident on the clouds,  $C$  is the fraction of the sky covered with clouds, and  $k$  is the transmission through clouds. Sikov suggests the value  $k \approx .32$  for  $25^\circ$  to  $35^\circ$  North latitude.

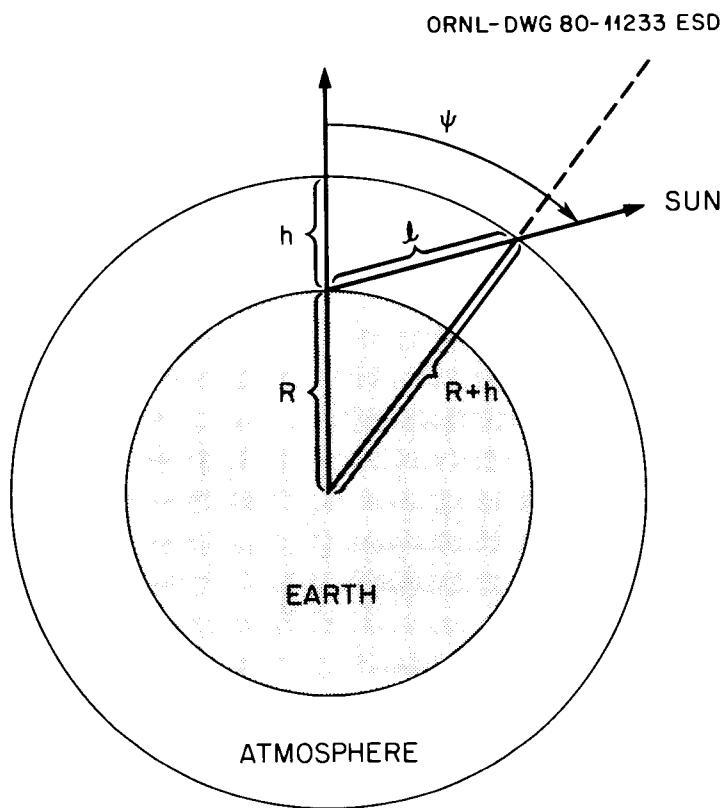


Fig. 1. Variables used in calculations with the incident solar radiation algorithm.  $R$  is the earth's radius,  $h$  the atmospheric thickness,  $l$  the optical path length, and  $\Psi$  the angle of the sun from the zenith.

When no solar radiation data are available, the total daily radiation on a horizontal slope is calculated assuming a nominal 10% of the sky is covered with clouds ( $C = 0.10$ ) and the cloud transmission is 32%. While solar radiation data are not usually available, average daily cloud cover at 3-h intervals is available from most weather stations. A program which reads average daytime cloud cover and computes average daily radiation is given in appendix A.

#### E. Algorithm for Average Daily Wind Speed

Annual average wind speeds vary considerably across the North American continent. The average wind speed is highest in the spring when temperatures are increasing rapidly. Examination of average climatological data shows that the annual variation is approximately 40% of the annual average wind speed. The algorithm for wind speed used is

$$V_w = V_a (1 + .2 \cos (.172 (D - 70))) , \quad (7)$$

where  $D$  is the Julian date and  $V_a$  is the annual average wind speed (mph).  $V_a$  varies typically between 6 and 16 km/h (4 and 10 mph). A value of 9.7 km/h (6 mph) is used in AGTEHM, in the model above, in the absence of input wind speed data.

#### F. Data Input for Sprinkler and Flood Irrigation

For agricultural applications a natural and necessary extension of the TEHM model is to include provisions for irrigation. A feature of irrigation in non-arid areas is that the time during which irrigation is actually in use is a small fraction of the total growing period. This fact is reflected in the way in which the irrigation data is

managed in the AGTEHM program. The irrigation data is stored by month in a compact form. At the start of the simulation of each day the irrigation data for that month is checked and any data pertinent to that day is copied into an array of hourly values.

Irrigation data are entered along with the climatic variables for a given land segment; see the description of the TEHM input data (Huff et al., 1977; see pp. 85-107). The irrigation data are preceded by a data-type card, 17 IRRIGATION, read with format (2I, 1X, A4). The next card reads a parameter called FIRRG in F6.0 format. FIRRG is the effective fraction of the segment surface that is being irrigated. For example, FIRRG would be less than 1.0 if the land is furrow irrigated (flooded irrigation). Set FIRRG equal to 1.0 if sprinkler irrigation is used. These cards are followed by any number of data cards and the set of irrigation data is terminated by a card with a dollar sign (\$) in column 1. The format is as follows:

| <u>Subroutine</u> | <u>Card number</u> | <u>Columns</u> | <u>Description of Input Data</u>   |
|-------------------|--------------------|----------------|--|
| RDIRIG            | 17.1 to ...        |                | FORMAT (A1, 6X, 2I2, 1I, 1F6.0)  |
|                   | 17.1               | 1-7            | X. May be used for identification purposes. The character \$ in column 1 signals that all irrigation data have been read and control should return to subroutine GETSET. |
|                   | 8-9                |                | Y, a two-digit integer signifying the year of input.   |
|                   | 10-11              |                | M, a two-digit integer signifying the month of input.  |
|                   | 12                 |                | K, a one-digit integer signifying the type of irrigation used. K can be equal to 1 (sprinkler), 2 (flood), or 3 (flood) as explained below.                              |

- 13-14      A two-digit integer signifying the day of month M.
- 15-16      A two-digit integer signifying the starting hour of the day with available hourly input. (This is the ordinal hour number - see example below).
- 17-18      N, a two-digit integer signifying the number of data items to follow if K = 1 or 2 ( $N \leq 10$ ). If K = 3, N is the number of hours that water stands on the surface (see below).
- 19-24      If K = 1 or 2, the input is the irrigation amount (inches) for the first hour (see explanation of K below). If K = 3, these columns would be like columns 13-18 above if data are available, or blank.
- 25-30      If K = 1 or 2 (and  $N > 1$ ) the input is the irrigation amount (inches) for the second hour. There will be N data items. For example, if N = 3, then input the third data item in columns 31-36. The user can input another string of data as follows. (If K = 3, these columns would be like columns 13-18 above if data are available, or blank.)
- :
- 37-38      See columns 13-14 above.
- 39-40      See columns 15-16 above.
- 41-42      See columns 17-18 above, only now  $N \leq 6$  (if N = 3 the first time).
- :
- etc.

Additional data cards 17.2, 17.3, etc. have the same format as card 17.1. The last card in this section of data will have a \$ in column 1.

To explain further, the first seven columns (see field F1 of the hypothetical card below) are not used by the program and may be used for identification purposes but must not contain a \$ character in column 1. The next four columns (F2) identify the year (76) and month (06), and the following column (F3) is the type of irrigation used (described below via the variable K).

The next six columns (F4) are interpreted as three two-digit numbers (15, 09, 02 in example below) and (when K = 1 or 2; see below) identify the string of actual irrigation data (F5) which follows. In the example below, 15 identifies the day, 09 the starting hour, and 02 the number of hourly irrigation amounts to follow. After the 02 hourly amounts (inches of water) are read, the next six columns are treated as a new identifier (F6). Here, 17 identifies the day, 09 the starting hour, and 02 the number of hourly irrigation amounts to follow. If these columns are blank, zero, or an invalid identifier (F8), the remainder of the card is ignored. Data on each card must be in chronological order.

Three types of irrigation are recognized, but all data on a given card are treated as the same data type. When K = 1 (see F1) the data are taken to be sprinkler irrigation and are treated like precipitation. When K = 2 the data represent irrigation by flooding with the application amount specified. This water is routed directly to the land surface, bypassing interception storage and impervious areas. When K = 3 flooding is again assumed; however, in this case

infiltration is determined by specifying the number of hours N (the last 2 columns of field F4) with water standing on the surface. The amount of infiltration is then determined internally by AGTEHM. In this case hourly identifiers (F4) follow one after another with no intervening data.

Consider the following example. If on June 15 and 17 of 1976 a field of corn near Florence, South Carolina was irrigated by sprinklers starting at 8:00 AM for two hours each day at a rate of 0.254 cm (0.10 inches) of water per hour, this might be specified on a data card by:

(^ signifies blank)

|         |      |    |        |               |        |             |    |
|---------|------|----|--------|---------------|--------|-------------|----|
| FSC-CRN | 7606 | 1  | 150902 | ^0.10 ^0.10 ^ | 170902 | ^0.10 ^0.10 |    |
| F1      | F2   | F3 | F4     | F5            | F6     | F7          | F8 |

The similarity to the hourly data format is so obvious that the differences should be made clear. All irrigation data are hourly so the variable K in column 12 is interpreted as irrigation type. When K = 3, the value N (columns 17-18) is the datum (i.e., number of hours that surface is flooded) rather than delimiting the data as in the cases where K = 1 or 2.

#### G. PROSPR Subroutine Modifications for Flood Irrigation

When there is flood irrigation (K = 2 or 3), no lateral flow or surface runoff is allowed in subroutine PROSPR. The soil layers are allowed to become saturated, but any excess water will remain on the surface at each time step. Within PROSPR, a check is made for the presence of irrigation water (by flooding) on the surface. If there is

surface water, the normal top to bottom calculations for the volumetric water content of each of the soil layers, surface runoff, lateral flow, and drainage to the groundwater are bypassed (Huff et al., 1977; see pp. 24-33), and PROSPR computes the soil water properties starting with the deepest soil layer. This was introduced to prevent lateral flow during flood irrigation. The first step in this reverse sequence is the calculation of drainage to the groundwater from the bottom layer. The volumetric water content of the deepest layer is calculated as usual. If the layer becomes saturated, the soil water entering the bottom layer from the layer above is limited to the amount that can drain out of the bottom layer. Thus, no lateral flow is allowed. Each soil layer is treated in the same way, i.e., when a layer becomes saturated, the amount entering from above is limited to the water that can drain into the soil layer below. At the surface no runoff is allowed and any excess irrigation water on the surface is saved for the next time step. When flood irrigation ceases ( $K \leq 1$ ) and all remaining irrigation water on the surface is zero, PROSPR proceeds as before (from top to bottom) allowing lateral flow and surface runoff.

Sprinkler irrigation follows the normal series of calculations (i.e., the same as for precipitation). See Fig. 2 for comparison between sprinkler and flood irrigation calculations by the PROSPR routine.

#### H. Algorithm for Stomatal Resistance vs Leaf-Water Potential

One of the most important factors influencing transpiration rates is the leaf stomatal resistance. Two important environmental factors

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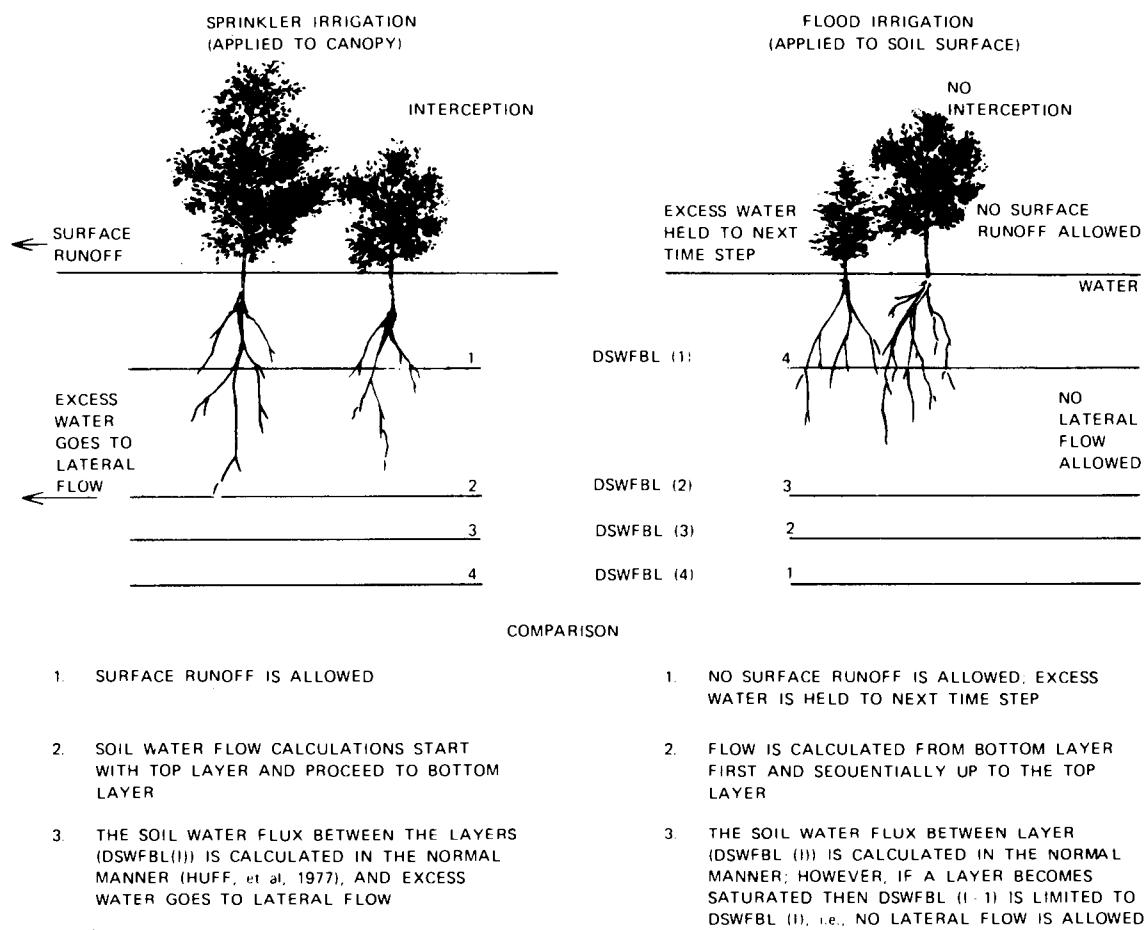


Fig. 2. Comparison of sprinkler and flood irrigation calculation sequences within subroutine PROSPR.

affecting the stomatal resistance during the growing season are the leaf-water potential and sunlight. The functional relation used in TEHM between the stomatal resistance and leaf-water potential is given by

$$r_s = \begin{cases} r_s(\min), & \Psi_\ell > 0.0 , \\ r_s(\min) + (r_s(\max) - r_s(\min)) \exp (\alpha(\Psi_\ell + \Psi_\ell(\max))), & -\Psi_\ell(\max) < \Psi_\ell < 0.0 , \\ r_s(\max), & \Psi_\ell < -\Psi_\ell(\max) . \end{cases} \quad (8)$$

These symbols (with their FORTRAN names given in parentheses) are:

$r_s$  (RRR) is leaf stomatal resistance,  $r_s(\min)$  (TM) is a minimum stomatal resistance,  $r_s(\max)$  (RESMAX) is a maximum stomatal resistance,  $\Psi_\ell$  (LWPA) is the leaf-water potential and is negative,  $\Psi_\ell(\max)$  (PWPMAX) is the leaf-water potential at which the maximum resistance is obtained (input as absolute value), and  $\alpha$  (POWER) is a negative number. Under dark conditions  $r_s$  is set equal to  $r_s(\max)$ . Figure 3a shows the relation among these variables.

Field data for corn stomatal resistance obtained for a range of leaf-water potentials were fitted to a hyperbolic function (Reicosky and Lambert, 1978) with the following form,

$$r_s = \begin{cases} \frac{r_s(\min)}{1 + \Psi_\ell/\Psi_\ell(\max)} , & \Psi_\ell > \tilde{\Psi}_\ell(\max) , \\ r_s(\max) , & \Psi_\ell < \tilde{\Psi}_\ell(\max) , \end{cases} \quad (9)$$

$$\text{where } \tilde{\Psi}_\ell(\max) = \Psi_\ell(\max) \left( \frac{r_s(\min)}{r_s(\max)} - 1 \right) . \quad (10)$$

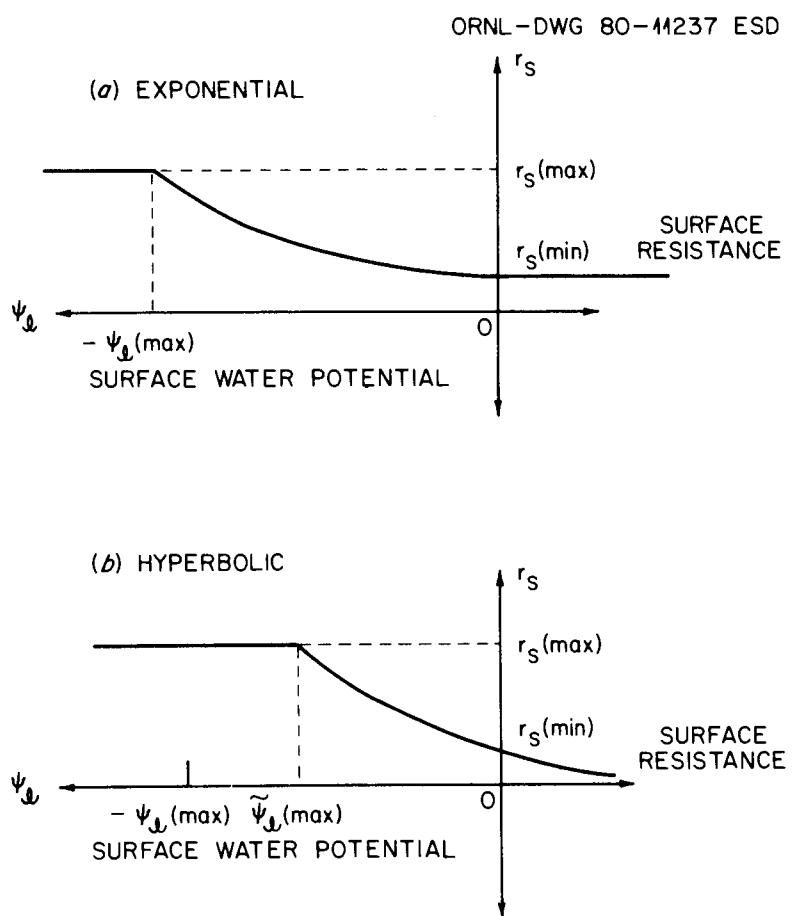


Fig. 3. Exponential (a) and hyperbolic (b) relationships between stomatal resistance ( $r_s$ ) and surface-water potential ( $\psi_l$ ).

Figure 3b shows a graph of the function. As with the first model, under dark conditions the resistance is set to  $r_s(\max)$  (RESMAX). The values of  $r_s(\max)$ ,  $r_s(\min)$ , and  $\Psi_l(\max)$  vary seasonally between values specified on data cards which are part of the input data block beginning "07 READIN." Formats are as described in the documentation of TEHM except that a new variable, LRMODL, is read in I5 format from columns 61 - 65 on card number 7.12 (Huff et al., 1977; see p. 99). A blank or "0" in column 65 selects the original "exponential model" while a "1" in column 65 selects the "hyperbolic model" for the stomatal resistance.

#### I. Algorithm for Variable Contributing Areas

The original version of TEHM (Huff et al., 1977; see pp. 34-37) contains an algorithm to account for lateral diversion of soil drainage to represent the subsurface runoff (interflow) contributions to stream flow during storm events. This algorithm (found in subroutine PROSPER) caused an increasing proportion of vertical soil drainage to be diverted to the stream with increase in soil drainage rate. This lateral diversion is represented by a ramp function (Fig. 4a). A similar function is used in AGTEHM to represent variable contributing areas with direct surface runoff during storm events. The size of the contributing areas is determined by the same subsurface drainage rate used in TEHM for interflow. To ensure a smooth change in the area size during rain storms, a moving average of the contributing area parameter over three time steps is computed. The net effect is that an increasing proportion of infiltration is diverted directly to the stream as

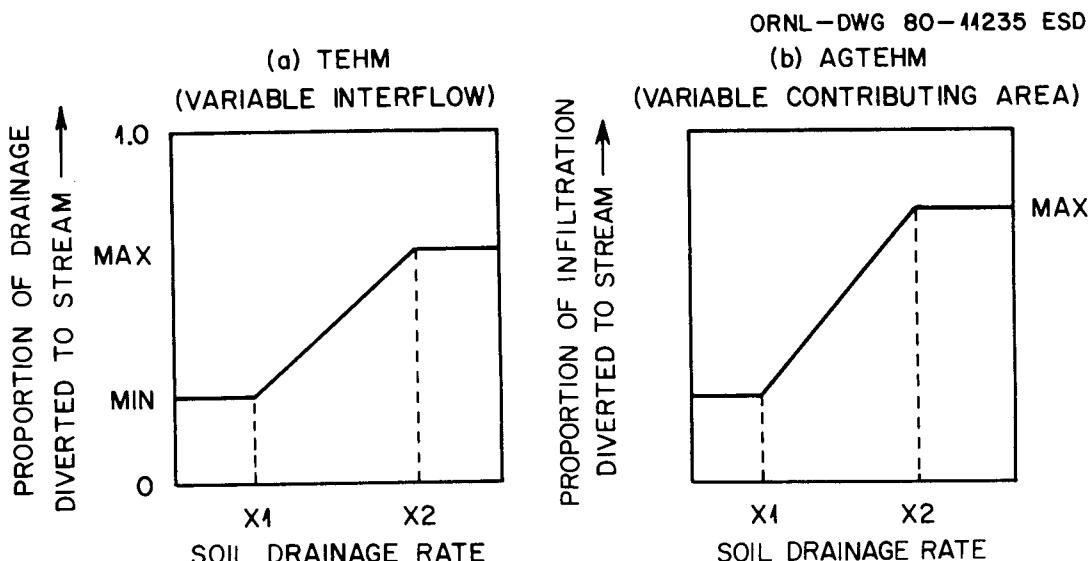


Fig. 4. Comparison of the TEHM and AGTEHM runoff algorithms.

#### COMPARISON

- 1. Constant impervious area with direct surface runoff to stream.
- 2. Infiltration enters whole watershed segment area.
- 3. A variable proportion of drainage between the A and B horizons is diverted to stream during storms. The remaining drainage enters whole segment area B horizon.\*
- 4. Additional subsurface lateral flow is generated from drainage into saturated soil layers.
- 1. Constant impervious area with direct surface runoff to stream.
- 2. Variable proportion of infiltration diverted to stream during storms. The remaining infiltration enters whole segment area.\*
- 3. All soil drainage percolates to groundwater.
- 4. Subsurface lateral flow to stream is generated from drainage to saturated soil layers.

\*NOTE: This provides a quasi-lateral redistribution of soil water.

additional surface runoff (i.e., in addition to that already calculated by the infiltration function in subroutine RAATS) with increase in soil drainage rate during storm events (Fig. 4b). Basically, AGTEHM partitions the incoming infiltration at an earlier stage than TEHM, i.e., at the soil surface rather than at the top of the B-soil horizon. The AGTEHM approach has conceptual similarities with variable-source-area behavior as described by Hewlett and Nutter (1970) and as simulated by Freeze (1972). Although both the TEHM and AGTEHM can be tuned to provide agreement between measured and simulated hydrographs, the difference in the water flow routing would show large differences when coupled with chemical transport simulation models.

The parameters defining the ramp function in AGTEHM have the same names and are read in the same sequence and format as the TEHM ramp function parameters (Huff et al., 1977; see p. 103). This format is repeated for convenience.

| <u>Subroutine</u> | <u>Card number</u> | <u>Columns</u> | <u>Description of Input Data</u>   |
|-------------------|--------------------|----------------|--|
| GETSET            |                    |                | FORMAT (10D8.0)<br>AREAL; the minimum (fractional) size of contributing areas (suggested value = 0.01 if not known). |
|                   | 8.1                | 1-8            |  |
|                   |                    | 9-16           | CUT; the drainage rate (cm/day) from contributing areas when their maximum extent is reached.                        |
|                   |                    | 17-24          | CUTL; the minimum drainage rate (cm/day) for contributing areas to contribute to streamflow.                         |
|                   |                    | 25-32          | WUP; the maximum (fractional) size of contributing areas.<br>AREAL $\leq$ WUP $\leq$ 1.0..                           |

33-40        RNTL; the number of soil-water transmission layers between the saturated zone and the region simulated by PROSPR (< 5).

A printout of the contributing area dynamics during storm events can be obtained with an input data switch called ISWIWT. If ISWIWT is nonzero, and if the size of the contributing areas (parameter WT in code) is greater than AREA1 (see above), then the program will write out the value of WT along with the corresponding day, hour, and minute. The variable ISWIWT is read in I5 format from columns 26-30 on card number 6.1 (Huff et al., 1977; see pp. 92-93). If a "1" (or nonzero number) is typed in column 30, the code will print the information about the contributing area dynamics during storm events. This information will not be printed if a "0" is entered in column 30 or if columns 26-30 are left blank.

It is anticipated that alternatives to the ramp function could be used for the variable-contributing-area algorithm to represent differing hydrologic behavior of watersheds with differing slope complexity. Some conceptual functions (Fig. 5) for landscape segments of a watershed with differing permeability and slope complexity would be expected to show greatly different variable-contributing-area behavior during storm events. Recent work by Beven and Kirkby (1979) have shown that geometrical analysis of a watershed can provide a useful basis for prediction of variable-contributing-area behavior.

#### J. Macropore-Mesopore Soil Water Flow Option

Algorithms for describing the channeling flow of water through soil profiles have been coded into three subroutines (SWIFT, RSWIFT,

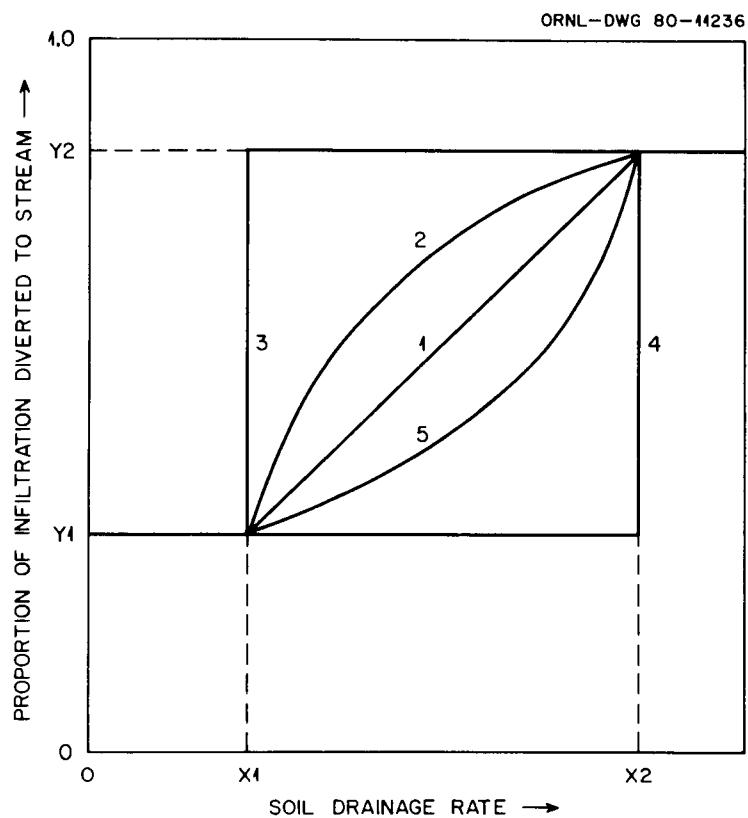


Fig. 5. Conceptual variable-contributing-area relationships for six landscape units where  $X_1$  is the soil drainage rate for minimum infiltration diversion ( $Y_1$ ) and  $X_2$  is the soil drainage rate for maximum infiltration diversion ( $Y_2$ ). The landscape units are (1) wedge (2D convergence), (2) piece of pie (3D convergence), (3) crusted surface, (4) sandhill, and (5) delta (3D divergence).

WSWIFT) and coupled to AGTEHM. The rationale and documentation of this development is given by Fong and Appelbaum (1980) and a brief outline is given here for user convenience.

Definitions are as follows:

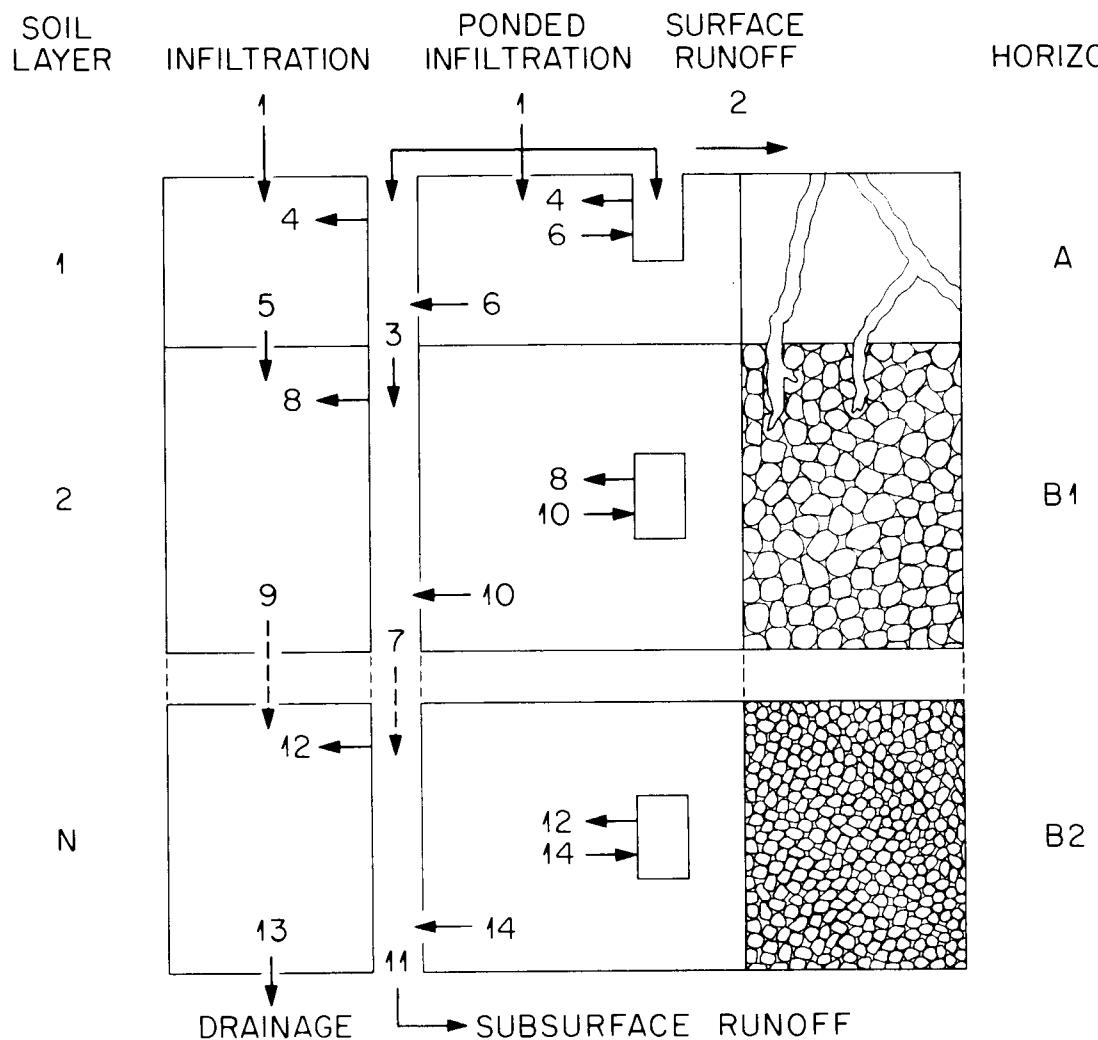
- (i) Macropores are large holes or cracks in soil that are water filled at suctions less than 0.3 kPa (3 cm of water, pore diam > 1 mm; crack width > 0.5 mm).
- (ii) Mesopores are pores that are water filled at suctions between 0.3 and 30 kPa (3 and 300 cm of water).
- (iii) Micropores are water filled pores at suctions greater than 30 kPa (field capacity).

The basic flows considered in the model (Fig. 6) include continuous and dead-end macropores. Continuous macropores pass between soil layers and dead-end macropores exist as reservoirs within a soil layer.

The following assumptions were made in the macropore-mesopore model:

1. Flow rate within macropores is rapid and not controlled by geometrical factors. At each time step, macropore flow between soil layers is the lesser of the macropore water content or the capacity to accept additional macropore water in the lower layer.
2. Flow from macropores to mesopores is controlled by the hydraulic properties of the mesopore matrix using cylindrical and linear flow equations for cylinders and cracks, respectively.

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 **FLOWS**

|                                |                                 |
|--------------------------------|---------------------------------|
| macropore to macropore 3, 7    | mesopore to macropore 6, 10, 14 |
| macropore to mesopore 4, 8, 12 | mesopore to mesopore 5, 9       |

Fig. 6. Continuous and dead-end macropore components in a mesopore matrix showing sequence of flow calculations.

3. Flow from mesopores to macropores results from the excess water entering mesopores above the saturation value.
4. Excess water in the continuous macropore system becomes subsurface runoff (Whipkey, 1967) and enters the stream channel.
5. Drainage from the mesopores enters the deep soil transmission zones and eventually percolates into ground water.

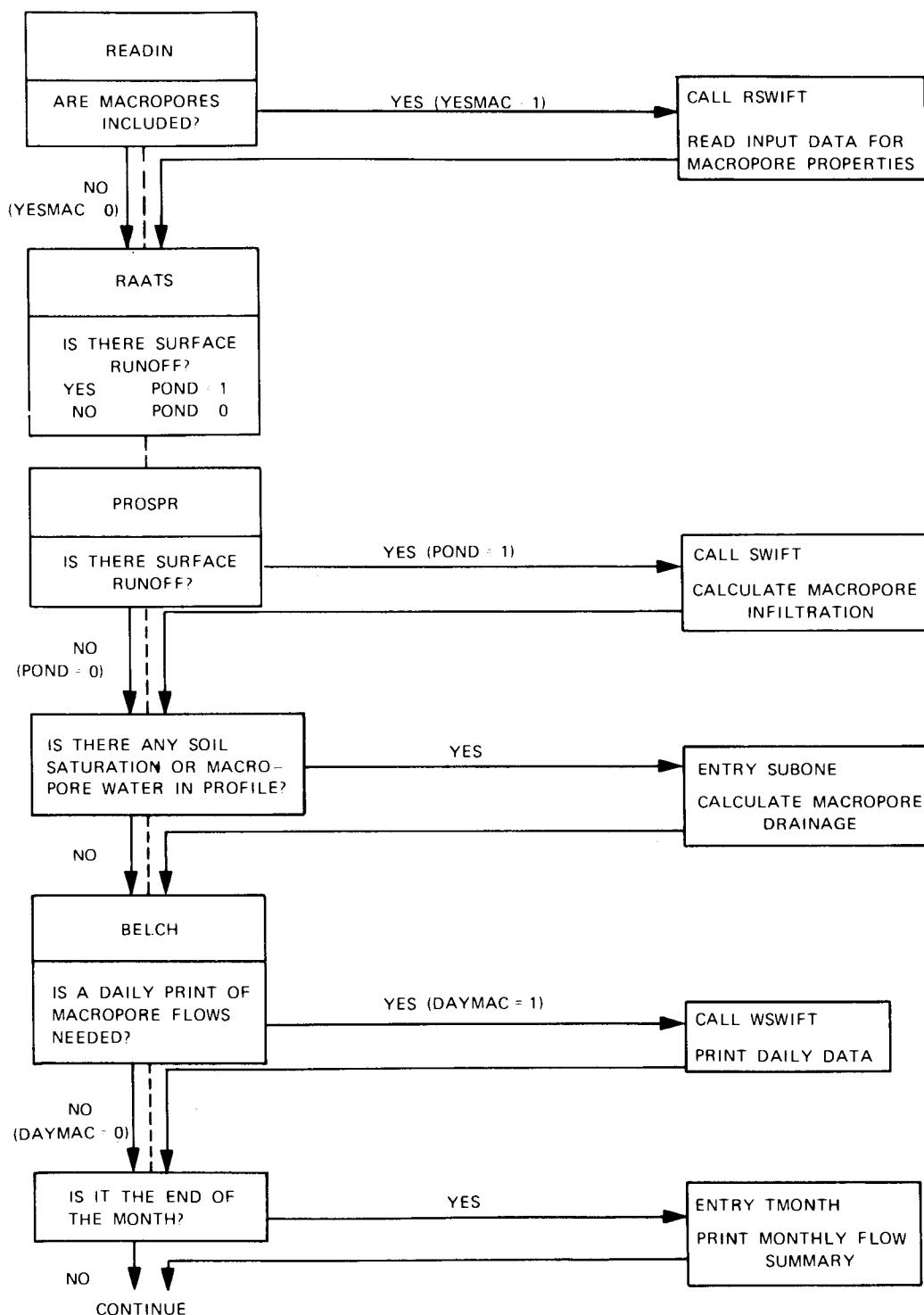
Subroutine RSWIFT is called in subroutine READIN if the macropore option is to be used. The input data for each soil layer are read by RSWIFT and some initial parameter values calculated. The flow calculations of macropore-mesopore drainage are conducted in SWIFT (including a subroutine entry, SUBONE) during periods of surface ponding and perched water tables (saturated zones) within the profile. Daily and monthly summaries of mesopore and macropore flow are printed from subroutine WSWIFT which is called from BELCH. The AGTEHM model can be executed with or without the macropore effects depending on the condition of a flag variable (YESMAC). A logic flow chart (Table 1) outlines the basic procedures involved.

The following give descriptions of the input data required for the macropore-mesopore option. The format here is the same as that used in the TEHM report (Huff, et al., 1977; see pp. 99, 103).

| <u>Subroutine</u> | <u>Card Number</u> | <u>Columns</u> | <u>Description of Input Data</u>  |
|-------------------|--------------------|----------------|---|
| READIN            | 7.11               | 31 - 40        | FORMAT (2G10.3, 2I5, 2F10.0)<br>YESMAC; flag for macropore flow effects.<br>YESMAC = 0.0 for no macropore effects.<br>YESMAC = 1.0 for macropore effects. |

Table 1. Flow chart of the interrelations between the hydrologic model and the macropore subroutines.

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|                                   |                          |   |
|-----------------------------------|--------------------------|---|
|                                   | 41 - 50                  | DAYMAC; flag for daily macropore flow print out.<br>DAYMAC = 0.0 for no daily macropore flow print out.<br>DAYMAC = 1.0 for daily macropore flow print out. |
| RSWIFT<br>(Called<br>from READIN) | 7.33<br>to<br>7.32 + NSL | FORMAT (6F10.4); one card per soil layer for NSL soil layers.   |
|                                   | 1 - 10                   | MCPOR; macroporosity of the layer (m <sub>1</sub> /m <sub>1</sub> ).  |
|                                   | 11 - 20                  | RP; radius of cylindrical pores if in A-horizon (cm) (put 0.0 for B-horizon).   |
|                                   | 21 - 30                  | WP; width of cracks if in B-horizon (cm) (put 0.0 for A-horizon).   |
|                                   | 31 - 40                  | PL; breadth of cracks if in B-horizon (cm) (put 0.0 for A-horizon).   |
|                                   | 41 - 50                  | PERC; proportion of dead-end macropores.  |
|                                   | 51 - 60                  | AGSIZE; average length of aggregate (cm).   |

### III. Subroutines Modified or Added to TEHM to Obtain AGTEHM

The following gives a summary of the subroutines in TEHM that were modified and of those that were added. The reader is referred to Appendix B which contains a listing of the subroutines. The job control language (JCL) used to submit a job to the ORNL IBM computer is given in Appendix D.

#### A. Changes in Subroutine ANUDAY

Modifications were made in the calling sequence and in the common statements ANGLES and HRLYS to handle parameters for irrigation and hourly radiation on the slope. The hourly radiation on the slope is now determined by calling subroutine HRADSL and passing the result back to subroutine LAND in array HNRAD. Calculations of the cloud cover factors PERMAX, CLD, and STCLD were changed. The daily radiation is now compared with the potential radiation calculated by FUNCTION SOLRAD rather than the previous sinusoidal model. This allows correct variation with latitude. Irrigation data contained in array PKIRIG (see Subroutine RDIRIG below) are examined to see if irrigation water was added during the day. If so, the hourly irrigation values are returned in the array HIRIG.

#### B. Changes in Subroutine ANUMON

The AGTEHM version of ANUMON calls subroutine MONDAT to compute the hourly model climatological data for the entire month, whereas ANUMON in TEHM calculated these data itself.

#### C. Changes in Subroutine ANUSEG

The parameter SASTOR was initialized to 0.0D0 and added to the common SRFSUM. Several lines of code, an artifact from an earlier TEHM version, were commented out. These lines involved computation with some variables which are uninitialized and unused in the present version of AGTEHM.

#### D. Changes in Subroutine ASPECT

The two variables DGLAT and DLONG were added with common ANGLES. These variables are the latitude and longitude of the site, respectively, in decimal degrees and are calculated in subroutine GETSET (see below). Also, ASPECT has been changed from the TEHM version to make it more efficient.

#### E. Changes in Subroutine BELCH

Two common statements (PIECES and BOOKS) and two subroutine calls (WSWIFT and TMONTH) were introduced into BELCH for the macropore water flow option.

#### F. Subroutine CHKCIF

Subroutine CHKCIF was written and added to AGTEHM to check the "smoothness" of the cumulative infiltration curve. The cumulative infiltration curve is read in as input data by subroutine READIN (Huff et al., 1977; see p. 103) and READIN then calls CHKCIF. The smoothness of the curve must be checked since, during execution, Lagrangian interpolation is used to calculate the cumulative infiltration for a given simulation time (or the equivalent time for a given cumulative infiltration). The interpolation uses the three "closest" points from

the cumulative infiltration curve. Thus, erroneous results could occur if this curve is not smooth (e.g., a parabola could be calculated). The algorithm used by CHKCIF takes the derivative of the Lagrangian polynomial through the first three points of the cumulative infiltration curve, sets it to 0.0, and solves the resulting equation to find the extrumum. If the extrumum lies outside the bounds of the three points, the test is satisfied, and CHKCIF continues by checking the second through fourth points of the curve. CHKCIF marches up the curve until the last three points are checked. If any three successive points fail the test, i.e., the interpolated curve is not monotonic within the bounds of the three points, then CHKCIF immediately stops execution and an error message is printed. For user convenience, the cumulative infiltration data can be checked separately using the utility program given in Appendix A.

#### G. Changes in Subroutines CLEAR0 and CLEAR2

CLEAR0 and CLEAR2 are used to load the labeled COMMON storage into regions of core that have been cleared to zero values (Patterson et al., 1974). Changes that were made to obtain AGTEHM enabled CLEAR0 and CLEAR2 to reduce the amount of storage that needed to be used.

#### H. Subroutine DEFER

DEFER is a subroutine that has been added and is called from subroutine MONDAT. It is used to write and retrieve a month's data from storage.

### I. Changes in Subroutine EVAL

EVAL was modified to include the algorithm for the hyperbolic relationship between stomatal resistance and leaf-water potential (discussed in Chapter II). Originally, only an exponential model was allowed, which was not suitable for some agricultural crops. If the variable LRMODL is read in as "0" the exponential algorithm is used and if read in as "1" the hyperbolic model is used. Refer to Chapter II for the details.

### J. Changes in Subroutine GETSET

The two variables DGLAT and DLONG were added to the common ANGLES. These variables, the latitude and longitude of the site in decimal degrees, are computed just prior to calling subroutine READIN from values which were entered with the precipitation data and were stored in LAT(3) and LONG(3) as integer degrees, minutes, and seconds. The TEHM version passes only the integer degrees to ASPECT in variable ELONG in common LOCATE.

Modifications were made to allow reading of irrigation data preceded by a data type card, 17 IRRIGATION (refer to Chapter II). When NSD = 17 (see p. 87 of TEHM; Huff et al., 1977), GETSET calls RDIRIG to read the irrigation data.

The change was made to read the switch parameter ISWIWT in I5 format from columns 26 - 30 on card number 6.1 (Huff et al., 1977; see p. 93). If ISWIWT ≠ 0, then subroutine LAND will print the variable-contributing-area parameter WT that is calculated in PROSPR for each time step that it is nonzero. That is, WT is the proportion of

infiltration that is diverted to the stream (see Fig. 5b). ISWIWT is passed to LAND via the common statement IMPAR.

A section of code executed at the end of subroutine GETSET was rearranged to allow for smoother program flow. Also, the two parameters SNOPAR and DUST were uninitialized in TEHM. In AGTEHM, these two variables are initialized to 0.0.

#### K. Subroutine HRADSL

Subroutine HRADSL takes the hourly solar radiation incident on a horizontal surface and computes the corresponding hourly solar radiation on a sloping surface. It is assumed that 5.6% of the hourly radiation on the horizontal is diffuse radiation from the sky. The slope is exposed to this diffuse radiation even if the sun has not risen on the slope. This diffuse radiation is, however, multiplied by the fraction of the whole sky visible from the slope. The remaining 94.4% of the incident radiation on the horizontal is assumed to be direct. When the sun is above the horizon on the slope this factor is multiplied by the ratio of the direct radiation on the slope, to the direct radiation on the horizontal and added to the diffuse radiation to give the total radiation for that hour. Correction is also made for map area. Multiple sunrises are considered.

A different formulation for the equation of time is used. The version used in subroutine EQUATI in TEHM has some undesirable numerical properties associated with the way the principal values of the arctangent function are handled.

HRADSL is called from ANUDAY.

#### L. Subroutine INDEX

This subroutine is called by subroutine MONDAT when calculating the hourly dew point for cases where the hourly dew point is not available. It takes the hourly temperatures for a day and indexes them in increasing order. This routine is used in the implementation of the hourly dew point algorithm explained in Chapter II.

#### M. Changes in Subroutine LAND

A dimension statement for the two arrays HNRAD and HIRIG was added in subroutine LAND. These arrays were included in the new calling sequence to ANUDAY which returns hourly values of solar radiation on the slope and hourly irrigation values for the day. Hourly sprinkler irrigation values were added to the precipitation values in the new call to subroutine XPREC and hourly flood irrigation conditions are passed to subroutine RAATS. The call to the PROSPR subroutine was modified to include irrigation parameters. The infiltration that is calculated by the RAATS subroutine is multiplied by the variable-source-area parameter (computer name WT) that was computed in subroutine PROSPR (see Chapter II). This result is added to the impervious area runoff, and the remaining water is passed to subroutine PROSPR. LAND prints the variable WT (along with the day, hour, and minute) if the switch parameter ISWIWT is not 0 and if WT > 0.

#### N. Subroutine MONDAT

Subroutine MONDAT is an added subroutine and is used to process a month's data. MONDAT will enter nominal or calculate daily meteorological data when input data are not available. When hourly

input data are not available, MONDAT will enter nominal or calculate hourly meteorological data inferred from the daily data.

O. Subroutine NATEMP

NATEMP is an algorithm that calculates mean daily temperatures in North America (see Chapter II). This subroutine is called by MONDAT if temperature data are not available. The Julian date, the latitude, and the altitude above mean sea level are used in the equation, which is applicable between 25° and 55° North latitude.

P. Changes in Subroutine PEVSRF

In PEVSRF, the calling sequence was changed to remove unnecessary variables and some redundant common statements were deleted. Modifications were made within the routine to make it flow more smoothly.

Q. Changes in Subroutine PROSPR

A few changes were made to PROSPR to allow the routine to run more efficiently. The model calculating the soil moisture content of each layer during flood irrigation (see Chapter II) was added. The algorithm for variable-source-area as described in Chapter II was modified with the results (parameter WT) being passed by common IMPAR to subroutine LAND. If the macropore-mesopore option is needed, PROSPR calls subroutine SWIFT.

R. Changes in Subroutine RAATS

The calling sequence in RAATS was changed to include the irrigation variables IRT (signifies type of irrigation; = K in Chapter II), QHIRRG

(quarter-hour irrigation), RIRRG (remaining irrigation), and FIRRG (fraction of the land surface that is flooded). If there is sprinkler irrigation or no flood irrigation ( $IRT < 2$ ), RAATS proceeds as in the original version. When  $IRT \geq 2$ , RAATS computes the infiltration depending on the type of flood irrigation. The corresponding infiltration takes FIRRG into account.

The occurrence of ponded water at the soil surface due to irrigation or excess rainfall results in a switch parameter POND to be set from 0.0 to 1.0. This switch then invokes the macropore algorithms if they are called for by the input data.

#### S. Subroutine RADIST

Subroutine RADIST uses daily solar radiation to estimate the hourly radiation on a horizontal surface. The hourly radiation, obtained by integrating the solar altitude equation, is reduced by the transmission factor  $T_h = e^{\alpha l}$  where  $l$  is substituted from equation (4) to give

$$T_h = \exp (\alpha h (2+r)/(\cos\phi + \sqrt{r(2+r) + \cos^2\phi})) , \quad (11)$$

where

$r$  = height of atmosphere/radius of earth  $\approx 0.002$  (dimensionless),

$\alpha h$  = attenuation coefficient = - 0.106, and

$\phi$  = solar altitude during the hour (radians).

This transmission factor gives slightly less radiation near sunrise and sunset than does the algorithm used by subroutine SRATIO in TEHM.

Subroutine RADIST is called from subroutine MONDAT.

#### T. Subroutine RDIRIG

Subroutine RDIRIG reads hourly irrigation data. These data are preceded by the card, 17 IRRIGATION, which signals subroutine GETSET to call RDIRIG (see Chapter II). The packed card images are stored by year and month with other hourly data and examined at daily intervals in subroutine ANUDAY.

#### U. Changes in Subroutine READIN

One modification made to subroutine READIN was to make the call to subroutine CHKCIF immediately after reading the cumulative infiltration curve (from the input data) in order to check the smoothness of the curve. Another change was that of reading the parameters LRMODL and YESMAC that were discussed in Chapter II. If YESMAC >0.0, subroutine RSWIFT is called from READIN.

#### V. Subroutine RSWIFT

The input data required for the macropore flow algorithms are read by RSWIFT. This subroutine is called from READIN.

#### W. Function SOLRAD

Function SOLRAD calculates the potential daily solar radiation at the earth's surface. The daily potential solar radiation on a horizontal surface is calculated from the date, latitude, and solar constant using the algorithm of Swift (1973). The atmospheric transmission factor is estimated from Eq. (11) where  $\phi$  is now the solar altitude from zenith at solar noon (radians). This is the clear air transmission and does not include tropospheric attenuation by clouds.

Function SOLRAD is called from subroutines MONDAT and ANUDAY.

#### X. Entry SUBONE

The entry to SUBONE is coded in subroutine SWIFT and the call to SUBONE is made from subroutine PROSPR. This entry invokes the macropore flow calculations for soil profile layers below the first soil layer.

#### Y. Subroutine SWIFT

Macropore flow algorithms for ponded infiltration and perched water tables are conducted by this subroutine. The instruction CALL SWIFT is made from subroutine PROSPR.

#### Z. Entry TMONTH

Monthly totals of macropore flow results are printed as a result of the ENTRY TMONTH into subroutine WSWIFT. The CALL TMONTH statement is coded in subroutine BELCH.

#### A1. Subroutine WSWIFT

The daily simulation results of macropore flows are printed (if requested) by WSWIFT which is called from subroutine BELCH. Monthly results are also printed with the entry TMONTH into subroutine WSWIFT.

#### B1. Changes in Subroutine XPREC

Subroutine XPREC was modified to handle sprinkler irrigation data. The calling sequence was changed and a section of redundant and unnecessary code was removed.

#### IV. Discussion

All of the new input data options and algorithms documented in this report have been tested through preliminary application of AGTEHM to corn and soybean crop studies and a grassland watershed. These applications and results will be documented in subsequent reports. Advances in understanding and prediction occur through the cycles of model development and application. AGTEHM is best viewed as a research tool for addressing hydrologic hypotheses in agricultural and forestry research. This is a necessary and important step which provides the hydrologic framework for coupling material transport subroutines. There are many chemical pollutant problems resulting from agricultural and forestry practices (pesticides, nitrate) and conversely agricultural and forest ecosystems may be impacted by pollutants from external sources. Systematic analysis of these chemical transport problems can be aided by simulation modeling using AGTEHM as a component model.

## V. References

- Bevan, K. J., and M. J. Kirkby. 1979. A physically based variable contributing area model of basin hydrology. *Hydrological Sciences Bulletin* 24: 43-69.
- Fong, L., and H. R. Appelbaum. 1980. Macropore-mesopore model of water flow through aggregated porous media. CEPS-X-312. Oak Ridge National Laboratory, Oak Ridge, Tennessee.
- Freeze, R. A. 1972. Role of subsurface flow in generating surface runoff. 2. Upstream source areas. *Water Resour. Res.* 8:1272-1283.
- Hewlett, J. D., and W. L. Nutter. 1970. The varying source area of streamflow from upland basins. Paper presented at Symposium on Interdisciplinary Aspects of Watershed Management. Montana State University, Bozeman, Montana.
- Huff, D. D., R. J. Luxmoore, J. B. Mankin, and C. L. Begovich. 1977. TEHM. A Terrestrial Ecosystem Hydrology Model. ORNL/NSF/EATC-27. Oak Ridge National Laboratory, Oak Ridge, Tennessee.
- Patterson, M. R., J. K. Munro, D. E. Fields, R. D. Ellison, A. A. Brooks, and D. D. Huff. 1974. A user's manual for the FORTRAN IV version of the Wisconsin Hydrologic Transport Model. ORNL/NSF/EATC-7, EDFB-IBP-74-9. Oak Ridge National Laboratory, Oak Ridge, Tennessee.
- Reicosky, D. C., and J. R. Lambert. 1978. Field measured and simulated corn leaf-water potential. *Soil Sci. Soc. Am. J.* 42:221-228.

- Sikov, S. I. 1971. Computation of Solar Radiation Characteristics.  
pp. 156-157. Keter Press, Jerusalem, Israel. 185 pp.
- Swift, L. W., Jr., and K. R. Knoerr. 1973. Estimating solar radiation  
on mountain slopes. Agric. Meteorol. 12:329-336.
- Thomas, G. W., and R. E. Phillips. 1979. Consequences of water  
movement in macropores. J. Environ. Qual. 8:149-152.
- U.S. Department of Commerce. 1968. Weather Atlas of the U.S.  
Reprinted 1975 by Gale Research Company. pp. 2-73. Book Tower,  
Detroit, Michigan. 262 pp.
- Whipkey, R. Z. 1967. Theory and mechanics of subsurface stormflow.  
pp. 255-260. IN Sopper, W. E., and H. W. Lull (eds.), Int. Symp.  
on Forest Hydrol. Pergamon Press, New York.

## APPENDIX A UTILITY PROGRAMS

This appendix includes two utility programs used in preparing data for AGTEHM. The first program reads average daytime cloud cover and generates average daily solar radiation data for AGTEHM. A description of the input data to the program is given below. An example input data set to the program is shown along with the corresponding output (Figs. A-1 - A-2). The second program reads the cumulative infiltration curve data and checks its "smoothness" (see Chapter III). This program allows the user to check these data before executing AGTEHM. Again, a description of the input data to the code is given along with a sample input data set (Fig. A-3).

### Input Description for Daily Solar Radiation Program

| <u>Card</u> | <u>Columns</u> | <u>Description of Input Data</u>  |
|-------------|----------------|---|
| 1           |                | FORMAT (A4, A3, 212, I1, 22F3.0)  |
| 1-7         |                | <u>I</u> - A seven-character field used to identify the data.   |
| 8-9         |                | <u>IY</u> - A two-digit integer signifying the year of the input.   |
| 10-11       |                | <u>IM</u> - A two-digit integer signifying the month of the input.  |
| 12          |                | <u>N</u> - A single digit number:<br>= 1 for days 1 through 11,<br>= 2 for days 12 through 22,<br>= 3 for days 23 through 31.   |
| 13-15       |                | <u>S(1)</u> - Fraction of possible sunshine for day 1 of month IM If N = 1, day 12 of month IM if N = 2, day 23 of month IM if N = 3. However, this entry is not used in the program. |

- 16-18      C(1) - Fraction of sky covered with clouds for day 1 of month IM if N = 1, day 12 of month IM if N = 2, day 23 of month IM if N = 3 in tenths (e.g., if 4/10 of the sky is covered enter 4.0).
- 19-78      S(J), C(J), J=2,11 - Similar to columns 13-18 with J signifying days 2 to 11 of month IM if N = 1, days 13 to 22 of month IM if N = 2, days 24 to 31 of month IM if N = 3.

All cards of the input data for this program are similar to card 1.

See the sample input data set in Fig. A-1 and the corresponding output in Fig. A-2. The program precedes these figures.

#### Input Description for the Cumulative Infiltration Check Program

| <u>Card</u>       | <u>Columns</u> | <u>Description of Input Data</u>   |
|-------------------|----------------|--|
| 1                 |                | FORMAT (13)  |
| 1-3               |                | <u>NRAATS</u> - The number of points to be included in the table of corresponding time and cumulative infiltration values.               |
| 2                 |                | FORMAT (16F5.2)  |
| 1-5, 6-10<br>etc. |                | <u>CIF(I), I=1, NRAATS</u> - Cumulative infiltration amounts corresponding to the (following) times since the start of water input (cm). |
| 3                 |                | FORMAT (16F5.2)  |
| 1-5, 6-10<br>etc. |                | <u>RTIM(I), I=1, NRAATS</u> - Elapsed time from beginning point for the cumulative infiltration curve (min).                             |

A sample input data set is shown in Fig. A-3 and the program precedes it. There is no output if the curve is "smooth." Otherwise, an error message is printed, and the user should alter the existing data or add more points or both so that the smoothness checks are satisfied.

```

C      MODEL DAILY RADIATION AT EARTHS SURFACE          MAIN  10
C      DIMENSION T(2),S(11),C(11),SA(11),NDY(12)        MAIN  20
C      NUMBER OF DAYS IN EACH MONTH                     MAIN  30
C      DATA NDY/31,28,31,30,31,30,31,31,30,31,30,31/    MAIN  40
C      ALAT IS LATITUDE OF SITE                         MAIN  50
C      DATA IN,IOUT/21,22/,AK/.35/,ALAT/35.3/          MAIN  60
C      SEE SIKOV FOR AK PARAMETER                      MAIN  70
C      AK1=1.-AK                                         MAIN  80
C      READ SUNSHINE S (NOT USED HERE),                 MAIN  90
C      AND FRACTION CLOUD COVER C                      MAIN 100
10 READ (IN,1000,END=60) T,IY,IM,N,(S(J),C(J),J=1,11)  MAIN 110
N2=MIN0(11,NDY(IM)-(N-1)*11)                           MAIN 120
C      WRITE (IOUT,1010) T,IY,IM,N,(C(J),J=1,N2)         MAIN 130
1000 FORMAT(A4,A3,2I2,I1,22F3.0)                         MAIN 140
JDY=0
IF(IM.EQ.1) GO TO 20
IMM=IM-1
DO 15 J=1,IMM
15 JDY=JDY+NDY(J)
20 JDY=JDY+(N-1)*11
DO 30 J=1,N2
30 JDY=JDY+1
C      GET POTENTIAL SOLAR RADIATION FOR DAY AND LATITUDE
DY=JDY
SP=SOLRAD(DY,ALAT)
C      CORRECT FOR CLOUD COVER
30 SA(J)=SP*(1.-.1*C(J)*AK1)
WRITE (IOUT,1010) T,IY,IM,N,(SA(J),J=1,N2)
1010 FORMAT(A4,A3,2I2,I1,11F6.0)
GO TO 10
60 CONTINUE
STOP
END
FUNCTION SOLRAD(DJULN,DGLAT)
C      CALCULATION OF DAILY POTENTIAL SOLAR RADIATION
C      ALGORITHM PREPARED BY LLOYD W. SWIFT JR. CHL
C      DJULN IS JULIAN DATE
C      DGLAT IS NORTH LATITUDE IN DEGREES
C      SOLRAD IS POTENTIAL DAILY DIRECT SOLAR RADIATION
C      SUNRN=SOLAR CONSTANT(CAL/CM**2/MIN)
C      AO=ATTENUATION OF RADIATION WHEN THE SUN IS AT ZENITH
C      ALFA=NATURAL LOGRITHM OF ATTENUATION AO
C      HA=EFFECTIVE HEIGHT OF THE ATMOSPHERE/EARTH RADIUS
C      DATA SUNRN/1.95/,ALFA,HA/-106.,.002/
C      SOLAR DECLINATION
SINDEC=.39785*SIN(4.868961+.0172024*DJULN+.033446*
+ SIN(6.22411+.0172024*DJULN))
COSDEC=SQRT(1.-SINDEC*SINDEC)
C      ECCENTRICITY CORRECTION TO EARTH ORBITAL RADIUS
E=1.0-0.0167*COS((DJULN-3.)*0.0172)
C      HOURLY RADIATION INCIDENT ON UPPER ATMOSPHERE
RI=60.*SUNRN/(E*E)
RADLAT=DGLAT*.01745329
SINLAT=SIN(RADLAT)
COSLAT=COS(RADLAT)
DAYL=A COS(-SINLAT/COSLAT*SINDEC/COSDEC)
C      DAILY RADIATION INCIDENT ON UPPER ATMOSPHERE
SOLRAD=RI*7.64*(SINDEC*SINLAT*DAYL+COSDEC*COSLAT*SIN(DAYL))
C      ATTENUATION OF DIRECT RADIATION BY CLEAR ATMOSPHERE
COST=COSDEC*COSLAT+SINDEC*SINLAT
ATTEN=EXP(ALFA*(2.+HA)/(COST+SQRT(HA*(2.+HA)+COST*COST)))
C      POTENTIAL DIRECT RADIATION AT EARTHS SURFACE
SOLRAD=SOLRAD*ATTEN
RETURN
END

```

```

S STUT 75011 80 6 44 8 20 10100 0 88 8100 2 9 10 54 5 64 5 20 10 78 4
S STUT 75012 32 6 96 2 87 6100 4 96 2 39 10 41 8 2 10 97 1 90 5 68 9
S STUT 75013 90 2 16 10 67 6100 1 77 4 52 10 64 8 45 10 0 10
S STUT 75021 0 10 2 10 9 10 14 10 39 9 42 9 98 1 76 9 90 3 45 8 31 8
S STUT 75022 35 8 84 5 80 6 38 10 27 10 64 8 48 8 67 6 96 0 92 2 9 10
S STUT 75023 6 10 56 8100 0 26 10 72 3 78 6
S STUT 75031 73 5 89 6 82 8 49 8100 6 36 10 89 4 98 2 14 10 36 10 6 10
S STUT 75032 6 10 6 10 86 3 42 10 40 9 48 10 42 10 92 1100 7 72 9 94 2
S STUT 75033 26 10 94 1100 0 72 5 20 10 4 10 17 10 90 6 28 10
S STUT 75041100 1 50 8 98 1100 2 98 6 96 4 66 10 13 10 66 9 72 6 82 4
S STUT 75042100 0 42 9 36 10100 2100 4 26 10 53 10 93 2100 0 97 1 80 4
S STUT 75043 74 8 47 8 77 6 72 8 78 8 40 10 58 8 57 10
S STUT 75051 80 4 56 8 72 8 95 0 86 4 78 8 66 6 58 9 63 8 76 6 58 9
S STUT 75052 98 2 97 7 50 9 43 10 44 10 61 4100 0 93 5 80 8 84 7 92 4
S STUT 75053 90 4 86 8 84 6 66 8 90 6 52 9 64 10 76 8 74 7
S STUT 75061 98 0 95 3 92 6 96 1 74 7 79 6 51 10 86 10 63 10 38 10 68 8
S STUT 75062100 0 96 0 62 10 73 6 82 7 66 10 94 4 80 6 96 3 77 6 86 6
S STUT 75063 88 5 95 2 92 3 89 4 70 5 85 2 82 4 86 2
S STUT 75071 83 3 77 8 74 3 86 3 87 4 70 7 58 6 79 6 84 4 70 7 93 2
S STUT 75072 94 2 96 4 98 1100 0 96 4 97 2 68 6 90 6 48 8 70 10 81 4
S STUT 75073 73 7 70 10 48 10 91 8 48 9 82 6 88 4 76 6 28 10
S STUT 75081 37 10 70 8 50 10 74 7 86 4 92 2 94 4 92 2 62 6 78 5 92 2
S STUT 75082 96 2 96 3 93 6 80 8 68 10 76 8 74 9 74 6 84 4 90 2 96 2
S STUT 75083 94 4 86 6 91 4 70 6 76 4 78 4 82 4 70 6 92 4
S STUT 75091 98 1100 0 96 1 97 1 34 10 66 6 97 2 94 3 54 8 64 9 96 6
S STUT 75092 22 10 45 8 57 9 18 10 45 10 42 8 80 4 49 9 96 1 72 8 45 8
S STUT 75093 8 4 49 10 90 2100 1100 0100 0 88 2 86 5
S STUT 75101 58 8100 0100 0 79 4 51 9 55 9 64 8 92 2100 0 99 0 96 2
S STUT 75102100 0100 1100 1 80 4 8 10 78 6 94 3100 0100 0100 0 93 2
S STUT 75103 64 6 52 8 1 10 94 0 30 9 50 8 42 10100 0 95 7
S STUT 75111 87 3 90 6 26 10 34 10 30 8 28 8 56 6 95 1 16 9 99 0 71 3
S STUT 75112100 0 69 4100 1100 0100 4100 0100 0 80 4 68 6 0 10 0 10
S STUT 75113 6 6 89 2 91 8 0 10 98 1 3 6 21 10 31 7
S STUT 75121 98 1100 0100 0 98 8 34 8 0 10 0 10 0 10 0 10100 0 97 2
S STUT 75122 91 8 34 8 10 10 0 10 36 8 32 6 95 2100 1 75 2 66 6 68 8
S STUT 75123 37 7 24 10 0 10 0 10 8 10 82 8 11 10 0 10 13 7
$
```

Fig. A-1. Sample input data set (Stuttgart, AK.) for the average daily solar radiation program.

S STUT 75 11 198. 156. 114. 328. 158. 288. 117. 226. 227. 119. 252.  
 S STUT 75 12 209. 301. 212. 260. 307. 125. 172. 127. 341. 248. 154.  
 S STUT 75 13 326. 132. 233. 360. 287. 137. 190. 140. 141.  
 S STUT 75 21 143. 144. 146. 147. 176. 178. 405. 182. 356. 214. 217.  
 S STUT 75 22 219. 311. 284. 165. 166. 230. 233. 299. 495. 435. 177.  
 S STUT 75 23 179. 247. 520. 184. 427. 327.  
 S STUT 75 31 365. 333. 265. 267. 343. 198. 423. 502. 204. 206. 208.  
 S STUT 75 32 209. 211. 490. 215. 257. 218. 220. 593. 348. 267. 565.  
 S STUT 75 33 229. 616. 664. 452. 236. 237. 239. 420. 242.  
 S STUT 75 41 652. 337. 661. 619. 437. 533. 254. 255. 304. 450. 549.  
 S STUT 75 42 746. 311. 264. 659. 564. 268. 269. 673. 777. 730. 580.  
 S STUT 75 43 378. 380. 485. 383. 385. 282. 388. 284.  
 S STUT 75 51 602. 392. 394. 823. 611. 398. 507. 346. 401. 512. 349.  
 S STUT 75 52 734. 461. 352. 298. 298. 633. 857. 580. 413. 470. 640.  
 S STUT 75 53 641. 416. 530. 418. 532. 363. 306. 421. 478.  
 S STUT 75 61 879. 708. 537. 825. 481. 539. 310. 310. 310. 310. 426.  
 S STUT 75 62 888. 888. 311. 542. 485. 311. 658. 543. 716. 543. 543.  
 S STUT 75 63 600. 774. 716. 658. 600. 772. 657. 772.  
 S STUT 75 71 713. 425. 712. 712. 654. 481. 538. 537. 651. 479. 763.  
 S STUT 75 72 762. 647. 817. 872. 644. 756. 529. 528. 415. 302. 637.  
 S STUT 75 73 468. 300. 299. 409. 353. 518. 626. 515. 295.  
 S STUT 75 81 294. 402. 292. 453. 614. 719. 610. 715. 499. 551. 707.  
 S STUT 75 82 704. 649. 490. 384. 279. 381. 328. 480. 580. 679. 676.  
 S STUT 75 83 572. 470. 567. 465. 561. 559. 556. 456. 550.  
 S STUT 75 91 691. 735. 683. 680. 253. 438. 621. 571. 339. 291. 425.  
 S STUT 75 92 242. 330. 283. 237. 236. 321. 492. 274. 612. 312. 310.  
 S STUT 75 93 474. 223. 549. 585. 621. 616. 532. 409.  
 S STUT 75101 289. 596. 591. 434. 241. 239. 274. 492. 561. 556. 479.  
 S STUT 75102 546. 506. 501. 393. 184. 318. 415. 511. 506. 501. 432.  
 S STUT 75103 300. 234. 169. 477. 196. 224. 162. 458. 247.  
 S STUT 75111 362. 271. 154. 153. 207. 205. 258. 392. 172. 411. 327.  
 S STUT 75112 403. 295. 370. 392. 287. 384. 381. 279. 228. 130. 129.  
 S STUT 75113 223. 315. 172. 125. 330. 214. 122. 189.  
 S STUT 75121 321. 341. 339. 162. 161. 117. 116. 116. 115. 327. 284.  
 S STUT 75122 156. 155. 113. 113. 154. 195. 278. 299. 278. 195. 153.  
 S STUT 75123 174. 112. 112. 112. 112. 154. 113. 113. 113. 176.  
 \$  
 .

Fig. A-2. Output data from the average daily solar radiation program using the input data from Fig. A-1. These data can then be read by AGTEHM.

```

      IMPLICIT REAL*8(A-H,O-Z)                      CHKC 10
      DIMENSION RTIM(50),CIF(50)                     CHKC 20
      READ(60,50)NRAATS                            CHKC 30
 50   FORMAT(I3)                                     CHKC 40
      READ(60,100)(CIF(I),I=1,NRAATS)              CHKC 50
      READ(60,100)(RTIM(I),I=1,NRAATS)             CHKC 60
 100  FORMAT(16F5.2)                                CHKC 70
      CALL CHKCIF(RTIM,CIF,NRAATS,1)                CHKC 80
      CALL CHKCIF(CIF,RTIM,NRAATS,2)                CHKC 90
      STOP                                         CHKC 100
      END                                           CHKC 110
      SUBROUTINE CHKCIF(X,Y,NR,IXY)                 CHKC 120
      IMPLICIT REAL*8(A-H,O-Z)                      CHKC 130
      DIMENSION X(1),Y(1)                           CHKC 140
      NR=NR                                         CHKC 150
      NM2=NM2-2                                     CHKC 160
      DO 10 I=1,NM2                                 CHKC 170
      TMDEN1=Y(I)*(X(I+1)-X(I+2))                CHKC 180
      TMDEN2=-Y(I+1)*(X(I)-X(I+2))               CHKC 190
      TMDEN3=Y(I+2)*(X(I)-X(I+1))               CHKC 200
      TMNUM1=TMDEN1*(X(I+1)+X(I+2))              CHKC 210
      TMNUM2=TMDEN2*(X(I)+X(I+2))                CHKC 220
      TMNUM3=TMDEN3*(X(I)+X(I+1))                CHKC 230
      DENOMR=TMDEN1+TMDEN2+TMDEN3                CHKC 240
      IF(DENOMR.EQ.0.0)GO TO 10                   CHKC 250
      XX=0.5*(TMNUM1+TMNUM2+TMNUM3)/DENOMR       CHKC 260
      IF(XX.GE.X(I+2).OR.XX.LE.X(I))GO TO 10     CHKC 270
      GO TO 20                                     CHKC 280
 10   CONTINUE                                     CHKC 290
      RETURN                                         CHKC 300
 20   IF(IXY.EQ.1)WRITE(61,30)X(I),X(I+2)        CHKC 310
 30   FORMAT(1X,'ERROR IN CIF CURVE @ RTIM = ',E11.4,' TO ',E11.4,
      1' (NOT SMOOTH)')                          CHKC 320
      IF(IXY.EQ.2)WRITE(61,40)X(I),X(I+2)        CHKC 330
 40   FORMAT(1X,'ERROR IN CIF CURVE @ CIF = ',E11.4,' TO ',E11.4,
      1' (NOT SMOOTH)')                          CHKC 340
      STOP                                         CHKC 350
      END                                           CHKC 360
                                              CHKC 370
                                              CHKC 380

```

16  
 0.0000.4251.1751.8752.2302.6252.9253.1203.2053.2253.2403.2753.3103.3503.4003.450  
 0. 10. 30. 50. 70. 120. 200. 300. 400. 450. 500. 700.1000.1300.1660.2000.

Fig. A-3. Sample input data for the cumulative infiltration check program.

APPENDIX B  
AGTEHM SUBROUTINE LISTINGS

|   |          |
|---|----------|
| SUBROUTINE ANUDAY(YEAR,MONTH,DAY,HNRAD,IP,IRT,HIRIG)                | ANUD 10  |
| C INITIALIZATION FOR START OF A NEW DAY                             | ANUD 20  |
| COMMON/TIMES/T1,T2,T3,T4,TMW,SIGS,SIGW,ALBS,ALBW                    | ANUD 30  |
| COMMON /RESIST/ R1,R2,R3,R4,R5,RR1,RRA,RRB,RRC,RRR,TM,RLIT          | ANUD 40  |
| COMMON/HUMID/FOLTYP,PAIR,CPO,RB,RX,SIGMA,XL,GM,GV,HT,ALEAF          | ANUD 50  |
| COMMON/DRAG/SDRAG,WDRAG,REDUC                                       | ANUD 60  |
| COMMON /ANGLES/ FILL(6),DGLAT,DLONG                                 | ANUD 70  |
| COMMON/DAILY/DEW(12,31), RAD(12,31), EVAP(12,31), TEM (2,12,31),    | ANUD 80  |
| > WINDS(12,31), IFILL(144)  | ANUD 90  |
| COMMON /HRLYS/ IYR,IMO,LOKN,IWRT,IKMPLT,IREC,JSTART, NUMDYS,        | ANUD 100 |
| > HDEW(24,31),HRAD(24,31),HWND(24,31),HTEM(24,31),                  | ANUD 110 |
| > IRIG,PKIRIG(87)   | ANUD 120 |
| COMMON/BLOCKE/RN,GND,TTT,EE,PWP,EV,VEL,JDATE                        | ANUD 130 |
| COMMON/SHIFT1/ RADCON,CONMLT,SCF,ELDIF, IDNS,FCI,DGM,WC,MPACK, K1,  | ANUD 140 |
| > A, LG, SS, NN, K24L, EPXM,SUNCON,CLD,CLDFAC                       | ANUD 150 |
| COMMON/THINGS/ALBVEG,CANON,CANOFF,SIMIN,SIMAX,ALMIN,ALMAX,SLOPE     | ANUD 160 |
| COMMON /SURF/ PWPS,PWPW,PWPMAX,RESS,RESW,RESMAX,POWS,POWW, POWER,   | ANUD 170 |
| > LRMODL  | ANUD 180 |
| COMMON /GET/ STCLD,MONTHP(12),EPXMIN, EPXMAX,RNON,SUNHR(24),        | ANUD 190 |
| > DUST(12),Y,M,T(744),JJ  | ANUD 200 |
| REAL#8 SDRAG,WDRAG,REDUC  | ANUD 210 |
| REAL#8 PWPS,PWPW,PWPMAX,RESS,RESW,RESMAX,POWS,POWW,POWER            | ANUD 220 |
| REAL#8 R1,R2,R3,R4,R5,RR1,RRA,RRB,RRC,RRR,TM,RLIT                   | ANUD 230 |
| REAL#8 T1,T2,T3,T4,RB,XL,GND,STCLD,TDATE, FOLTYP,ALBVEG,TMS,        | ANUD 240 |
| > TMW,SIGS,SIGW, ALBS,ALBW,PAIR,CPO,RX,SIGMA,GM,GV,HT,ALEAF,RN,TTT, | ANUD 250 |
| > EE,PWP,EV, VEL,CANON,CANOFF,SIMIN,SIMAX,ALMIN,ALMAX,SLOPE         | ANUD 260 |
| REAL IDNS,MPACK,K1,LG,K24L,NN                                       | ANUD 270 |
| INTEGER DAY,YEAR,Y  | ANUD 280 |
| DIMENSION HNRAD(24),HIRIG(24)                                       | ANUD 290 |
| C   | ANUD 300 |
| JLAST=JSTART+NUMDYS   | ANUD 310 |
| JDATE=JSTART+DAY  | ANUD 320 |
| TDATE=JDATE   | ANUD 330 |
| XDATE=JDATE   | ANUD 340 |
| C SET DAILY VALUE OF EPXM (INTERCEPTION STORAGE),                   | ANUD 350 |
| C ALEAF (LEAF AREA), ALBVEG (ALBEDO OF VEGETATION)                  | ANUD 360 |
| IF (TDATE.LT.T4.AND.TDATE.GT.T1) GO TO 10                           | ANUD 370 |
| C WINTER VALUES   | ANUD 380 |
| EPXM = EPXMIN   | ANUD 390 |
| ALEAF=ALMIN   | ANUD 400 |
| ALBVEG=ALBW   | ANUD 410 |
| SIGMA=SIGW  | ANUD 420 |
| PWPMAX=PWPW   | ANUD 430 |
| RESMAX=RESW   | ANUD 440 |
| POWER=POWW  | ANUD 450 |
| REDUC=WDRAG   | ANUD 460 |
| TM=TMW  | ANUD 470 |
| GO TO 50  | ANUD 480 |
| C SOME NON-WINTER VALUES  | ANUD 490 |
| 10 SIGMA=SIGS   | ANUD 500 |
| PWPMAX=PWPS   | ANUD 510 |
| RESMAX=RESS   | ANUD 520 |
| POWER=POWS  | ANUD 530 |
| TM=TMS  | ANUD 540 |
| IF (TDATE.GT.T2) GO TO 20   | ANUD 550 |
| C COEFFICIENTS FOR SPRING VALUES                                    | ANUD 560 |
| FRS=(TDATE-T1)/(T2-T1)  | ANUD 570 |
| FRW=1.-FRS  | ANUD 580 |
| GO TO 40  | ANUD 590 |
| 20 IF (TDATE.GT.T3) GO TO 30  | ANUD 600 |
| C SUMMER VALUES   | ANUD 610 |

## APPENDIX B (continued)

```

EPXM=EPXMAX          ANUD 620
ALEAF=ALMAX          ANUD 630
ALBVEG=ALBS          ANUD 640
REDUC=SDRAG          ANUD 650
GO TO 50             ANUD 660
C      COEFFICIENTS FOR FALL VALUES   ANUD 670
30 FRW=(TDATE-T3)/(T4-T3)           ANUD 680
FRS=1.-FRW            ANUD 690
40 EPXM=FRS*EPXMAX+FRW*EPXMIN     ANUD 700
ALEAF=FRS*ALMAX+FRW*ALMIN        ANUD 710
ALBVEG=FRS*ALBS+FRW*ALBW        ANUD 720
REDUC=FRS*SDRAG+FRW*WDRAG       ANUD 730
50 CONTINUE             ANUD 740
C      ESTIMATE CLOUD COVER, STATISITICAL CLOUD FACTOR   ANUD 750
PERMAX=AMIN1(RAD(MONTH, DAY)/SOLRAD(XDATE, DGLAT), 1.) ANUD 760
CLD=1.0-(PERMAX-0.1)/.9         ANUD 770
IF (PERMAX.LE.0.1) CLD=1.0       ANUD 780
STCLD = 0.9*CLD**2            ANUD 790
C      HOURLY SOLAR RADIATION INCIDENT ON SLOPE          ANUD 800
CALL HRADSL(XDATE,HRAD(1, DAY),HNRAD)      ANUD 810
GND=GROUND(GM, GV, TDATE)           ANUD 820
RIF=1.-ALBVEG-GND/RAD(IMO, DAY)      ANUD 830
CLDFAC=1.-STCLD                  ANUD 840
SR2=RAD(MONTH, DAY)                ANUD 850
CALL SUNMAP(XDATE, SR2)            ANUD 860
SOLNET=(SR2*(1.-ALBVEG))-GND      ANUD 870
SUNCON=SR2/SOLNET                ANUD 880
C      CORRECT FOR ALBEDO TO GET NET RADIATION          ANUD 890
DO 60 IH=1,24                    ANUD 900
HNRAD(IH)=HNRAD(IH)*RIF          ANUD 910
60 HIRIG(IH)=0.                 ANUD 920
IRT=0                            ANUD 930
70 IF(IP.GT.IRIG) GO TO 110      ANUD 940
C      LOOK FOR IRRIGATION DATA          ANUD 950
K=PKIRIG(IP)                   ANUD 960
ID=K/100000                     ANUD 970
IF(ID.NE.DAY) GO TO 110          ANUD 980
K=K-100000*ID                  ANUD 990
IH=K/1000                        ANUD 1000
K=K-IH*1000                      ANUD 1010
IH=IH-1                          ANUD 1020
IN=K/10                           ANUD 1030
IRT=K-10*IN                      ANUD 1040
IF(IRT.EQ.3) GO TO 90            ANUD 1050
IPL=IP                           ANUD 1060
IP=IP+IN+1                       ANUD 1070
IF(IN.LE.0) GO TO 110            ANUD 1080
DO 80 I=1,IN                      ANUD 1090
80 HIRIG(IH+I)=PKIRIG(IPL+I)     ANUD 1100
GO TO 70                         ANUD 1110
90 DO 100 I=1,IN                 ANUD 1120
100 HIRIG(IH+I)=1.0              ANUD 1130
IP=IP+1                          ANUD 1140
GO TO 70                         ANUD 1150
110 CONTINUE                      ANUD 1160
RETURN                           ANUD 1170
END                             ANUD 1180

```



## APPENDIX B (continued)

```

MIN = 0 ANUM 620
IF(IDY.NE.0) GO TO 10 ANUM 630
MON=MONTH ANUM 640
DO 15 J=1,12 ANUM 650
IDN(J)=MON ANUM 660
MON=MON+1 ANUM 670
IF(MON.EQ.13) MON=1 ANUM 680
15 CONTINUE ANUM 690
IDY=1 ANUM 700
ANUM 710
10 TARGET = TE ANUM 720
IF (NOW.GE.TARGET) GO TO 1000 ANUM 730
NXTF=1 ANUM 740
IF(MONTH.EQ.10) GO TO 4 ANUM 750
NX=MOD(MONTH+1,12)+1 ANUM 760
DO 5 I=1,NX ANUM 770
II = MOD((I+8),12) + 1 ANUM 780
5 NXTF = NXTF + LASDAY(YEAR,II) ANUM 790
4 NXTF=NXTF+NXTF ANUM 800
C ZERO ARRAY TO RECEIVE RUNOFF AND OUTFLOWS ANUM 810
DO 200 NDEX = 1,6 ANUM 820
DO 200 INDEY = 1, 1488 ANUM 830
200 RS30M(NDEX,INDEY) = 0 ANUM 840
C LOAD MONTHS PRECIPITATION DATA FROM PRECIP FILE ANUM 850
NREC = 12 * YEAR + MONTH + 3 ANUM 860
CALL TSEARC (PDRUM,PREC,DSNAME,NREC,RP,1493) ANUM 870
CALL IN (PDRUM,RP,1DUMMY,1493) ANUM 880
KEY = 1DUMMY(2) ANUM 890
DO 5555 II=1,3 ANUM 900
5555 DUMTOT(II) = 1DUMMY(II+2) ANUM 910
C SEE EQUIVALENCE STATEMENT FOR DUMTOT ARRAY ANUM 920
RP = RP + 1 ANUM 930
WRITE(6,2020) MONTHS(MONTH), YEAR, SEG, DSNAME, NREC ANUM 940
2020 FORMAT(1H1,
      + ' SIMULATION OF ',A4,' 19',I2,' BEGINS FOR SEGMENT NO. ',I3,'. PRECIP FILE KEY = ',I6,I4) ANUM 950
      +I3,'. PRECIP FILE KEY = ',I6,I4) ANUM 960
C LOAD MONTH OF HOURLY METEOROLOGICAL DATA ANUM 970
C CALL MONDAT(YEAR,MONTH,1) ANUM 980
C ANUM 990
C ANUM 1000
C PRINT 103 ANUM 1010
103 FORMAT(T1,'0 DAY INFILT RUNOFF DRAINAGE ET ANUM 1020
      +FLLAT FLNET SURF.CON SURF.POT THETA1 THETA2 ANUM 1030
      +THETAN') ANUM 1040
      PRINT 104 ANUM 1050
104 FORMAT(T7,' (CM) ----- (CM PER DAY)----- ANUM 1060
      +(CM/SEC) (BAR) -(CM PER CM)-') ANUM 1070
1000 CONTINUE ANUM 1080
      RETURN ANUM 1090
      END ANUM 1100

```

## APPENDIX B (continued)

## APPENDIX B (continued)

|                   |          |
|-------------------|----------|
| SASTOR=0.0D0      | ANUS 620 |
| DO 40 J=1,NTL     | ANUS 630 |
| 40 SSGT(J)=SSG(J) | ANUS 640 |
| RES1 = RES        | ANUS 650 |
| SINTFA = 0.0      | ANUS 660 |
| SFILT=0.0         | ANUS 670 |
| SINTC=0.0         | ANUS 680 |
| PCKRN=0.0         | ANUS 690 |
| SMELT=0.0         | ANUS 700 |
| LIQW1=LIQW        | ANUS 710 |
| CNPE=0.0          | ANUS 720 |
| PACK1=PACK        | ANUS 730 |
| SUMSNO=0.0        | ANUS 740 |
| MSRVAP=0.0        | ANUS 750 |
| SSCEP=0.0         | ANUS 760 |
| C SRGX1=0.0       | ANUS 770 |
| SGW1 = SGW        | ANUS 780 |
| LZS1 = LZSINV     | ANUS 790 |
| SCEP1=0.0         | ANUS 800 |
| IDX = 1           | ANUS 810 |
| IDX15 = 1         | ANUS 820 |
| IDX30 = 1         | ANUS 830 |
| ASPR =1.0         | ANUS 840 |
| CKDH = 1.         | ANUS 850 |
| RETURN            | ANUS 860 |
| END               | ANUS 870 |

|   |                                  |
|---|----------------------------------|
| SUBROUTINE ASPECT   | ASPE 10                          |
| COMMON/ANGLES/RADINC,RADLAT,DELONG,PI,D,EQLAT,DGLAT,DLONG   | ASPE 20                          |
| REAL*8 RADINC   | ASPE 30                          |
| PI=3.141592654D0  | ASPE 40                          |
| FAC=PI/180.0  | ASPE 50                          |
| READ(5,10100) DEGINC,AZIM,DGLAT   | ASPE 60                          |
| RADINC=DEGINC*FAC   | ASPE 70                          |
| RDAZ=AZIM*FAC   | ASPE 80                          |
| RADLAT=DGLAT*FAC  | ASPE 90                          |
| COSLAT=COS(RADLAT)  | ASPE 100                         |
| SINLAT=SIN(RADLAT)  | ASPE 110                         |
| RDINC=RADINC  | ASPE 120                         |
| COSINC=COS(RDINC)   | ASPE 130                         |
| SININC=SIN(RDINC)   | ASPE 140                         |
| COSAZ=COS(RDAZ)   | ASPE 150                         |
| SINAZ=SIN(RDAZ)   | ASPE 160                         |
| EQLAT=ARSIN(COSINC*SINLAT+SININC*COSLAT *COSAZ)   | ASPE 170                         |
| DENOM=COSINC*COSLAT-SININC*SINLAT *COSAZ  | ASPE 180                         |
| DELONG=ATAN2(SININC*SINAZ,DENOM)  | ASPE 190                         |
| DEQLAT=EQLAT/FAC  | ASPE 200                         |
| WRITE(6,10000) DEGINC,AZIM,DGLAT,DLONG,DEQLAT,DELONG  | ASPE 210                         |
| RETURN  | ASPE 220                         |
| 10000 FORMAT(' DEGINC=',F7.2,5X,'AZIM=',F7.2,5X,'DGLAT=' ,<br>& F7.2,5X,'DLONG=',F7.2,5X,'DEQLAT=',F7.2,5X,'DELONG=' ,<br>& F7.2) | ASPE 230<br>ASPE 240<br>ASPE 250 |
| 10100 FORMAT(3F10.5)  | ASPE 260                         |
| END   | ASPE 270                         |

## APPENDIX B (continued)

```

SUBROUTINE BELCH(JLAST)                               BELC 10
IMPLICIT REAL*8 (A-H,O-Z)                           BELC 20
REAL*8 MACEX                                       BELC 30
DIMENSION FBETA(8),FDBET(8)                         BELC 40
COMMON/THINGS/ALEVEG,CANON,CANOFF,SIMIN,SIMAX,ALMIN,ALMAX,SLOPE
COMMON/PORES/VP(8),F,S(8),SEV,ETGW,DNFAC,WP1,WP2,NSL,NBL,NS
COMMON/HUMID/FOLTP,PAIR,CPO,RB,RX,SIGMA,XL,GM,GV,HT,ALEAF
COMMON/GOMET/DL(8),AT(2),ARAT(2),FC(8),THETA(8),SWT(8)
COMMON/BLOCKE/RN,GND,TTT,EE,PWP,EV,VEL,JDATE
COMMON/PLACE/ CASEID(20),LASTDY(12),MOBEG
COMMON/SOLPOT/PSI(8)
COMMON/TOTMON/ROFF,TDRN,PSEUDO,ETOT,PTOT,PRES,RF1MON,RF2MON
COMMON/TODAY/DDRAIN,DET,FLLAT,FLNET,RUNO,DPTOT
COMMON/DAYMID/RM,POT,SW1M,SW2M,SWNM
COMMON/PIECES/TRUNO,ZS(8),PRE1,POND,TBET(8),YESMAC.PSM(8),REMAIN
COMMON/BOOKS/DMEMA(8),DMAME(8),DMAMA(8),MACEX(8),BETA(8),DBET(8)
DATA PTOTAL,ETOTAL/0.,0./,STMAC/0.0/
DATA FBETA,FDBET/0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,
10.,0./
SWAT1=SW1M/DL(1)                                     BELC 110
SWAT2=SW2M/DL(2)                                     BELC 120
SWATN=SWNM/DL(NSL)                                    BELC 130
PSL=POT*9.81D-4                                      BELC 140
CM=1./RM                                           BELC 150
WRITE(6,10000) JDATE,DPTOT,RUNO,DDRAIN,DET,FLLAT,FLNET,CM,PSL,
> SWAT1,SWAT2,SWATN                                  BELC 160
IF(YESMAC.GT.0.) CALL WSWIFT                         BELC 170
IF(JDATE.NE.JLAST) GO TO 40                           BELC 180
10 PRINT 10100                                         BELC 190
WINL=0.                                                 BELC 200
WFIN=0.                                                 BELC 210
DO 20 K=1,NSL                                         BELC 220
WFIN=WFIN+THETA(K)                                    BELC 230
20 WINL=WINL+SWT(K)                                    BELC 240
SOILWT=WFIN-WINL                                      BELC 250
IF(YESMAC.EQ.0.)GO TO 27                           BELC 260
SMINL=0.0                                              BELC 270
SMFIN=0.0                                              BELC 280
DO 25 K=1,NSL                                         BELC 290
SMFIN=SMFIN+BETA(K)+DBET(K)                         BELC 300
25 SMINL=SMINL+FBETA(K)+FDBET(K)                    BELC 310
STMAC=SMFIN-SMINL                                     BELC 320
27 CONTINUE                                            BELC 330
BALANC=PTOT-ROFF-PSEUDO-TDRN-ETOT-SOILWT-STMAC
PRINT 10200, PTOT,ETOT,ROFF,TDRN,PSEUDO,SOILWT,BALANC,RF1MON,
> RF2MON                                             BELC 340
C
C       IF(YESMAC.GT.0.)PRINT 10400, STMAC             BELC 350
C       DO 23 I=1,NSL                                 BELC 360
C 23 PRINT 10500, BETA(I),FBETA(I),DBET(I),FDBET(I)
IF(BALANC.GT.0.5) CALL ERROR                         BELC 370
PTOTAL=PTOTAL+PTOT                                     BELC 380
ETOTAL=ETOTAL+ETOT                                     BELC 390
PTOT=0.
ETOT=0.
ROFF=0.
TDRN=0.
PSEUDO=0.
RF1MON=0.
RF2MON=0.
IF(YESMAC.EQ.0.0)GO TO 29                           BELC 400
BELC 410
BELC 420
BELC 430
BELC 440
BELC 450
BELC 460
BELC 470
BELC 480
BELC 490
BELC 500
BELC 510
BELC 520
BELC 530
BELC 540
BELC 550
BELC 560
BELC 570
BELC 580
BELC 590
BELC 600
BELC 610

```

## APPENDIX B (continued)

```

SUBROUTINE CHKCIF(X,Y,NR,IXY)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION X(1),Y(1)
N=NR
NM2=N-2
DO 10 I=1,NM2
TMDEN1=Y(I)*(X(I+1)-X(I+2))
TMDEN2=-Y(I+1)*(X(I)-X(I+2))
TMDEN3=Y(I+2)*(X(I)-X(I+1))
TMNUM1=TMDEN1*(X(I+1)+X(I+2))
TMNUM2=TMDEN2*(X(I)+X(I+2))
TMNUM3=TMDEN3*(X(I)+X(I+1))
DENOMR=TMDEN1+TMDEN2+TMDEN3
IF(DENOMR.EQ.0.0)GO TO 10
XX=0.5*(TMNUM1+TMNUM2+TMNUM3)/DENOMR
IF(XX.GE.X(I+2).OR.XX.LE.X(I))GO TO 10
GO TO 20
10 CONTINUE
RETURN
20 IF(IXY.EQ.1)WRITE(6,30)X(I),X(I+2)
30 FORMAT(1X,'ERROR IN CIF CURVE @ RTIM = ',E11.4,' TO ',E11.4,
1' (NOT SMOOTH)')
40 IF(IXY.EQ.2)WRITE(6,40)X(I),X(I+2)
FORMAT(1X,'ERROR IN CIF CURVE @ CIF = ',E11.4,' TO ',E11.4,
1' (NOT SMOOTH)')
STOP
END

```

## APPENDIX B (continued)

|   |   |  |
|---|---|--|
| C | SUBROUTINE CLEAR0<br>NEW DIMENSIONS 5/10/77 - JTH<br>DIMENSION L(87000)<br>CALL CLEAR(L,87000,0.0)<br>RETURN<br>END | CLE0 10<br>CLE0 20<br>CLE0 30<br>CLE0 40<br>CLE0 50<br>CLE0 60 |
| C | SUBROUTINE CLEAR2<br>NEW DIMENSIONS 5/10/77 - JTH<br>DIMENSION L(70000)<br>CALL CLEAR(L,70000,0.0)<br>RETURN<br>END | CLE2 10<br>CLE2 20<br>CLE2 30<br>CLE2 40<br>CLE2 50<br>CLE2 60 |

|   |  |  |
|---|--|--|
| C | ENTRY OFFER<br>WRITE REMAINING DATA ON FILE FOR POSSIBLE SAVING<br>IBB=2<br>IF(IWRT.EQ.1) GO TO 40<br>200 WRITE (10'1) JAM<br>PRINT 1310,MREC,LREC,NREC<br>1310 FORMAT(//1X,'MREC =',I4,5X,'LREC =',I4,5X,'NREC ='I4//)<br>PRINT 1320<br>1320 FORMAT(4X,'NTRY',5X,'LOREC',4X,'LOCREF')/<br>DO 210 I=1,NREC<br>210 PRINT 1300,NTRY(I),LOREC(I),LOCREF(I)<br>1300 FORMAT(1X,3I10)<br>IF(ISTOP.NE.0) STOP 10<br>RETURN<br>END | DEFE1230<br>DEFE1240<br>DEFE1250<br>DEFE1260<br>DEFE1270<br>DEFE1280<br>DEFE1290<br>DEFE1300<br>DEFE1310<br>DEFE1320<br>DEFE1330<br>DEFE1340<br>DEFE1350<br>DEFE1360<br>DEFE1370 |
|---|--|--|

## APPENDIX B (continued)

|    |  |          |
|----|--|----------|
| C  | SUBROUTINE DEFER   | DEFE 10  |
| C  | COMMON /HRLYS/ IYR,IMO,LOKN,IWRT,IKMPLT,IREC,JSTART,       | DEFE 20  |
| &  | NUMDYS,HDEW(24,31),HRAD(24,31),HWND(24,31),HTEM(24,31),    | DEFE 30  |
| &  | & IRIG,PKIRIG(87)  | DEFE 40  |
| &  | DIMENSION BUFFER(3072),JAM(154),NTRY(50),LOCREC(50),       | DEFE 50  |
| &  | & LOCREF(50)   | DEFE 60  |
| &  | EQUIVALENCE (IYR,BUFFER(1)), (MDUMY,JAM(1)),(MREC,JAM(2)), | DEFE 70  |
| &  | & (LREC,JAM(3)),(NREC,JAM(4)),(NTRY(1),JAM(5)),            | DEFE 80  |
| &  | & (LOCREC(1),JAM(55)),(LOCREF(1),JAM(105))                 | DEFE 90  |
|    | DATA MXREC/16/, MDUMY/0/, ISTOP/0/                         | DEFE 100 |
|    |  | DEFE 110 |
| C  | DEFINE RANDOM ACCESS FILE ON UNIT 10 WITH A MAXIMUM OF     | DEFE 120 |
| C  | MXREC RECORDS EACH OF LENGTH 3072 WORDS AND UNFORMATTED    | DEFE 130 |
| C  | ACCESS WITH ASSOCIATED VARIABLE IVAR                       | DEFE 140 |
| C  | MXREC MAY BE MADE AS LARGE AS 50 WITHOUT CHANGING THE      | DEFE 150 |
| C  | EQUIVALENCE STATEMENT ABOVE, BUT CHANGE DEFINE FILE TOO    | DEFE 160 |
| C  |  | DEFE 170 |
| C  | DEFINE FILE 10(MXREC,3072,U,IVAR)                          | DEFE 180 |
| C  | DEFINE FILE 10(16,3072,U,IVAR)                             | DEFE 190 |
| C  | ASK IBM WHY THIS WRITE IS NECESSARY!!!                     | DEFE 200 |
|    | WRITE (10'1) MDUMY   | DEFE 210 |
|    | MUREC=MXREC-1  | DEFE 220 |
|    | READ (10'1) JAM  | DEFE 230 |
|    | IF(LREC.EQ.3072) RETURN                                    | DEFE 240 |
| C  | THIS IS A NEW FILE SO SET UP REFERENCE INFORMATION         | DEFE 250 |
|    | DO 30 I=1,154  | DEFE 260 |
| 30 | JAM(I)=0   | DEFE 270 |
|    | MREC=MXREC   | DEFE 280 |
|    | LREC=3000  | DEFE 290 |
|    | RETURN   | DEFE 300 |
| C  | THE ARRAYS NTRY, LOCREC, AND LOCREF ALLOW INDEXING OF      | DEFE 310 |
| C  | RECORDS BY YEAR AND MONTH OR RECORD NUMBER WITH CROSS      | DEFE 320 |
| C  | REFERENCES FOR VALIDITY CHECKS WHEN WRITING RECORDS        | DEFE 330 |
| C  |  | DEFE 340 |
| C  | ENTRY PROPER   | DEFE 350 |
| C  | IBB=1  | DEFE 360 |
| C  | WRITE OUT RECORD IN BUFFER                                 | DEFE 370 |
| 40 | INTRY=IYR*12+IMO   | DEFE 380 |
|    | IF(IREC.GE.MUREC) GO TO 90                                 | DEFE 390 |
|    | IBR=1  | DEFE 400 |
| C  | GO FIND PROPER POSITION IN STACK IF NEW ENTRY              | DEFE 410 |
|    | IF(IREC.EQ.NREC+1) GO TO 140                               | DEFE 420 |
| C  | CHECK RECORD CROSS REFERENCES BEFORE STORING               | DEFE 430 |
|    | INDX=LOCREC(IREC)  | DEFE 440 |
|    | IF(NTRY(INDX).NE.INTRY) GO TO 95                           | DEFE 450 |
|    | IF(LOCREC(INDX).NE.IREC) GO TO 95                          | DEFE 460 |
|    | GO TO 80   | DEFE 470 |
| C  | RETURN TO HERE FROM TABLE SEARCH (STATEMENT 140)           | DEFE 480 |
| 60 | IF(IPPLACE.GT.NREC) GO TO 75                               | DEFE 490 |
| C  | PUSH PART OF STACK DOWN                                    | DEFE 500 |
|    | K=NREC   | DEFE 510 |
|    | DO 70 I=IPPLACE,NREC                                       | DEFE 520 |
|    | NTRY(K+1)=NTRY(K)  | DEFE 530 |
|    | LOCREC(K+1)=LOCREC(K)                                      | DEFE 540 |
|    | INDX=LOCREC(K+1)   | DEFE 550 |
|    | LOCREF(INDX)=LOCREF(INDX)+1                                | DEFE 560 |
| 70 | K=K-1  | DEFE 570 |
| 75 | NTRY(IPPLACE)=INTRY  | DEFE 580 |
|    |  | DEFE 590 |
|    |  | DEFE 600 |
|    |  | DEFE 610 |

## APPENDIX B (continued)

```

NREC=NREC+1 DEFE 620
LOCREC(IPLACE)=NREC DEFE 630
LOCREF(NREC)=IPLACE DEFE 640
C   WRITE OUT RECORD DEFE 650
80 KREC=IREC+1 DEFE 660
    WRITE (10'KREC) BUFFER DEFE 670
    GO TO (85,200),IBB DEFE 680
85 RETURN DEFE 690
C   ERROR MESSAGES DEFE 700
90 PRINT 1100,IREC,INTRY,IYR,IMO,LOKN,MUREC DEFE 710
1100 FORMAT('OPROFER - DATA FILE OVERFLOW ON RECORD',I3,
      & ' => ',I8,' (',I2,1H.,I2,A5,')/' ONLY',I3,
      & 'MONTHS DATA CAN BE STORED')
      RETURN DEFE 750
95 PRINT 1101,INTRY,IYR,IMO,LOKN DEFE 760
1101 FORMAT('OPROFER - FILE ENTRY FOR RECORD',I8,' (',I2,
      & 1H.,I2,A5,') NOT CONSISTANT')
      ISTOP=1 DEFE 780
      GO TO 200 DEFE 790
DEFE 800
C   ENTRY GOFER(IYEAR,MONTH,NXREC) DEFE 810
C   RETRIEVE DATA FOR YEAR "IYEAR" AND MONTH "MONTH" DEFE 820
C   IF IT IS ON FILE IN WHICH EVENT NXREC=0. DEFE 830
C   OTHERWISE SET NXREC=NREC+1, THE NEXT AVAILABLE DEFE 840
C   RECORD. DEFE 850
DEFE 860
C   INTRY=IYEAR*12+MONTH DEFE 870
NXREC=NREC+1 DEFE 880
IF(NREC.EQ.0) GOTO 110 DEFE 890
IBR=2 DEFE 900
C   BRANCH TO SEARCH PROCEDURE FOR ENTRY IN TABLE DEFE 910
GO TO 140 DEFE 920
DEFE 930
C   RETURN FROM SEARCH FOR ENTRY IN TABLE DEFE 940
100 IF(IPLACE.GT.NREC) GO TO 110 DEFE 950
IF(NTRY(IPLACE).NE.INTRY) GO TO 110 DEFE 960
DEFE 970
C   FOUND RECORD REFERENCE, NOW READ RECORD DEFE 980
KREC=LOCREC(IPLACE)+1 DEFE 990
READ(10'KREC,ERR=120) BUFFER DEFE 1000
NXREC=0 DEFE 1010
110 RETURN DEFE 1020
120 PRINT 1200,INTRY,IYR,IMO,LOKN DEFE 1030
1200 FORMAT('OGOFER - FILE ENTRY FOR RECORD',I8,' (',I2,
      & 1H.,I2,A5,') IN ERROR')
      ISTOP=1 DEFE 1040
      GO TO 200 DEFE 1050
DEFE 1060
C   * BEGIN PROCEDURE TO FIND DESIRED ENTRY IN TABLE *
C   140 IF(NREC.EQ.0) GO TO 155 DEFE 1070
C   140 IF(NTRY.GE.8) GO TO 160 DEFE 1080
C   USE SIMPLE SEQUENTIAL SEARCH IF LESS THAN 8 ENTRIES DEFE 1090
DO 150 I=1,NREC DEFE 1100
IPLACE=I DEFE 1110
IF(NTRY(I).GE.INTRY) GO TO 160 DEFE 1120
150 CONTINUE DEFE 1130
155 IPLACE=NREC+1 DEFE 1140
160 GO TO (60,100), IBR DEFE 1150
C   USE BINARY SEARCH DEFE 1160
C   END SEARCH PROCEDURE DEFE 1170
C   DEFE 1180
DEFE 1190
DEFE 1200
DEFE 1210
C   DEFE 1220

```

## APPENDIX B (continued)

```

SUBROUTINE EVAL(Y,P)                                EVAL  0
IMPLICIT REAL*8 (A-H,O-Z)                         EVAL  5
REAL*8 LWPB,LLWP,LWPA                            EVAL 10
COMMON/RESIST/R1,R2,R3,R4,R5,RR1,RRA,RRB,RRC,RRR,TM,RLIT
COMMON/SURF/PWPS,PWPW,PWPMAX,RESS,RESW,RESMAX,POWS,POWW,POWER , EVAL 15
> LRMODL
COMMON/PORES/VP(8),F,S(8),SEV,ETGW,DNFAC,WP1,WP2,NSL,NBL,NS
COMMON/HUMID/FOLTyp,PAIR,CPO,RA,RX,SIGMA,XL,GM,GV,HT,ALEAF
COMMON /BLOCKE/ RN,GND,TTT,EE,PWP,EV,VEL,JDATE
COMMON /SOLPOT/PSI(8)                               EVAL 20
C      DETERMINE ELECTRICAL ANALOG PARAMETERS          EVAL 25
RR=R4+RR1                                         EVAL 30
D=R1+R2+R5                                         EVAL 35
RT1=R1*R5/D                                         EVAL 40
RT2=R1*R2/D                                         EVAL 45
RT3=R2*R5/D+RR                                     EVAL 50
D=RT1+RT3+R3+RLIT                                 EVAL 55
RRA=RT2+RT1*RT3/D                                 EVAL 60
RRB=(R3+RLIT)*RT3/D                               EVAL 65
RRC=(R3+RLIT)*RT1/D                               EVAL 70
D=RRA+RRC                                         EVAL 75
C      MODEL OF LEAF RESISTANCE VS LEAF WATER POTENTIAL EVAL 80
C      Y IS LEAF WATER POTENTIAL IN MILLIBARS AND IS NEGATIVE EVAL 85
IF (TM.GE.RESMAX) GO TO 30                         EVAL 90
IF (LRMODL.EQ.0) GO TO 10                         EVAL 95
C      HYPERBOLIC RELATION                           EVAL 100
LWPB=1.0D-3*Y                                      EVAL 105
C      LWPB IS LEAF WATER POTENTIAL IN BARS          EVAL 110
LLWP=PWPMAX*(TM/RESMAX-1)                          EVAL 115
IF (LWPB.LE.LLWP) GO TO 30                         EVAL 120
RRR=TM/(1.+LWPB/PWPMAX)                           EVAL 125
GO TO 40                                           EVAL 130
C      EXPONENTIAL RELATION                         EVAL 135
10 LWPA=9.81D-4*Y                                  EVAL 140
C      LWPA IS LEAF WATER POTENTIAL IN ATMOSPHERES   EVAL 145
IF (LWPA.LT.0) GO TO 20                           EVAL 150
RRR=TM                                              EVAL 155
GO TO 40                                           EVAL 160
C      ENTRY POINT GOES HERE                         EVAL 165
20 IF (LWPA.LT.-PWPMAX) GO TO 30                  EVAL 170
RRR=TM+(RESMAX-TM)*DEXP(POWER*(LWPA+PWPMAX))    EVAL 175
GO TO 40                                           EVAL 180
30 RRR=RESMAX                                       EVAL 185
40 RX=RRR                                         EVAL 190
C      COMPUTE SURFACE RESISTANCE                   EVAL 195
CALL EVAPOR(EV,RN,GND,TTT,EE,ETGW)                EVAL 200
P=-(Y-(RRA*PSI(1)/D+RRC*PSI(2)/D))/(RRB+RRA*RRC/D)-EE
RETURN                                            EVAL 205
C      DETERMINE EVAPOTRANSPIRATION                 EVAL 210
ENTRY FEVAL(Y,P)                                    EVAL 215
CALL FEVAP(EE,ETGW)                                EVAL 220
P=-(Y-(RRA*PSI(1)/D+RRC*PSI(2)/D))/(RRB+RRA*RRC/D)-EE
RETURN                                            EVAL 225
C      DETERMINE EVAPOTRANSPIRATION                 EVAL 230
ENTRY FEVAL(Y,P)                                    EVAL 235
CALL FEVAPO(EE,ETGW)                                EVAL 240
P=-(Y-(RRA*PSI(1)/D+RRC*PSI(2)/D))/(RRB+RRA*RRC/D)-EE
RETURN                                            EVAL 245
C      DETERMINE EVAPOTRANSPIRATION                 EVAL 250
ENTRY FEVAL(Y,P)                                    EVAL 255
CALL FEVAPO(EE,ETGW)                                EVAL 260
P=-(Y-(RRA*PSI(1)/D+RRC*PSI(2)/D))/(RRB+RRA*RRC/D)-EE
RETURN                                            EVAL 265
C      DETERMINE EVAPOTRANSPIRATION                 EVAL 270
ENTRY FEVAL(Y,P)                                    EVAL 275
CALL FEVAPO(EE,ETGW)                                EVAL 280
P=-(Y-(RRA*PSI(1)/D+RRC*PSI(2)/D))/(RRB+RRA*RRC/D)-EE
RETURN                                            EVAL 285
C      DETERMINE EVAPOTRANSPIRATION                 EVAL 290
ENTRY FEVAL(Y,P)                                    EVAL 295
CALL FEVAPO(EE,ETGW)                                EVAL 300
P=-(Y-(RRA*PSI(1)/D+RRC*PSI(2)/D))/(RRB+RRA*RRC/D)-EE
RETURN                                            EVAL 305
C      DETERMINE EVAPOTRANSPIRATION                 EVAL 310
ENTRY FEVAL(Y,P)                                    EVAL 315
CALL FEVAPO(EE,ETGW)
P=-(Y-(RRA*PSI(1)/D+RRC*PSI(2)/D))/(RRB+RRA*RRC/D)-EE
RETURN
END

```

## APPENDIX B (continued)

```

C SUBROUTINE GETSET(GA,DCS,TE,TS,YR1,YR2) GETS 10
C COMMON/DAILY/DEW(12,31), RAD(12,31), EVAP(12,31), TEM (2,12,31), GETS 20
C > WINDS(12,31), IDEW(36),IRAD(36),ITEM(36),IWND(36) GETS 30
C INTEGER*2 IDEW,IRAD,ITEM,IWND GETS 40
C COMMON /HRLYS/ IYR,IMO,LOKN,IWRT,IKMPLT,IREC,JSTART, NUMDYS, GETS 50
C > HDEW(24,31),HRAD(24,31),HWND(24,31),HTEM(24,31), GETS 60
C > IRIG,PKIRIG(87) GETS 70
C COMMON /ANGLES/ FILL(6),DGLAT,DLONG GETS 80
C COMMON/SSRF/PORE,SBD(5),KSAT(5),SA(5),KSGW,CUT,CUTL,WUP GETS 90
C COMMON/TLYR/NTL GETS 100
C COMMON/SSF/SSG(5) GETS 110
C COMMON/THSRF/WCK1,WCK2 GETS 120
C COMMON/FLAGS/KTEMP,KDEW,KRAD,KWIND,KSNOW,KLAND,KSOILM,KPE GETS 130
C COMMON/AR/AREA1,AREA2,PA GETS 140
C COMMON/AWYPLC/NU1(10),NU2(10),NU3(10),TITL(10,6),NPLTS,NAWPLT GETS 150
C COMMON/CM/CMMO,CMYR GETS 160
C INTEGER CMMO,CMYR GETS 170
C COMMON/PRSPLC/NPRPLT,NMPLT,NSPLTS,NMSPLT,MONSPL(12),MONPLT(12), GETS 180
C > PORPLT(36),NBEG(12),NEND(12),MACHIN GETS 190
C COMMON/PLTALL/XMIN,XMAX,INC1,ISTRA,NQUES GETS 200
C REAL MACHIN GETS 210
C INTEGER#2 MONSPL,MONPLT,PORPLT,NBEG,NEND GETS 220
C COMMON/SHIFT1/ RADCON,CONNLT,SCF,ELDIF, IDNS,FCI,DGM,WC, MPACK, K1,GETS 230
C > A, LG, SS, NN, K24L, EPXM,SUNCON,CLD,CLDFAC GETS 240
C COMMON/PORES/VP(8),F,S(8),SEV,ETGW,DNFAC,WP1,WP2,NSL,NBL,NS GETS 250
C COMMON/SURFXP/RZ,PR,ORAIN,FF,FIXM,RGX,SHRD,A3,AUZZ,ASDS,AINF GETS 260
C COMMON/INVG/A,NAME(6),ELEV,LAT(3),LONG(3),GTYP(2), GETS 270
C > INTRVL,ELEM(5), INITP,DSNAME,STRTYR,ENDYR, INITS,RODSNA,ROSTYR, GETS 280
C > RENDYR, INITD,DDSNAM,DSTYR,DENDYR, INITR,DSDSNA,DSSTYR, DSENDY, GETS 290
C > FRADCN,FCNMLT,FSCF,FELDF,FDNS,FFCI,FDCM,FWC,FMPACK, FK1,FA, FL,GETS 300
C > FSS, FNN, FK24L, FEPXM, GETS 310
C THE FOLLOWING 13 PARAMETERS TEMPORARILY REMOVED 12 19 75 GETS 320
C + BARES, ANOTS, KDS, LFTOVS, OCRITS, ONCRTS, AZEROS, SDPM, SEDMPSGETS 330
C + .SONES, STWOS, STRES, SFORS, GETS 340
C + SGWINV,LZSINV,LIQW,DEPTH,NEMELT,PACK,KEYTIM, DUM1,DUM2,UNUSED(24) GETS 350
C COMMON/GEOMET/DL(8),AT(2),ARAT(2),FC(8),THETA(8),SWT(8) GETS 360
C COMMON/LOCATE/ELONG GETS 370
C COMMON/OPTS/CHMOPT,CEROPT,DRYOPT GETS 380
C LOGICAL CHMOPT,CEROPT,DRYOPT GETS 390
C COMMON/GET/STCLD,MONTHP(12),EPXMIN, EPXMAX,RNON,SUNHR(24),DUST(12)GETS 400
C > ,Y,M,T(744),JJ GETS 410
C COMMON/IMPAR/WT,WT1,WT2,ISWIWT GETS 420
C DIMENSION SNOPAK(4),SOILM(4),SNOPAR(9), SLTEMP(16), GETS 430
C > SEGMENT(49),DCS(13), INDATA(8),ID(12) GETS 440
C REAL#8 SLBL(4),SA,RLNLBL(10),AREA1,AREA2,THETA ,SBD,SSG,CUT,WUP, GETS 450
C > PORE,CUTL,KSAT,KSGW, PA,DL,AT,ARAT,FC,SWT,VP,F,S,SEV,ETGW,STCLD, GETS 460
C > DNFAC,WP1,WP2,TLBL(6),WCK1,WCK2,RNTL,WT,WT1,WT2 GETS 470
C INTEGER Y,BZ,GA,TS,ENDYR,STRTYR,DCS,TEM , YR1,YR2,RODSNA, GETS 480
C > ROSTYR,RENDYR,DSTYR,DENDYR,DSDSNA,DSSTYR, DSNAME,DSENDY GETS 490
C REAL K24L,NN,LANPAR(7),LZSINV,MPACK,K1,LG, IDNS,LIQW,NEMELT GETS 500
C INTEGER DSNAME,DSENDY GETS 510
C EQUIVALENCE (SOILM(1),SGWINV),(INDATA(1),KTEMP), (SEGMENT(1), GETS 520
C > SNOPAR(1),FRADCN),(SNOPAK(1),LIQW), (LANPAR(1),FK1), (SLTEMP(1), GETS 530
C > RADCON) GETS 540
C DATA SLBL/'SGW=      ','LZS=      ','FIXM=      ','FF=      '/ GETS 550
C DATA RLNLBL/'BARE=','ANOT=','KD=','LFTOV=','OCRIT=','ONCRT=', GETS 560
C > 'AZERO=','SDPM=','SEDMP=','SONE='/ GETS 570
C DATA TLBL/'K1=','A=','LG=','SS=','NN=','K24L='/ GETS 580
C DATA KPLUS/'+'/ GETS 590

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## APPENDIX B (continued)

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C                                     GETS 620
NBZ = 8                               GETS 630
10 INDATA(NBZ) = 1                   GETS 640
C                                     GETS 650
ENTRY ONMARK(GA,DCS,TE,TS,YR1,YR2)   GETS 660
CALL DATIM(TS,IY,MO,ID,IH,IMN)       GETS 670
LM=MO-1                               GETS 680
IF (LM.EQ.0) LM=12                  GETS 690
READ 10000, NBZ,NSCL, BZ             GETS 700
WRITE(6,10100) NBZ,BZ               GETS 710
GO TO (30,40,60,50,100,110,180,120,140,150,160,80,70,90,170,200,    GETS 720
> 165,20),NBZ                      GETS 730
20 PRINT 10200                      GETS 740
STOP 3004                           GETS 750
30 SFAC=1.                           GETS 760
IF (NSCL.EQ.KPLUS) SFAC=.1          GETS 770
READ 10300,DCS(13)                 GETS 780
CALL DAYTEM(BZ,TEM,HTEM,ITEM,SFAC,DCS(13),&10)   GETS 790
C                                     TEM(1,M,D)=DAILY MAXIMUM TEMPERATURE, TEM(2,M,D)=MIN
40 CALL DAYIN(BZ,DEW,HDEW,IDEW,&10)   GETS 800
50 CALL DAYIN(BZ,WINDS,HWND,IWND,&10)   GETS 810
60 CALL DAYIN(BZ,RAD,HRAD,IRAD,&10)   GETS 820
70 NBZ = 3                           GETS 830
CALL BIMON(BZ,RAD,HRAD,IRAD,&10)     GETS 840
80 NBZ = 2                           GETS 850
CALL BIMON(BZ,DEW,HDEW,IDEW,&10)     GETS 860
90 NBZ = 4                           GETS 870
CALL BIMON (BZ,RAD,HRAD,IRAD,&10)    GETS 880
100 READ 10400,SNOPAR, SNOPAK      GETS 890
DCS(10)=1                           GETS 900
GO TO 10                            GETS 910
110 READ 10500, (LANPAR(I),I=1,5),ISWIWT   GETS 920
INC1=0                               GETS 930
READ(5,10600)EPXMAX,EPXMIN,RNON,CMMO,CMYR,NAWPLT,NPRPLT,NSPLTS   GETS 940
WRITE(6,11000) EPXMAX,EPXMIN,RNON,CMMO,CMYR,NAWPLT, NPRPLT,NSPLTS GETS 950
EPXMAX=EPXMAX/2.54                  GETS 960
EPXMIN=EPXMIN/2.54                  GETS 970
IF (NAWPLT.NE.0) READ(5,10900) NPLTS,(NU1(I),NU2(I),NU3(I),      GETS 980
> (TITL(I,J),J=1,6),I=1,NPLTS)    GETS 990
IF (NPRPLT.NE.0) READ(5,10700) NMPLT,(MONPLT(I),(PORPLT(J+(I-1)*3)GETS 1000
> ,J=1,3),I=1,NMPLT)              GETS 1010
IF (NSPLTS.NE.0) READ(5,10800) NMSPLT,MACHIN,(MONSPL(I),NBEG(I) , GETS 1020
> NEND(I),I=1,NMSPLT)             GETS 1030
GO TO 10                            GETS 1040
120 READ 11200,AREA1,CUT,CUTL,WUP,RNTL   GETS 1050
C                                     AREA1 IS THE MINIMUM EXTENT OF SOURCE AREAS
C                                     CUTL IS THE DRAIN RATE WHEN DEEP SOILS BEGIN TO DRAIN TO CHANNEL
C                                     CUT IS THE DRAIN RATE WHEN MAX. FRACTION OF DEEP SOILS
C                                     DRAINING TO CHANNEL (WUP) IS REACHED.
C                                     RNTL IS THE NUMBER OF SOIL TRANSMISSION LAYERS CONSIDERED.
C                                     AREA2= 1.0 - AREA1
C                                     NTL= IFIX(SNGL(RNTL))
C                                     READ 11200,(SBD(I),I=1,NTL)
C                                     SBD IS THE LAYER THICKNESS OF TRANSMISSION LAYERS (CM).
C                                     READ 11200,(SSG(I),I=1,NTL)
C                                     SSG IS THE VOLUMETRIC WATER CONTENT -- CONVERTED TO INCHES BELOW.
DO 130 K=1,NTL                      GETS 1110
130 SSG(K)=SSG(K)*SBD(K)            GETS 1120
READ 11200,PORE,((KSAT(I),SA(I)),I=1,3),WCK1,WCK2      GETS 1130
C                                     PORE IS THE FRACTIONAL PORE SPACE FOR ALL TRANSMISSION LAYERS
C                                     KSAT AND SA CHARACTERIZE 3 LIMBS OF THE K VS. THETA CURVE,
GETS 1140
GETS 1150
GETS 1160
GETS 1170
GETS 1180
GETS 1190
GETS 1200
GETS 1210
GETS 1220

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## APPENDIX B (continued)

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C      FROM LOW TO HIGH K VALUES.                                GETS1230
C      WCK1 AND WCK2 ARE BREAKPOINTS (THETAS) BETWEEN LIMBS (1&2)   GETS1240
C      AND (2&3).                                                 GETS1250
C      READ 11100,KSGW,SGW,K24L                                     GETS1260
C      SGW=SGW/2.54D0                                              GETS1270
C      KSOILM=1                                                 GETS1280
C      SGWINV=SGW                                              GETS1290
C      LANPAR(6)=K24L                                             GETS1300
C      KSGW IS THE CONSTANT THAT RELATES GW FLOW TO GW STORAGE, I.E.  GETS1310
C      GWF=KSGW*SGW, AND HAS UNITS 1/HOUR.                         GETS1320
C      SGW IS THE GW STORAGE (CM)                                    GETS1330
C      K24L IS THE FRACTION OF GW LOST TO DEEP SEEPAGE ACROSS THE  GETS1340
C      WATERSHED DIVIDE.                                         GETS1350
C      KSSRF = 1                                                 GETS1360
C      WRITE(6,11300) AREA1,CUT,CUTL,WUP,RNTL                      GETS1370
C      WRITE(6,11400) (SBD(I),I=1,NTL)                            GETS1380
C      WRITE(6,11500) (SSG(I),I=1,NTL)                            GETS1390
C      WRITE(6,11600) PORE,((KSAT(I),SA(I)),I=1,3),WCK1,WCK2       GETS1400
C      WRITE(6,11700) KSGW,SGW,K24L                               GETS1410
C      GO TO 10                                                 GETS1420
140 CALL RDCHM                                              GETS1430
C      GO TO 10                                                 GETS1440
150 CALL RDCER                                              GETS1450
C      GO TO 10                                                 GETS1460
160 CALL RDDRY                                              GETS1470
C      GO TO 10                                                 GETS1480
165 CONTINUE                                                 GETS1490
CALL RDIRIG                                              GETS1500
C      GO TO 10                                                 GETS1510
170 NBZ=8                                                 GETS1520
CALL EVAPO (YR1,YR2,BZ,&10)                                 GETS1530
180 DGLAT=LAT(1)+LAT(2)/60.+LAT(3)/3600.                     GETS1540
DLONG=LONG(1)+LONG(2)/60.+LONG(3)/3600.                   GETS1550
CALL READIN                                              GETS1560
LZSINV=0.                                                 GETS1570
DO 190 K=1,NSL                                              GETS1580
190 LZSINV=LZSINV + THETA(K)/2.54                           GETS1590
C      GO TO 10                                                 GETS1600
200 WRITE(6,11800) NAME,STANF,WB,TS,TE                      GETS1610
IF (KLAND.EQ.0) WRITE(6,11900)                                GETS1620
C      THE FOLLOWING OPTION IS NOT APPLICABLE IN THE TEHM AT PRESENT  GETS1630
C      HOWEVER, IT MAY BE ADDED BACK INTO THE CODE WHEN APPROPRIATE.  GETS1640
C      READ 79, (MONTHP(I),I=1,12), NOPOS                      GETS1650
C79  FORMAT (13I5)                                            GETS1660
IF (KPE.EQ.0) WRITE(6,12000)                                GETS1670
IF (KSOILM.EQ.0) WRITE(6,12100)                            GETS1680
IF (KTEMP.EQ.0) GO TO 250                                  GETS1690
IF ((DCS(10).GT.0).AND.(KSNOW.GT.0)) GO TO 240            GETS1700
WRITE(6,12200)                                              GETS1710
DO 230 I = 1, 4                                           GETS1720
230 SNOPAK(I) = 0.0                                         GETS1730
DO 235 L=1,9                                              GETS1740
235 SNOPAR(L)=0.                                           GETS1750
240 IF (KRAD.EQ.0) WRITE(6,12300)                           GETS1760
250 DO 260 L = 1, 16                                         GETS1770
260 SLTEMP(L) = SEGMENT(L)                                 GETS1780
IF (A.LE.1.0.AND.K24L.LE.1.0.AND.NN.LE.1.0) GO TO 270    GETS1790
PRINT 12400,((TLBL(I),SLTEMP(I+9)),I=1,6)                GETS1800
STOP 3005                                                 GETS1810
270 WRITE(6,12500) STRYR,ENDYR,LAT,LONG,ELEV,GTYPE        GETS1820
WRITE(6,12600) ((TLBL(I),SLTEMP(I+9)),I=1,6)              GETS1830

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## APPENDIX B (continued)

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C      EROSION REMOVED UNTIL IT CAN BE UPDATED FOR SOURCE AREAS.      GETS1840
IF (KLAND.EQ.1) LANPAR(3)=LANPAR(3)*3.28084                      GETS1850
FIXM=1.0                           GETS1860
FF=1.0                            GETS1870
DO 272 I=1,12                         GETS1880
272 DUST(I)=0.                         GETS1890
C      WRITE(6,2017) (RLNLBL(I),RLNPAR(I),I=1,10)                   GETS1900
CC2017 FORMAT ('OBASIN RADIOAEROSOL INVENTORY AND STARTING PARAMETERS'//GETS1910
C      + 2(3X,A6,F7.2,4(' ', 'A6,F7.2//))                         GETS1920
      WRITE(6,12700) (SLBL(I),SOILM(I),I=1,2),SLBL(3),FIXM,SLBL(4),FF   GETS1930
IF (KSSRF.EQ.1) GO TO 280                                         GETS1940
      WRITE(6,13100) GA                                           GETS1950
      PORE = .304D0                                         GETS1960
      DO 275 J=1,5                                         GETS1970
      SBD(J) = 9.0D01                                         GETS1980
275  SSG(J) = 2.07D01                                         GETS1990
      AREA1 = 0.05D0                                         GETS2000
      AREA2 = 0.95D0                                         GETS2010
      KSAT(1)=39.63586D0                                     GETS2020
      SA(1)=95.56D0                                         GETS2030
      KSAT(2)=1.19606D02                                     GETS2040
      SA(2)=1.422D02                                         GETS2050
      KSAT(3)=2.505879D02                                    GETS2060
      SA(3)=5.12D02                                         GETS2070
      KSGW=1.0D-03                                         GETS2080
280  WRITE(6,12800) NTL                                         GETS2090
      WRITE(6,12900) (I,SBD(I),SSG(I),I=1,NTL)                 GETS2100
      WRITE(6,13000) (I,KSAT(I),SA(I),I=1,3),WCK1,WCK2,AREA1,WUP,
> CUTL,CUT                                         GETS2110
      DO 290 K=1,NTL                                         GETS2120
      SBD(K)=SBD(K)/2.54                                     GETS2130
      SSG(K)=SSG(K)/2.54                                     GETS2140
290  CONTINUE                                         GETS2150
      IF (KSNOW.GT.0) WRITE(6,13200) SNOPAR,SNOPAK             GETS2160
      PRINT 13300, DCS(10),DCS(13)                           GETS2170
      ELONG=LONG(1)                                         GETS2180
      IF (LONG(2).GE.30.) ELONG=LONG(1)+1.                  GETS2190
      RETURN                                         GETS2200
10000 FORMAT (I2,A1,A4)                                         GETS2210
10100 FORMAT (/1X,I2,2X,A4)                                         GETS2220
10200 FORMAT('OERROR, UNKNOWN CONTROL LABEL IN LAND SURFACE SIMULATION')GETS2230
10300 FORMAT(I1)                                         GETS2240
10400 FORMAT( 9F6.2,4F5.2)                                         GETS2250
10500 FORMAT (5F5.1,I5)                                         GETS2260
10600 FORMAT(3F10.4,10X,5I1)                                         GETS2270
10700 FORMAT(I5,(4I2))                                         GETS2280
10800 FORMAT(I5,A4,(3I2))                                         GETS2290
10900 FORMAT(I2,(3I2,6A4))                                         GETS2300
11000 FORMAT(5X,'EPXMAX=',F8.4,' EPXMIN=',F8.4,' RNON=',F8.4, ' CMMO=',
> I2, 'CMYR=',I2,'NAWPLT=',I2,' NPRPLT=',I2 , 'NSPLTS=',I2)    GETS2310
11100 FORMAT(D10.5,2F10.5)                                         GETS2320
11200 FORMAT(10D8.0)                                         GETS2330
11300 FORMAT(1X,'AREA1,CUT,CUTL,WUP,RNTL= ',5G12.6)          GETS2340
11400 FORMAT(1X,'SBD(I)= ',5(1X,G12.6))                         GETS2350
11500 FORMAT(1X,'SSG(I)= ',5(1X,G12.6))                         GETS2360
11600 FORMAT(1X,'PORE,KSAT&SA,WCK1,WCK2= ',7(1X,G12.6)/2(1X,G12.6))  GETS2370
11700 FORMAT(1X,'KSGW,SGW,K24L= ',3(1X,G12.6))                GETS2380
11800 FORMAT ('LAND SURFACE SIMULATION FOR SEGMENT AT ',6A4,
> 'STANFORD NO= ',I3, 5X,'WEATHER BUREAU NO= ',I6/10X,'PERIOD = ',
> Z8,' TO ', Z8,' (HEX)')                                         GETS2390
11900 FORMAT ('OLAND SURFACE PARAMETERS WERE ASSIGNED FROM FILE')    GETS2400

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## APPENDIX B (continued)

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12000 FORMAT ('OWARNING, POTENTIAL EVAPOTRANSPIRATION HAS BEEN CARRIED FGETS2450
>ROM THE PREVIOUS SEGMENT') GETS2460
12100 FORMAT ('OWARNING, INITIAL SOIL MOISTURES WERE ASSIGNED BY DEFAULTGETS2470
>; STARTING DATE NOT ON FILE') GETS2480
12200 FORMAT ('OWARNING, INITIAL SNOWPACK CONDITIONS WERE ASSIGNED BY DEGETS2490
>FAULT; STARTING DATE NOT ON FILE') GETS2500
12300 FORMAT ('OWARNING, RADIATION HAS BEEN CARRIED FROM THE PREVIOUS SEGETS2510
>GMENT') GETS2520
12400 FORMAT ('OEXECUTION DELETED DUE TO UNREASONABLE LAND SURFACE PARAMGETS2530
>ETERS //10X,6(A6,F6.3,3X)) GETS2540
12500 FORMAT ('ORAINGAGE RECORDS START AT WY',I3,', END AT WY',I3/
> ' LOCATION=',1X,3(1X,I2),' LATITUDE, ',I3,2(1X,I2),' LONGITUDE'/GETS2550
> ' ELEVATION=',I5,' FEET// EQUIPMENT= ',A4,A4/) GETS2570
12600 FORMAT ('OLAND SURFACE PARAMETERS//(3X,A6,F7.2,5(', ',A6,F7.2) /GETS2580
> //)) GETS2590
12700 FORMAT ('OSOIL MOISTURE PARAMETERS//3X, A6,F7.2,3(', ', A6,F7.2)GETS2600
> //) GETS2610
12800 FORMAT(1X,'SUBSURFACE AND SOURCE AREA PARAMETERS: //4X, GETS2620
> 'THERE ARE ',I1,' SOIL WATER TRANSMISSION LAYERS AS FOLLOWS://') GETS2630
12900 FORMAT(8X,'LAYER',4X,'THICKNESS (CM)',4X,'WATER CONTENT (CM)'/ GETS2640
> (10X,I1,7X,G12.6,8X,G12.6/)) GETS2650
13000 FORMAT(/4X,'CONDUCTIVITY CURVE PARAMETERS: //8X,'INDEX',8X, GETS2660
> 'KSAT(INDEX)',8X,'SA(INDEX)//3(10X,I1,10X,G12.6,9X,G12.6/),/ GETS2670
> 4X,'BREAKPOINTS (THETA VALUES) IN CONDUCTIVITY CURVES:', GETS2680
> 2(3X,G12.6)//4X,'MINIMUM AND MAXIMUM EXTENT OF SOURCE AREAS (DE',GETS2690
> 'CIMAL):',2(3X,G12.6)//4X,'DRAINAGE RATES (CM/DAY) AT LOWER AND 'GETS2700
> , 'UPPER SOURCE AREA EXTENTS:',2(3X,G12.6/)) GETS2710
13100 FORMAT(5X,'SUBSRF PARAMETERS ASSIGNED BY DEFAULT FOR', GETS2720
> ' SEGMENT =',I4) GETS2730
13200 FORMAT('OSNOWPACK PARAMETERS'/3X,'RADCON',3X,'CONMLT',4X,'SCF',5X,GETS2740
> 'ELDIF',5X,'INDS',6X,'FCI',6X, 'DGM',6X,'WC',5X,'MPACK',5X, GETS2750
> 'LIQW',5X,'DEPTH',3X,'NEMELT',4X,'PACK'/13(F8.3,1X)) GETS2760
13300 FORMAT('DCS(10)= ',I2,' DCS(13)= ',I2/) GETS2770
END GETS2780

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## APPENDIX B (continued)

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SUBROUTINE HRADSL(DY,HRAD,HNRAD)          HRAD 10
C
C      MODEL THE DIURNAL VARIATION OF THE SOLAR    HRAD 20
C      RADIATION INCIDENT ON A SLOPE               HRAD 30
C
C      COMMON /ANGLES/ RADINC,RADLAT,DELONG,PI,D,EQLAT,DLAT,DLONG   HRAD 40
C      REAL#8 RADINC                                         HRAD 50
C      DIMENSION HRAD(24),HNRAD(24)
C
C      DAYL(SINL,COSL)=ARCOS(AMAX1(-1.,AMIN1(1.,-SINL/COSL*TANDEC)))  HRAD 60
C
C      TH=RADINC                                         HRAD 70
C      SECINC=1./COS(TH)                                HRAD 80
C      DIFUSE RADIATION FROM THE SKY                  HRAD 90
C      ASSUME TO BE 5% OF POTENTIAL SOLAR RADIATION  HRAD 100
C      RDIFUS=.056*(1.-RADINC/3.1415926)*SECINC      HRAD 110
C      DO 10 IH=1,24
10   HNRAD(IH)=RDIFUS*HRAD(IH)             HRAD 120
C      DIRECT RADIATION FROM THE SUN                HRAD 130
C      AT=.01720242*DY-1.41430                   HRAD 140
C      BT=.033446*SIN(.01720242*DY-.059075)       HRAD 150
C      SINET=SIN(AT+BT)                           HRAD 160
C      SINDEC=.39785*SINET                         HRAD 170
C      COSDEC=SQRT(1.-SINDEC*SINDEC)              HRAD 180
C      TANDEC=SINDEC/COSDEC                      HRAD 190
C      SUNRISE AND SUNSET ON THE SLOPE            HRAD 200
C      SINEQ=SIN(EQLAT)                          HRAD 210
C      COSEQ=COS(EQLAT)                         HRAD 220
C      SKIP IF SUN DOES NOT RISE ON SLOPE        HRAD 230
C      IF(COSEQ.LE.-SINEQ*TANDEC) GO TO 70       HRAD 240
C      TS=DAYL(SINEQ,COSEQ)                      HRAD 250
C      TS1=(-TS-DELONG)/.2617994                 HRAD 260
C      TS2=(TS-DELONG)/.2617994                 HRAD 270
C      EQUATI=3.819718*ATAN2(SIN(BT)-.082549*SINET*COS(AT),  HRAD 280
C      & COS(BT)-.082549*SINET*SIN(AT))           HRAD 290
C      SNOON=12.-(AINT(DLONG/15.+.5)-DLONG/15.)+EQUATI  HRAD 300
C      IF(TS1.LT.-SNOON) TS1=TS1+24.                HRAD 310
C      IF(TS2-24.0.GT.-SNOON) TS2=TS2-24.0         HRAD 320
C      SUNRISE AND SUNSET ON THE HORIZONTAL        HRAD 330
C      RLAT=.01745329*DLAT                         HRAD 340
C      SINLAT=SIN(RLAT)                           HRAD 350
C      COSLAT=COS(RLAT)                          HRAD 360
C      SKIP IF SUN DOES NOT RISE ON HORIZONTAL    HRAD 370
C      IF(COSLAT.LE.-SINLAT*TANDEC) GO TO 70       HRAD 380
C      TH2=DAYL(SINLAT,COSLAT)/.2617994          HRAD 390
C      TH1=-TH2                                     HRAD 400
C      NUMBER OF SUNRISES ON SLOPE MAY BE 0, 1, OR 2  HRAD 410
C      NUMSR=1                                     HRAD 420
C      IF(TS1.GT.TS2) GO TO 20                     HRAD 430
C      TS1=AMAX1(TS1,TH1)                         HRAD 440
C      TS2=AMIN1(TS2,TH2)                         HRAD 450
C      GO TO 40                                     HRAD 460
20   IF(TH2.GT.TS1) GO TO 30                   HRAD 470
C      TS1=TH1                                     HRAD 480
C      GO TO 40                                     HRAD 490
30   IF(TS2.GT.TH1) GO TO 35                   HRAD 500
C      TS2=TH2                                     HRAD 510
C      GO TO 40                                     HRAD 520
35   TS4=TH2                                     HRAD 530
C      TS3=TS1                                     HRAD 540
C

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## APPENDIX B (continued)

```

TS1=TH1          HRAD 620
NUMSR=2          HRAD 630
40 IF(TS1.GE.TS2) GO TO 70          HRAD 640
TH1=TS1          HRAD 650
I1=TH1+SNOON+1. HRAD 660
TH2=I1-SNOON    HRAD 670
I2=TS2+SNOON+1. HRAD 680
C               HRAD 690
DO 60 IH=I1,I2  HRAD 700
RATIO=1.          HRAD 710
IF(RADINC.EQ.0.) GO TO 50          HRAD 720
T1=.2617994*TH1          HRAD 730
T2=.2617994*TH2          HRAD 740
PRAD=SINDEC*SINLAT*(T2-T1)+COSDEC*COSLAT*(SIN(T2)-SIN(T1))  HRAD 750
SRAD=SINDEC*SINEQ*(T2-T1)+COSDEC*COSSEQ*  HRAD 760
& (SIN(T2+DELONG)-SIN(T1+DELONG))  HRAD 770
RATIO=SRAD/PRAD          HRAD 780
50 HNRAD(IH)=HNRAD(IH)+.944*HRAD(IH)*RATIO*SECINC  HRAD 790
TH1=TH2          HRAD 800
60 TH2=AMIN1(TH2+1.,TS2)          HRAD 810
IF(NUMSR.EQ.1) GO TO 70          HRAD 820
NUMSR=1          HRAD 830
TS1=TS3          HRAD 840
TS2=TS4          HRAD 850
GO TO 40          HRAD 860
70 RETURN          HRAD 870
END              HRAD 880

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C   SUBROUTINE INDEX (L,Y,N)
      INDEX ELEMENTS OF Y IN INCREASING ORDER
      DIMENSION L(1),Y(1)
      M=N          INDE 10
10   M=M/2          INDE 20
      IF(M.EQ.0) RETURN          INDE 30
      K=N-M          INDE 40
      J=1          INDE 50
20   I=J          INDE 60
30   IM=I+M          INDE 70
      IF(Y(L(I)).LE.Y(L(IM))) GO TO 40          INDE 80
      LL=L(I)          INDE 90
      L(I)=L(IM)          INDE 100
      L(IM)=LL          INDE 110
      I=I-M          INDE 120
      IF(I.GE.1) GO TO 30          INDE 130
40   J=J+1          INDE 140
      IF(J.GT.K) GO TO 10          INDE 150
      GO TO 20          INDE 160
      END              INDE 170
                                INDE 180
                                INDE 190
                                INDE 200

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## APPENDIX B (continued)

|  |          |
|--|----------|
| SUBROUTINE LAND (NSEG,*)   | LAND 10  |
| C  | LAND 20  |
| HOURLY VERSION OF LAND MODIFIED BY J. HOLDEMAN AND                       | LAND 30  |
| R. LUXMOORE TO ACCEPT HOURLY DATA - 3/2/76.                              | LAND 40  |
| C THIS IS SUBROUTINE LAND, CONTAINING AN N-LAYER VERSION OF              | LAND 50  |
| C PROSPR THAT WAS ASSEMBLED BY R J LUXMOORE, BASED ON WORK BY            | LAND 60  |
| C R A GOLDSTEIN AND J B MANKIN. THE LAND VERSION THAT FOLLOWS HERE       | LAND 70  |
| C WAS ASSEMBLED ON 12 17 75 BY D. D. HUFF, BASED UPON THE HYDROLOGICLAND | LAND 80  |
| C TRANSPORT MODEL AND AN EARLIER VERSION OF THE STANFORD                 | LAND 90  |
| C WATERSHED MODEL (VERSION V) BY CRAWFORD AND LINSLEY. THIS VERSION      | LAND 100 |
| C MODIFIED TO INCLUDE IRRIGATION BY D.M. HETRICK AND J.T. HOLDEMAN.      | LAND 110 |
| C  | LAND 120 |
| IMPLICIT INTEGER (T)   | LAND 130 |
| COMMON/TLYR/NTL  | LAND 140 |
| COMMON/SSF/SSG(5)  | LAND 150 |
| COMMON/SSRF/PORE,SBD(5),KSAT(5),SA(5),KSGW,CUT,CUTL,WUP                  | LAND 160 |
| DOUBLE PRECISION PORE,SBD,KSAT,SA,KSGW,CUT,CUTL,WUP,AAMAX,WT,WT1,        | LAND 170 |
| 1 WT2  | LAND 180 |
| COMMON/OPT5/CHMOPT,CEROPT,DRYOPT   | LAND 190 |
| LOGICAL CHMOPT,CEROPT,DRYOPT,CLDRY                                       | LAND 200 |
| COMMON /HOLNAM/ IBATCH,LENDRU,LPRECI,LDISTR,LANDS, LCHAN, NEMPTY, LAND   | LAND 210 |
| > EMPTY, IHOLNO,OPEN,HINPUT,HOUTPT,DDOL, RAING, UPRECI,READH,READM, LAND | LAND 220 |
| > UPDATE,HDEPOS,PREC1,READS, IHOLBL, SDOL,HOLBL4,HOLBL3,NSDOL,           | LAND 230 |
| > WEATHE,STANFO,ERNATE, HOLZRO, HOLMB2,HOLMB1,HOL999,HOL998,IHRLY,       | LAND 240 |
| > HOLC,H3BZRO,HMBBB, H4000,HMBBB,HBBBO,HZZZM,HZMB,HB998, IDAILY,         | LAND 250 |
| > STORAG, RECORD,SINITL,SGETH,HDAM,HOLBL,DIVIN,DIOUT                     | LAND 260 |
| DOUBLE PRECISION ALEAF,PAIR,CPO,XL,THETA,DL,AT, ARAT,FC, GM,GV,RB, LAND  | LAND 270 |
| > RX,HT,SIGMA ,TSTEP,CIFLAS,P4,RRX,CIF, RTIM,STCLD,RNLW,VAPMB ,          | LAND 280 |
| > FILT, TMP,SOLAR,VAPOR,ET,DDRRAIN, RNXS,SW,ETGW,TTE ,TIMST,SWT,VP,      | LAND 290 |
| > F,S,FOLTYP, SEV,DNFAC, WP1,WP2,ROFF,TDRN,PSEUDO,ETOT,PTOT,U,           | LAND 300 |
| > RASOL,QFILT,QET, QDRAIN,QRNXS,HDRAIN,HRNXS,HET,DELINF,PRES ,           | LAND 310 |
| > AREA1,AREA2, SSG,TST,PDRN,FL01, FL02,FL03,PA, RF1MON,RF2MON,           | LAND 320 |
| > SDRAG,WDRAG,REDUC,SSGCM(5),SBDCM(5),QFILTW                             | LAND 330 |
| COMMON/ DRAG /SDRAG,WDRAG,REDUC  | LAND 340 |
| COMMON/AR/AREA1,AREA2,PA   | LAND 350 |
| COMMON/HUMID/FOLTYP,PAIR,CPO,RB,RX,SIGMA,XL,GM,GV,HT,ALEAF               | LAND 360 |
| COMMON/GEOMET/DL(8),AT(2),ARAT(2),FC(8),THETA(8),SWT(8)                  | LAND 370 |
| COMMON/PETRUS/TSTEP,TIMST,CIFLAS,CIF(50),RTIM(50),NRASTS                 | LAND 380 |
| COMMON/PORES/VP(8),F,S(8),SEV,ETGW,DNFAC,WP1,WP2,NSL,NBL, NS             | LAND 390 |
| COMMON/TOTMON/ROFF,TDRN,PSEUDO,ETOT,PTOT,PRES,RF1MON, RF2MON             | LAND 400 |
| COMMON/TOTS/TOTALS(2,3)  | LAND 410 |
| INTEGER#2 RS30M,SU30M,RAC30M, TOTALS,PRC,DEPOS                           | LAND 420 |
| REAL LAPSE,LAPS,TMPX,MSRVAP,TOTCMC,TBALWB, LZSOUT,MONCEM(13,25),         | LAND 430 |
| > MELT,NEMELT,LIQW,LIQW1   | LAND 440 |
| DIMENSION CMC(12),BALWB(12),ID(12)                                       | LAND 450 |
| DIMENSION DCS(13),SUMCM(16),INCH(25),CM(25)                              | LAND 460 |
| INTEGER CMYR,CMMO  | LAND 470 |
| COMMON/CM/CMMO,CMYR  | LAND 480 |
| COMMON/AWYPLC/NU1(10),NU2(10),NU3(10),TITL(10,6),NPLTS, NAWPLT           | LAND 490 |
| INTEGER RR,RS, SEG,STANFD, YRTE, DCS, FLAG, YR1, YR2, YEAR, HOUR         | LAND 500 |
| > Y, DAY   | LAND 510 |
| REAL T, MONSUM,TOTAL,IMPV,LZSMO, IDNS, MPACK,K1, K24L,LG,NN,LZS,         | LAND 520 |
| > LZSINV,LANPAR, LZ,INFQ,LOUT, LQO,INTF,TOTELH, LOS,INVTMP               | LAND 530 |
| INTEGER DSTYR, DSDSA, DSENDY, DSNAME, ENDYR, STRTYR, DENDYR,             | LAND 540 |
| > DSSTYR, RENDYR, RODSNA, STAN, ROSTYR, DRUM, PDRUM, SDRUM, RDRUM,       | LAND 550 |
| > SCRACH, SURF, PREC, NEMPTY   | LAND 560 |
| COMMON/UNITS/ DRUM, IDRUM, PDRUM, SDRUM, RDRUM, SCRACH                   | LAND 570 |
| COMMON/C/MONTHS(12)  | LAND 580 |
| COMMON/E/ PREC, DEPS, SURF, RSRF, INV, MAXWYR, TAPESZ, DATE(4)           | LAND 590 |
| COMMON/S/STAN(200), WATSHD(7)  | LAND 600 |
| COMMON/INVGA/STANF, WB,NAME(6),ELEV,LAT(3),LONG(3),GTYPE(2) ,            | LAND 610 |

## APPENDIX B (continued)

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> INTRVL, ELEM(5), INITP,DSNAME,STRTYR,ENDYR, INITS, RODSNA,ROSTYR,LAND 620
> RENDYR, INITD,DDSNAM,DSTYR,DENDYR, INITR, DSDSNA,DSSTYR,DSENDY, LAND 630
> FRADCN,FCNMLT,FSCF,FELDIF,FIDNS, FFCI,FDGM,FWC,FMPACK, FK1,FA, LAND 640
> FL, FSS, FNN, FK24L, FEPXM, LAND 650
C   THE FOLLOWING 13 PARAMETERS TEMPORARILY REMOVED 12 19 75 LAND 660
C   + BARES, ANOTS, KDS, LFTOVS, OCRITS, ONCRTS, AZEROS, LAND 670
C   + SDPMs, SEDMPS, SONES, STWOS, STRES, SFORS, LAND 680
>SGWINV,LZSINV,LIQW,DEPTH,NEMELT,PACK,KEYTIM, DUM1,DUM2, UNUSED(24)LAND 690
DIMENSION SEGMENT(49), SNOPAR(9), LANPAR(7), SOILM(2), SNOPAK(4), LAND 700
> INVENT(88)
EQUIVALENCE (SEGMENT(1),SNOPAR(1),FRADCN), (LANPAR(1),FK1), LAND 720
> (SOILM(1),SGWINV), (SNOPAK(1),LIQW), (INVENT(1),STANF) LAND 730
COMMON/FLAGS/KTEMP,KDEW,KRAD,KWIND,KSNOW,KLAND,KSOILM,KPE LAND 740
COMMON /SOISNO/ SG,LZ,WCON,SDE,COL,PAC LAND 750
COMMON/MOSUMS/ IMPV(13),SURFCE(13),SFL1MO(13),SFL2MO(13), LAND 760
> BASTRM(13),TOTAL(13), RECHGE(13),SLTOMO(13),RNFM(13), LAND 770
> SIENMO(13),SPRSMO(13),SOILMO(13),TEHLMO(13),SVAPMO(13), LAND 780
> POTENT(13),SPETMO(13),STSNSMO(13),SCEPMO(13),RESMO(13), UZSMO(13),LAND 790
> LZSMO(13),STD1MO(13),STD2MO(13).SGWMO(13), STBTM0(13) LAND 800
COMMON/SHIFT1/ RADCON,CONMLT,SCF,ELDIF, IDNS,FCI,DGM,WC, MPACK, K1, LAND 810
> A, LG, SS, NN, K24L, EPXM,SUNCON,CLD,CLDFAC LAND 820
C   CONTAMINANT TRANSPORT IS REMOVED TEMPORARILY. 12 19 75-DDH. LAND 830
C   COMMON/SHIFT2/
C   + BARE, ANOT, KD, LFTOVR, OCRIT, ONCRIT, AZERO, SDPM, SEDMP, LAND 850
C   + SONE, STWO, STRE, SFOR LAND 860
COMMON/SHIFT3/ SGW, LZS, WTRT, DEPTH, COLD, PACKT LAND 870
DIMENSION SLTEMP(16), INV TMP(2), INDATA(8), SOIL(2), SNOW(4), LAND 880
> STRAYS(25), MONSUM(13,25), MONVEC(325), SUM(20) LAND 890
EQUIVALENCE (SLTEMP(1),RADCON), (INV TMP(1),SGW), (INDATA(1),KTEMP) LAND 900
> ,(SOIL(1),SG),(SNOW(1),WCON), (MONSUM(1),MONVEC(1),IMPV(1)), LAND 910
> (STRAYS(1),SIMP) LAND 920
COMMON/MISC/ SIMP,SSUR,SAR1,SAR2,SBAS,STOT,SRCH,SLTO,SRA, SIEN, LAND 930
> SPRS,SOILEV, TOTELH,SNEVAP,SNET,SPET,STSNO,SCEP,RES, STDEP,STUS, LAND 940
> STDS1,STDS2,STGW,STBT LAND 950
COMMON/LOCALS/RU,SCI,F1,F1A,GWF,LOS,EP, RECE,ROS,HRLYRN, EPHRLI, LAND 960
> AETR LAND 970
COMMON/SURFXP/RZ,PR,ORAIN,FF,FIXM,RGX,SHRD,A3,AUZS,ASDS, AINF LAND 980
COMMON/DAILY/DEW(12,31), RAD(12,31), EVAP(12,31), TEM (2,12,31), LAND 990
> WINDS(12,31),IFILL(144) LAND 1000
REAL TEM LAND 1010
COMMON /HRLYS/ IYR,IMO,LOKN,IWRT,IKMPLT,IREC,JSTART, NUMDYS, LAND 1020
> HDW(24,31),HRAD(24,31),HWND(24,31),HTEM(24,31),IRIG,PKIRIG(87) LAND 1030
COMMON/T/TWORD(3), RUNSCL, AERSCL LAND 1040
COMMON/GET/STCLD,MONTHP(12),EPXMIN, EPXMAX, RNON, SUNHR(24), LAND 1050
> DUST(12),Y,M,T(744),JJ LAND 1060
COMMON/NMON/NOW,KEY,SEG,HRNI,TARGET,NXTF LAND 1070
COMMON/XPRE/DEP,SEP,INDRTS LAND 1080
COMMON/SNO/SSCEP,PCKRN,SMELT,MSRVAP,SUMSNO,SDEN,ALBEDO LAND 1090
COMMON/STOSNO/NDASTO,ISTDAY(31),STOPAC(31),STODEP(31),STOSDE(31), LAND 1100
> STOALB(31),STONEM(31),STOLIQ(31),STOSRA(31),STOMSR(31), LAND 1110
> STORAD(31),STOCON(31) LAND 1120
COMMON/NSEG/ SRC,DEC,IDX,SSG1,RES1,SGW1,LZS1,ASPR,CKDH, SFILT, LAND 1130
> LIQW1,PACK1,SSG2,SCEP1,SNOBAL,STRANS,SDDRAN,SINTFA LAND 1140
COMMON/PEV/CNPE,DSEQL,DSOLOS LAND 1150
COMMON/IMPAR/WT,WT1,WT2,ISWIWT LAND 1160
EQUIVALENCE (TWORD(1),TSL), (TWORD(2),TEL), (TWORD(3),TKL) LAND 1170
INTEGER DUMTOT(3) LAND 1180
EQUIVALENCE (TOTALS(1,1),DUMTOT(1)) LAND 1190
REAL#8 SET,QSET,WETDEP(5), LAB(2,25),THOUT(8),SGOUT(5) LAND 1200
DIMENSION HNRAD(24),LAPSE(24),RADIST(24),HIRIG(24) LAND 1210
C                                     LAND 1220

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## APPENDIX B (continued)

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DATA LAPSE /0.6,5*0.0,1.0,2.0,3.0,11*4.0,3.2,2.6,2.0,1.2/ LAND1230
DATA RADIST/6*0.0,0.019,0.041,0.067,0.088,0.102,3*0.11, 0.105, LAND1240
> 0.095,0.081,0.055,0.017,5*0.0/ LAND1250
DATA INCH/25*4H IN./,CM/25*4H CM./,C254/2.54/ LAND1260
DATA LAB/ 'IMPERV R','UNOFF ','SURFACE ','RUNOFF ', 'SOURCE A',LAND1270
> 'REA1 RO ','SOURCE A','REA2 RO ','BASE FLO', 'W      ', LAND1280
> 'TOTAL ST','REAMFLOW','UNMSRD S','EEPAGE ', 'TOTAL OU', LAND1290
> 'TFLOW ', 'TOTAL PR','ECIP ','INTRCEP ', 'EVAP   ', LAND1300
> 'PROSPR T','RANSP ','SOIL EVA','POR    ', 'G.W.TRAN', LAND1310
> 'SP     ','SNOW EVA','POR    ','TOTAL ET', '      ', LAND1320
> 'POTENTIA','L ET    ','SNOWPACK',' TOTAL ', 'INTERCEP', LAND1330
> 'TED STOR','DETENTIO','N STOR ','DEPRESSI', 'ON STOR ', LAND1340
> 'UPPER SO','ILS     ','DEEP SOI','L 1     ','DEEP SOI', LAND1350
> 'L 2     ','GROUNDWA','TER     ','TOTAL CO', 'NTENT   '/ LAND1360
DATA CLDRY/.FALSE./ LAND1370
C LAND1380
C LAND1390
RUSCAL = RUNSCL LAND1400
SCSCAL = AERSCL LAND1410
WRITE(6,10000) LAND1420
TMP = 50.0 LAND1430
BAL = 0.0 LAND1440
FCI = 0.0 LAND1450
DCS(10)=0 LAND1460
DCS(13)=1 LAND1470
RES = 0.0 LAND1480
SRGX = 0.0 LAND1490
SCEP = 0.0 LAND1500
AUZS = 0 LAND1510
ASDS = 0 LAND1520
ALZS = 0 LAND1530
DSOLOS=0. LAND1540
INDRTS=0 LAND1550
RIRRG=0. LAND1560
CALL TIMEWD LAND1570
TS = TSL LAND1580
10 CALL PERIOD (TS, TE) LAND1590
IF (TE.NE.TEL) TE = TEL LAND1600
C LAND1610
C START NEW SEGMENT FOR THE GIVEN WATER YEAR *****
C LAND1620
C LAND1630
DO 500 NG = 1,NSEG LAND1640
TSTEP=15. LAND1650
CIFLAS=0. LAND1660
TIMST=0. LAND1670
DDRAIN=0. LAND1680
C INITIALIZE MONTHLY WATER TERMS FOR PROSPR-BELCH LAND1690
CLDRY=.FALSE. LAND1700
ROFF=0. LAND1710
TDRN=0. LAND1720
RF1MON=0.0D0 LAND1730
RF2MON=0.0D0 LAND1740
PSEUDO=0. LAND1750
ETOT=0. LAND1760
PTOT=0. LAND1770
FILT=0. LAND1780
RNXS=0. LAND1790
SRCH=0. LAND1800
SNET=0. LAND1810
SOILET=0.0 LAND1820
SPET=0. LAND1830

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## APPENDIX B (continued)

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ELH=0.          LAND1840
TOTELH = 0.0    LAND1850
P4=0.          LAND1860
HRNI=0.          LAND1870
SDEN=.6          LAND1880
ALBEDO=.8        LAND1890
NEMELT=0        LAND1900
PACK=0.0          LAND1910
NDASTO=0        LAND1920
READ 10100,IDOL,SEG,STANFD,YR1,YR2    LAND1930
C INPUT SEG. NO. AND CORRESPONDING STANFORD NO. USE STANFORD    LAND1940
C NO. TO FILE. SEVERAL SEGMENT NO. CAN GO INTO ONE STANFORD    LAND1950
C NO. I.E. SAME SEGMENT NO. CAN NOT APPEAR MORE THAN ONCE.    LAND1960
C IF (IDOL.EQ.NSDOL) GO TO 500    LAND1970
C   IF (YR(TE).EQ.YR2) GO TO 11    LAND1980
CALL DATIM(TE,YRTE,MODUM,DADUM,HRDUM,MINDUM)    LAND1990
IF (YRTE.EQ.YR2) GO TO 20    LAND2000
PRINT 10200,SEG    LAND2010
STOP 3001    LAND2020
20 TL = TS    LAND2030
DO 30 N = 1,NSEG    LAND2040
IF (STANFD.EQ.STAN(N)) GO TO 40    LAND2050
30 CONTINUE    LAND2060
PRINT 10300,STANFD    LAND2070
STOP 3002    LAND2080
40 CALL TSEARC ( DRUM,INV,STANFD,0,RR,86)    LAND2090
CALL IN ( DRUM,RR,INVENT,88)    LAND2100
IF (NAME(1).NE.NEMPTY) GO TO 50    LAND2110
PRINT 10400,SEG    LAND2120
STOP 3003    LAND2130
50 CALL CLEAR (INDATA, 8, 0)    LAND2140
CALL CLEAR (MONVEC, 325, 0)    LAND2150
IF (KEYTIM.EQ.TS) GO TO 60    LAND2160
CALL ONMARK(NSEG,DCS,TE,TS,YR1,YR2)    LAND2170
GO TO 70    LAND2180
60 CALL GETSET(NSEG,DCS,TE,TS,YR1,YR2)    LAND2190
70 CALL ANUSEG(DCS,SINTC,BAL,IDX15,IDX30,SINT)
PA=1.0    LAND2200
A=0.0    LAND2210
WT=AREA1    LAND2220
WT1=WT    LAND2230
WT2=WT    LAND2240
MONSUM(13,17)=LIQW+PACK    LAND2250
MONSUM(13,18)=SCEP    LAND2260
MONSUM(13,19)=RES    LAND2270
MONSUM(13,20)=0.0    LAND2280
MONSUM(13,21)=LZS*PA    LAND2290
MONSUM(13,22)=SSG(1)*PA    LAND2300
SUMS=0.    LAND2310
IF (NTL.LT.2) GO TO 90    LAND2320
DO 80 JC=2,NTL    LAND2330
80 SUMS=SUMS+SSG(JC)*PA    LAND2340
90 MONSUM(13,23)=SUMS    LAND2350
MONSUM(13,24)=SGW    LAND2360
MONSUM(13,25)=0.    LAND2370
DO 100 K=17,24    LAND2380
100 MONSUM(13,25)=MONSUM(13,25)+MONSUM(13,K)    LAND2390
C START OF MONTH LOOP    LAND2400
C                                     LAND2410
110 CALL ANUMON(TL,TE,HOUR,YEAR,MONTH,MIN,DAY,ID)    LAND2420
C                                     LAND2430
C                                     LAND2440

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## APPENDIX B (continued)

```

AAMAX=0.0          LAND2450
IF (NOW.GE.TARGET) GO TO 360   LAND2460
IDX=(DAY-1)*24+1   LAND2470
IDX30=IDX+IDX-1   LAND2480
IDX15=IDX30+IDX30-1  LAND2490
DLYDST=DUST(MONTH)/NUMDYS  LAND2500
JLAST=JSTART+NUMDYS  LAND2510
FLAG=0             LAND2520
IP=1               LAND2530
C                 LAND2540
C       START OF DAY LOOP  LAND2550
C
120 CALL ANUDAY(YEAR,MONTH,DAY,HNRAD,IP,IRT,HIRIG)  LAND2570
EP=EVAP(MONTH,DAY)  LAND2580
C                 LAND2590
C       START OF HOUR LOOP  LAND2600
C
130 HET=0.          LAND2610
SET=0.             LAND2620
HDRAIN=0.          LAND2630
HRNXS=0.           LAND2640
HRLYRN = .01*K1*PRC(DAY,HOUR+1)  LAND2650
PR = 0.25*HRLYRN  LAND2660
HRNI=HRNI+100.*HRLYRN  LAND2670
SRA=SRA + HRLYRN  LAND2680
DO 140 K=1,4      LAND2690
140 WETDEP(K)=0.01*DEPOS(DAY,HOUR+1,K)  LAND2700
IF (HRNI.GT.0.) GO TO 150  LAND2710
DEP=.25*DLYDST  LAND2720
GO TO 170         LAND2730
150 HRNI = 0.0     LAND2740
160 DEP = 0.0025*DEPOS(DAY,HOUR+1,1)  LAND2750
C       HOURLY WINDSPEED IN CM/SEC CORRECTED FOR CANOPY DRAG  LAND2760
170 REDU=REDUC    LAND2770
U=AAMAX1(50.,HWND(HOUR+1,DAY)*44.704*REDU)  LAND2780
HIR=HIRIG(HOUR+1)  LAND2790
IF(IRT.EQ.1) PR=PR+HIR*.25  LAND2800
HTMP=HTEM(HOUR+1,DAY)  LAND2810
HT=607.25-.311*TMP  LAND2820
TTE=(HTMP-32.)*0.5555556+273.16  LAND2830
VAPOR=217060.*EXP(-7482.6/(AMIN1(HTMP,HDEW(HOUR+1,DAY))+ 398.36))  LAND2840
VAPMB=1000.*VAPOR  LAND2850
TMP=HTMP          LAND2860
SOLHR=HNRAD(HOUR+1)  LAND2870
RASOL = SOLHR    LAND2880
IF (RN0N.LT.1.) GO TO 190  LAND2890
IF (RASOL.LE.0.) GO TO 180  LAND2900
C       CALCULATE LONG WAVE BALANCE FOR VEGETATION  LAND2910
RNlw = RNLONG(STCLD,RASOL,VAPMB,TTE)  LAND2920
RASOL=RASOL-RNlw  LAND2930
180 IF (RASOL.LT.0.0) RASOL=0.0  LAND2940
SOLHR=RASOL    LAND2950
IF (DAY.EQ.2) PRINT 10500,STCLD,RASOL,VAPMB,TMP,RNlw  LAND2960
190 IF (FOLTY.PT.0) GO TO 200  LAND2970
C       FOLTY.PT.0 INDICATES NEEDLE TYPE CANOPY, NOT LEAVES  LAND2980
RB=1.3*DSQRT(XL/U)  LAND2990
GO TO 210         LAND3000
200 RB=3.3*XL**.3/DSQRT(U)  LAND3010
210 CONTINUE        LAND3020
IF (HOUR.NE.6) GO TO 220  LAND3030
CHAN=(HTEM(17,DAY)-HTEM(7,DAY))/27.  LAND3040
                                         LAND3050

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## APPENDIX B (continued)

```

IF (CHAN.GT.1.0) CHAN=1.0 LAND3060
RADFAC = RADCON*CHAN*RAD(MONTH, DAY) LAND3070
C THE ABOVE COMPUTATATIONS ARE ALWAYS NECESSARY IF SNOW IS POSSIBLE LAND3080
C TEMP IN ZONES LAND3090
220 LAPS=LAPSE(HOUR + 1) LAND3100
IF (HRLYRN.GT.0.05) LAPS = .75*LAPS LAND3110
TMPX = TMP-LAPS*ELDIF LAND3120
TMPXR =0.557*(TMPX -32.0)+273.0 LAND3130
IF (DCS(10).EQ.0) GO TO 230 LAND3140
C SKIP SNOWMELT DURING THE SUMMER MONTHS LAND3150
C
IF((TMPX-0.75*LAPS).LT.32..OR.PACK.GT.0.001)CALL SNOMLT(T,DCS, LAND3160
> TMPX,TMPXR,HRLYRN,FLAG,RADIST,RADFAC, DAY ,HOUR, LAND3170
> MONTH,TMP,LAPS,SOLHR) LAND3180
LAND3190
230 PRES=PR+RES+RIRRG LAND3200
C
C START 15 MINUTE LOOP *****
C
C ROUTE PRECIPITATION THRU INTERCEPTION STORAGE AND LAND3240
C THRUFAUL LAND3250
C
235 CALL XPREC(PR,PACK,IDSID,SINTC,P3,P4) LAND3260
IF(ISWIWT.EQ.0)GO TO 234 LAND3270
C PRINT OUT VARIABLE SOURCE AREA PARAMETER WT, (CALC. IN PROSPR) LAND3280
IF(WT.GT.AREA1)WRITE(6,236)DAY,HOUR,MIN,WT LAND3290
LAND3300
236 FORMAT(1X,'DAY = ',I3,' HOUR = ',I2,' MIN = ',I2,' WT = ',E11.4) LAND3310
234 QFILT=0. LAND3320
IF(RIRRG.GT.0) GO TO 237 LAND3330
IRIRRG=0 LAND3340
GO TO 239 LAND3350
237 IRIRRG=IRIRRG+1 LAND3360
IF(HIR.LE.0.0)GO TO 238 LAND3370
IRIRRG=0 LAND3380
GO TO 240 LAND3390
238 IF(IRIRRG.LT.96)GO TO 240 LAND3400
RIRRG=0. LAND3410
IRIRRG=0 LAND3420
239 IF (IDSID.EQ.1 . AND. IRT.LE.1) GO TO 260 LAND3430
C LOWER ZONE AND GRNDWATER INFILTR LAND3440
IF (INDRTS.LT.96) GO TO 240 LAND3450
TIMST=0. LAND3460
CIFLAS=0. LAND3470
240 INDRTS=0 LAND3480
QHIR=HIR*.25 LAND3490
C ROUTE THRUFAUL PRECIP TO INFILTRATION AND RUNNOFF LAND3500
C
IF(IRT.EQ.2 .OR. IRT.EQ.3.AND.QHIR.GT.0.0) PRES=PRES+.01 LAND3510
CALL RAATS(TSTEP,TIMST,CIFLAS,IRT,QHIR,RIRRG,P4,RRX, LAND3520
> QFILT,CIF,RTIM,NRAATS) LAND3530
C WT IS VARIABLE SOURCE AREA PARAMETER CALC IN PROSPR LAND3540
QFILT=QFILT*WT LAND3550
RU=RU+QFILT
SIMP=SIMP+QFILT
QFILT=QFILT-QFILT
IF (RRX.LE.0) RES=0.0
FILT=FILT+QFILT
IF (RRX.LE.0.) GO TO 260
C 25 LINES REMOVED
C THE VARIABLE RX HAS BEEN CHANGED TO RZ TO AVOID PROSPER CONFLICT
RZ = RRX
C RZ IS THE VOL TO OVLAND FLOW SURF DETENT

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## APPENDIX B (continued)

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DE = (RES+RZ)/2.0          LAND3670
X = DE                      LAND3680
IF (RZ.GT.RES) X = DEC*((RZ-RES)**0.6)    LAND3690
IF (X.GT.DE) DE = X          LAND3700
ROS = 0.0                    LAND3710
IF (RES+RZ.GT.0.0008) ROS=0.25*SRC*((RES+RZ)/2.0)**1.67)* ((1.0+
> 0.6*((RES+RZ)/(2.0*DE))**3.0)**1.67)    LAND3720
IF (ROS.GT.0.75*RZ) ROS = 0.75*RZ          LAND3730
R = PA * ROS                LAND3740
IF (R.LT.0) WRITE(6,10600) TL,R,RES,RZ,ROS,DE,P4
SSUR =SSUR + R              LAND3750
RU = RU + R                LAND3760
LAND3770
LAND3780
C THE FOLLOWING SECTION HAS BEEN REMOVED BECAUSE THE
C TRANSPORT IS INCOMPATIBLE WITH SOURCE AREAS CONCEPT
RES = RZ - ROS              LAND3790
LAND3800
IF (RES.GE.0.0008) GO TO 260
FILT = FILT + RES          LAND3810
LAND3820
RES = 0.0                    LAND3830
LAND3840
260 CONTINUE                 LAND3850
WT=AREA1                     LAND3860
IF (PRES.LE.0.) GO TO 290     LAND3870
LAND3880
C CALL PROSPR(QFILT,TMP,RASOL,VAPOR,U,QET,QDRAIN,QRNXS,SW, SCEP,
> MONTH,DAY,HOUR,YEAR,MIN,QSET,IRT,QHIR,RIRRG)    LAND3890
LAND3900
C IF (CHMOPT) CALL SCEHM(QDRAIN,QFILT,YEAR,MONTH,DAY,HOUR, MIN,
> WETDEP,ROS)               LAND3910
LAND3920
LAND3930
C IF (DRYOPT.AND.CLDRY) CALL DRYADS(PRES,HOUR,MIN,MONTH, YEAR ,DAY) LAND3940
HET=HET+QET                  LAND3950
SET=SET+QSET                  LAND3960
LAND3970
HDRAIN=HDRAIN+QDRAIN         LAND3980
SINTFA=SINTFA+QRNXS*PA       LAND3990
SRGX=SRGX+QRNXS*PA          LAND4000
LZS=0.0                       LAND4010
DO 270 K=1,NSL                LAND4020
270 LZS = LZS + THETA(K)/2.54   LAND4030
TST = 15.0D0                  LAND4040
FL01 = QRNXS                  LAND4050
PDRN = (QDRAIN )*6.0D01/TST   LAND4060
C LAND4070
CALL SUBSRF(TST,PDRN,FL01,FL02,FL03,K24L,SRCH,SGW)
INTF = FL01 + FL02            LAND4080
GWF = FL03                     LAND4090
R = INTF                      LAND4100
SINT = SINT + R                LAND4110
RU = RU + R                   LAND4120
SBAS = SBAS + GWF             LAND4130
RU = RU + GWF                 LAND4140
IRSTOR = IFIX(RU*RUSCAL+0.5) + SU30M(IDX30)    LAND4150
C LAND4160
SU30M(IDX30) = IRSTOR        LAND4170
CALL SU30MR(IDX30, IRSTOR)    LAND4180
IOSTOR = IFIX(SCI*SCSCAL+0.5) + RAC30M(IDX30,1)  LAND4190
C LAND4200
RAC30M (IDX30,1) = IOSTOR    LAND4210
CALL RAC30R(IDX30,1,IOSTOR)   LAND4220
IF (IDX.EQ.1) JFLG = 0         LAND4230
IF (JFLG.GT.0) GO TO 280      LAND4240
IF (IRSTOR.LE.30000.AND.IOSTOR.LE.30000.AND.RU.GE.0.0) GO TO 280
PRINT 10700,IRSTOR,RU,IOSTOR,SCI,IDX30,TL      LAND4250
JFLG = 1                      LAND4260
280 CONTINUE                  LAND4270

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## APPENDIX B (continued)

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        STOT = STOT + RU          LAND4280
        ATOT = ATOT + SCI         LAND4290
290  CONTINUE                      LAND4300
        IF (MIN.NE.45) GO TO 340   LAND4310
C
        CALL PEVSRF(SOLHR,TTE,VAPOR,ETCNPY,RASOL)    LAND4320
        DELINF=0.                           LAND4330
        IF (PRES.GT.0.) GO TO 330           LAND4340
C
        IF(DAY.EQ.1) WRITE(6,612) DELINF,TMP,RASOL,VAPOR,U,HET,    LAND4350
        + HDRAIN,HRNXS,SW,SCEP,MONTH,DAY,HOUR,YEAR,MIN,SET      LAND4360
C
        WT1=AREA1                         LAND4370
        WT2=WT1                           LAND4380
        CALL PROSPR(DELINF,TMP,RASOL,VAPOR,U,HET,HDRAIN,HRNXS,SW, SCEP,    LAND4390
        > MONTH,DAY,HOUR,YEAR,MIN,SET,IRT,QHIR,RIRRG)          LAND4400
C
        IF (CHMOPT) CALL SCEHM(HDRAIN,DELINF,YEAR,MONTH,DAY,HOUR, MIN ,    LAND4410
        > WETDEP,ROS)                         LAND4420
C
        IF (DRYOPT.AND.CLDRY) CALL DRYADS(PRES,HOUR,MIN,MONTH, YEAR ,DAY)  LAND4430
C
        IF(DAY.EQ.1) WRITE(6,612) DELINF,TMP,RASOL,VAPOR,U,HET,    LAND4440
        + HDRAIN,HRNXS,SW,SCEP,MONTH,DAY,HOUR,YEAR,MIN,SET      LAND4450
        LZS=0.0                                LAND4460
        DO 300 K=1,NSL                         LAND4470
300 LZS = LZS + THETA(K)/2.54          LAND4480
        TST = 30.0DO                         LAND4490
        PDRN = (HDRAIN )                     LAND4500
        DO 320 ISS = 1,2                      LAND4510
        FLO1=0.5*HRNXS                      LAND4520
        CALL SUBSRF(TST,PDRN,FLO1,FLO2,FLO3,K24L,SRCH,SGW)      LAND4530
        INTF = FLO1 + FLO2                   LAND4540
        GWF = FLO3                           LAND4550
        R = INTF                            LAND4560
        SINT = SINT + R                     LAND4570
        RU = R                             LAND4580
        SBAS = SBAS + GWF                  LAND4590
        RU = RU + GWF                     LAND4600
        IDSS = IDX30 +ISS - 2              LAND4610
        IRSTOR = IFIX(RU*RUSCAL+0.5)       LAND4620
        CALL SU30MR(IDSS, IRSTOR)          LAND4630
        IOSTOR = IFIX(SCI*SCSCAL+0.5)      LAND4640
        CALL RAC30R(IDSS,1,IOSTOR)          LAND4650
        IF (IDX.EQ.1) JFLG = 0             LAND4660
        IF (JFLG.GT.0) GO TO 310          LAND4670
        IF (IRSTOR.LE.30000.AND.IOSTOR.LE.30000.AND.RU.GE.0.0) GO TO 310  LAND4680
        PRINT 10700,IRSTOR,RU,IOSTOR,SCI,IDX30,TL
        JFLG = 1                           LAND4690
310  CONTINUE                      LAND4700
        STOT = STOT + RU                 LAND4710
320  ATOT = ATOT + SCI               LAND4720
C
        DLAYIN SUBROUTINE WILL START HERE *****
330  CALL DLAYIN(DAY,HOUR,YEAR,MONTH,U,VAPOR,HDRAIN,JLAST,RNXS, FILT,    LAND4730
        > SOLAR,NSEG,ET,SW,HET,ELH,ALZS,HRNXS)          LAND4740
C
        IF (CEROPT) CALL CERES(SOLHR,TMP,HOUR,MONTH,DAY,YEAR)    LAND4750
        CLDRY=.TRUE.                         LAND4760
        SOILET=SOILET+SET                  LAND4770
        SET=0.0DO                            LAND4780
C

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## APPENDIX B (continued)

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340 MIN = MIN + 15          LAND4890
    AAMAX=DMAX1(AAMAX,WT)   LAND4900
    TL = ITWRD(YEAR,MONTH,DAY,HOUR,MIN) LAND4910
    IDX15=IDX15+1           LAND4920
    IDX30=IDX30+MOD(IDX15,2) LAND4930
    IF (MIN.LT.60) GO TO 235 LAND4940
C                                           LAND4950
C       END OF 15 MINUTE LOOP      LAND4960
C                                           LAND4970
C       IDX=IDX+1                LAND4980
C       CALL TIMEIC(TL)          LAND4990
C       CALL DATIM(TL,YEAR,MONTH,DAY,HOUR,MIN) LAND5000
C       IF (HOUR.GT.0) GO TO 130  LAND5010
C                                           LAND5020
C       END OF HOUR LOOP        LAND5030
C                                           LAND5040
C       PRINT DAILY WATER BUDGET AND MONTHLY SUMMARY LAND5050
C       CALL BELCH(JLAST)        LAND5060
C       IF (DAY.GT.1) GO TO 120  LAND5070
C                                           LAND5080
C       END OF DAY LOOP         LAND5090
C                                           LAND5100
C       PREPARE FOR MONTH END   LAND5110
PA=1.0                           LAND5120
A=0.                            LAND5130
CALL TSEARC (SDRUM,SURF,NEMPTY,0,RS,146) LAND5140
CALL PUTOUT(BAL,NOPOS,SINTC,RS,MONTH,MONSUM,SINT,SOILET) LAND5150
WRITE(6,11800)AAMAX               LAND5160
11800 FORMAT(1X,' MAXIMUM A = ',E11.4) LAND5170
C                                           LAND5180
GO TO 110                         LAND5190
C                                           LAND5200
C       END OF MONTH LOOP      *****LAND5210
C                                           LAND5220
C       360 LASTYR = YEAR - 1    LAND5230
A=0.0                           LAND5240
PA=1.                           LAND5250
IF (NAWPLT.NE.0) CALL AWYPLT(MONSUM) LAND5260
WRITE(6,10800) WATSHD,SEG,DSNAME,LASTYR,YEAR LAND5270
CALL CLEAR (SUM, 20,0.0)          LAND5280
DO 370 I = 1, 16                 LAND5290
DO 370 J = 1, 12                 LAND5300
370 SUM(I) = SUM(I) + MONSUM(J,I) LAND5310
C MONCEM IS THE MONSUM ARRAY IN CENTIMETERS INSTEAD OF INCHES. LAND5320
C IF CMYR IS ONE THE VALUES PRINTED OUT WILL BE IN CM. IF ZERO LAND5330
C THE VALUES PRINTED OUT WILL BE IN INCHES. LAND5340
IF (CMYR.EQ.0) GO TO 430          LAND5350
DO 390 J=1,16                     LAND5360
DO 380 I=1,12                     LAND5370
MONCEM(I,J)=MONSUM(I,J)*C254     LAND5380
380 CONTINUE                       LAND5390
SUMCM(J)=SUM(J)*C254              LAND5400
390 CONTINUE                       LAND5410
DO 400 I=1,13                     LAND5420
DO 400 J=17,25                    LAND5430
MONCEM(I,J)=MONSUM(I,J)*C254     LAND5440
400 CONTINUE                       LAND5450
WRITE(6,10900)(MONTHS(ID(J)),J=1,12) LAND5460
WRITE(6,11000) (LAB(1,I),LAB(2,I),(MONCEM(ID(J),I),J=1,12), LAND5470
> SUMCM(I),CM(I),I=1,8)          LAND5480
WRITE(6,11100) (MONTHS(ID(J)),J=1,12) LAND5490

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## APPENDIX B (continued)

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      WRITE(6,11200) (LAB(1,I),LAB(2,I),(MONCEM(ID(J),I),J=1,12),
> SUMCM(I),CM(I),I=9,16) LAND5500
      WRITE(6,11300)(MONTHS(ID(J)),J=1,12) LAND5510
      WRITE(6,11400) (LAB(1,I),LAB(2,I),MONCEM(13,I), (MONCEM(ID(J),I),
> J=1,12),CM(I),I=17,25) LAND5530
      DO 410 J=2,12 LAND5540
      CMC(ID(J))=MONCEM(ID(J),25)-MONCEM(ID(J-1),25) LAND5550
410 CONTINUE LAND5560
      CMC(ID(1))=MONCEM(ID(1),25)-MONCEM(13,25) LAND5570
      DO 420 JJ=1,12 LAND5580
420 BALWB(JJ)=MONCEM(JJ,8)+MONCEM(JJ,15)-MONCEM(JJ,9)+CMC(JJ) LAND5600
      TOTCMC=MONCEM(ID(12),25)-MONCEM(13,25) LAND5610
      TBALWB=SUMCM(8)+SUMCM(15)-SUMCM(9)+TOTCMC LAND5620
      WRITE(6,11500)(MONTHS(ID(J)),J=1,12) LAND5630
      WRITE(6,11600)(MONCEM(ID(J),9),J=1,12),SUMCM(9), CM(1),
> (MONCEM(ID(J),15),J=1,12),SUMCM(15),CM(1), (MONCEM(ID(J), 8),J=1,
> 12),SUMCM(8),CM(1), (CMC(ID(J)),J=1,12),TOTCMC, CM(1),
> (BALWB(ID(J)),J=1,12), TBALWB,CM(1) LAND5640
      GO TO 460 LAND5660
430 WRITE(6,10900)(MONTHS(ID(J)),J=1,12) LAND5670
      WRITE(6,11000) (LAB(1,I),LAB(2,I),(MONSUM(ID(J),I),J=1,12), SUM(I)
> ,INCH(I),I=1,8) LAND5680
      WRITE(6,11100) (MONTHS(ID(J)),J=1,12) LAND5690
      WRITE(6,11200) (LAB(1,I),LAB(2,I),(MONSUM(ID(J),I),J=1,12), SUM(I)
> ,INCH(I),I=9,16) LAND5700
      WRITE(6,11300)(MONTHS(ID(J)),J=1,12) LAND5710
      WRITE(6,11400) (LAB(1,I),LAB(2,I),MONSUM(13,I), (MONSUM(ID(J),I),
> J=1,12),INCH(I),I=17,25) LAND5720
      TOTCMC=0. LAND5730
      DO 440 J=2,12 LAND5740
      CMC(ID(J))=MONSUM(ID(J),25)-MONSUM(ID(J-1),25) LAND5750
440 CONTINUE LAND5760
      CMC(ID(1))=MONSUM(ID(1),25)-MONSUM(13,25) LAND5770
      DO 450 JJ=1,12 LAND5780
450 BALWB(JJ)=MONSUM(JJ,8)+MONSUM(JJ,15)-MONSUM(JJ,9)+CMC(JJ) LAND5790
      TOTCMC=MONSUM(ID(12),25)-MONSUM(13,24) LAND5800
      TBALWB=SUM(8)+SUM(15)-SUM(9)+TOTCMC LAND5810
      WRITE(6,11500)(MONTHS(ID(J)),J=1,12) LAND5820
      WRITE(6,11600)(MONSUM(ID(J),9),J=1,12),SUM(9),INCH(1),
> (MONSUM(ID(J),15),J=1,12),SUM(15),INCH(1) ,(MONSUM(ID(J), 8),J=1,
> 12),SUM(8),INCH(1), (CMC(ID(J)),J=1,12),TOTCMC, INCH(1),
> (BALWB(ID(J)),J=1,12) ,TBALWB,INCH(1) LAND5830
460 DO 461 ITH = 1,NSL LAND5840
461 THOUT(ITH) = THETA(ITH)/DL(ITH) LAND5850
      DO 462 ISG = 1,NTL LAND5860
      SSGCM(ISG) = 2.54 * SSG(ISG) LAND5870
      SBDCM(ISG) = 2.54 * SBD(ISG) LAND5880
462 SGOUT(ISG) = SSG(ISG)/SBD(ISG) LAND5890
      SGWOUT = 2.54*SGW LAND5900
      WRITE(6,11601) LAND5910
      WRITE(6,11602) NSL,(I,THETA(I),DL(I),THOUT(I),I=1,NSL) LAND5920
      WRITE(6,11603) (I,SSGCM(I),SBDCM(I),SGOUT(I),I=1,NTL) LAND5930
      WRITE(6,11604) SGWOUT LAND5940
      WRITE(6,11605) CALL TSEARC (DRUM,INV,STANFD,0,RR,88) LAND5950
      DO 470 I = 1, 5 LAND5960
      IF (ELEM(I).NE.HOLBL4) GO TO 480 LAND5970
470 CONTINUE LAND5980
      GO TO 490 LAND5990
480 IF (YR1.LT.DSSTYR.OR.DSSTYR.EQ.0) DSSTYR = YR1 LAND6000
      IF (YR2.GT.DSENDY) DSENDY = YR2 LAND6010

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## APPENDIX B (continued)

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490 CONTINUE
  IF (YR1.LT.ROSTYR.OR.ROSTYR.EQ.0) ROSTYR = YR1      LAND6110
  IF (YR2.GT.RENDYR.OR.RENDYR.EQ.0) RENDYR = YR2      LAND6120
  CALL OUT (DRUM,RR,INVENT,88)                         LAND6130
  CALL OUT (SDRUM,RS,NEMPTY,1)                         LAND6140
500 CONTINUE
  TS = TE                                              LAND6150
  NOW = TE                                             LAND6160
  TARGET = TEL                                         LAND6170
  IF (NOW.LT.TARGET) GO TO 10                          LAND6180
C
C     END OF SEGMENT LOOP *****
C
C     WRITE(6,11700)
C     RETURN 1
10000 FORMAT ('0*** BEGIN LAND SURFACE SIMULATION ROUTINES ***'//) LAND6190
10100 FORMAT (A1,I2,1X,I3,1X,I2,1X,I2)                LAND6200
10200 FORMAT('OERROR** INPUT OUT OF SEQUENCE FOR SEGMENT ',I3) LAND6210
10300 FORMAT(' ERROR** UNKNOWN STANFORD NUMBER ',I3,      LAND6220
           > ' IN LAND SURFACE SIMULATION')
10400 FORMAT(' ERROR** NO INVENTORY INFO IS ON FILE FOR SEGMENT ',I3) LAND6230
10500 FORMAT(1H , 'STCLD,RASOL,VAPMB,TMP,RNLW=',3X,5G15.7) LAND6240
10600 FORMAT('HEX=',Z9,5X,10E10.4)                   LAND6250
10700 FORMAT ('0',10X,'IRSTOR=',I10, ', RU=',E10.2, ', IOSTOR=', I10, LAND6260
           > ', SCI=',E10.2, ', IDX30=',I5, ', TL=',Z8)    LAND6270
10800 FORMAT (1H1,7A4,' SEGMENT ',I4,' GAGE ',I6,24X, ' WATER YEAR 19', LAND6280
           > I 2,'-',I2//)                                LAND6290
10900 FORMAT(' SEGMENT RUNOFF SUMMARY'/22X,12(A4,4X), 'ANNUAL'//) LAND6300
11000 FORMAT(8(1X,2A8,1X,13F8.2,A8//)               LAND6310
11100 FORMAT(' SEGMENT PRECIP/ET SUMMARY'/22X,12(A4,4X),4X, 'ANNUAL'//) LAND6320
11200 FORMAT(8(1X,2A8,1X,13F8.2,A8//))              LAND6330
11300 FORMAT(' SEGMENT MOISTURE STATUS-BEGINNING OF THE MONTH VALUES'/ LAND6340
           > 22X,13(A4,4X)//)                            LAND6350
11400 FORMAT(9(1X,2A8,1X,13F8.2,A8//))              LAND6360
11500 FORMAT(' SEGMENT WATER BUDGET SUMMARY'/22X,12(A4,4X),4X, 'ANNUAL'/LAND6370
           > /)                                     LAND6380
11600 FORMAT(' PRECIPITATION',5X,13F8.2,A8/' INPUT'/ LAND6390
           > ' EVAPORANSPIRATION',1X,13F8.2, A8/' LOSS'/' OUTFLOW', 11X, LAND6400
           > 13F8.2, A8/' TOTAL'/' CHANGE IN MOISTURE', 13F8.2,A8,/ LAND6410
           > ' CONTENT'/' BALANCE' 11X,13F8.2,A8)        LAND6420
C     THE FOLLOWING FIVE FORMATS OUTPUT NEXT YEAR START VALUES LAND6430
11601 FORMAT(1H1,' THE END OF THE YEAR VALUES TO BE USED TO START NEXT',LAND6440
           > ' YEAR SIMULATIONS FOLLOW:'//)             LAND6450
11602 FORMAT(1X,'FOR THIS SEGMENT THERE ARE ',I3,' SOIL LAYERS SIMULAT',LAND6460
           >'ED BY PROSPER'//1X,'THEY HAVE THE FOLLOWING PROPERTIES://1X, LAND6470
           >'LAYER',3X,'WATER CONTENT (CM)',3X,'LAYER THICKNESS (CM)', LAND6480
           >3X,'THETA VALUE'/(3X,I1,7X,G14.8,7X,G16.8,6X,G12.6//)) LAND6490
11603 FORMAT(/1X,'THE SOIL WATER TRANSMISSION LAYERS HAVE THE ', LAND6500
           >'FOLLOWING PROPERTIES'//1X,'LAYER',3X,'WATER CONTENT (CM)', LAND6510
           >3X,'LAYER THICKNESS (CM)',3X,'THETA VALUE'/(3X,I1,7X,G14.8,7X, LAND6520
           >G16.8,6X,G12.6//))                           LAND6530
11604 FORMAT(/1X,'THE GROUNDWATER STORAGE VALUE IS ',G12.6,' CM.') LAND6540
11605 FORMAT(1H1)                                     LAND6550
11700 FORMAT ('0*** END OF LAND SIMULATION ***')      LAND6560
  END

```

## APPENDIX B (continued)

```

C          SUBROUTINE MONDAT(YEAR,MONTH,IFFIN)
C          PROCESS A MONTH'S DATA
C
C          COMMON /DAILY/ DEW(12,31),RAD(12,31),EVAP(12,31),
C          & TEM(2,12,31), WINDS(12,31),IDEW(36),IRAD(36),ITEM(36),
C          & IWND(36)
C          YEAR, MONTH, LOCATION, WRITE FLAG, COMPLETE FLAG, RECORD
C          NUMBER, JULIAN DATE MINUS ONE OF FIRST DAY OF MONTH,
C          NUMBER OF DAYS IN MONTH
C          COMMON /HRLYS/ IYR,IMO,LOKN,IWRT,IKMPLT,IREC,JSTART,
C          & NUMDYS,HDEW(24,31),HRAD(24,31),HWND(24,31),HTEM(24,31),
C          & IRIG,PKIRIG(87)
C          COMMON /ANGLES/ FILL(6),DGLAT,DLONG
C          INTEGER#2 IDEW,IRAD,ITEM,IWND
C          INTEGER YEAR
C          DIMENSION ZERO(3064)
C          EQUIVALENCE (ZERO(1),HDEW(1))
C          MODEL FOR HOURLY TEMPERATURES INFERED FROM DAILY HIGH
C          AND LOW TEMPERATURES
C          HOURLY TEMPERATURE VARIATION, TEMPF=(T-TMAX)/(TMAX-TMIN)
C          DIMENSION TEMPF(24),LOC(24)
C          DATA TEMPF/.17.,.13.,.09.,.06.,.04.,.02.,.00.,.02.,.08.,.22.,
C          & .40.,.60.,.77.,.90.,.96.,.99.,1.00.,.95.,.88.,.78.,.65.,.50.,.37.,.25/
C          DATA LOC/ 1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,
C          & 19,20,21,22,23,24/
C          DATA IFDEFF/0/,IBLANK/'      ',TWOPI/6.2832/
C          ANNUAL AVG. DAILY TEMPERATURE, SEASONAL VARIATION OF
C          ANNUAL AVERAGE WINDSPEED, AVERAGE CLOUD COVERAGE,
C          TRANSMISSION OF SOLAR RADIATION THROUGH CLOUDS.
C          DATA AAWIND/ 4.5/, CLDF,CLDT/ .1, .32/
C
C          JRETRN=1
C          HAS DIRECT ACCESS FILE BEEN 'DEFINED'?
C          IF(IFDEFF.NE.0) GO TO 10
C          IN NOT THEN 'DEFINE' IT
C          CALL DEFER
C          IFDEFF=1
C          IWRT=0
C          GO TO 20
C          IS NEW MONTH DATA ALREADY AVAILABLE?
10       IF(YEAR.EQ.IYR .AND. MONTH.EQ.IMO) GO TO 60
C          NOT AVAILABLE, SEE IF OLD MONTHS DATA SHOULD BE WRITTEN
C          HAS OLD MONTHS HOURLY DATA BEEN COMPLETED?
C          IF(IKMPLT.EQ.1) GO TO 18
C          NO, COMPLETE ANY POSSIBLE ENTRIES
C          JRETRN=2
C          GO TO 150
C          RETURN FROM POSSIBLE UPDATE
16       JRETRN=1
C          SHOULD OLD DATA BE WRITTEN OUT?
C          IF(IWRT.EQ.0) GO TO 20
C          WRITE OUT OLD MONTH'S DATA ON FILE
C          IWRT=0
C          CALL PROFER
C          GET RECORD NUMBER IF DATA AVAILABLE FOR NEW MONTH,
C          ELSE GET A RECORD NUMBER ASSIGNED TO NEW MONTH
20       CALL GOFER(YEAR,MONTH,NXREC)
C          IF(NXREC.EQ.0) GO TO 60
C          RECORD NOT FOUND SO CREATE A BLANK RECORD
30       IYR=YEAR

```

## APPENDIX B (continued)

```

IMO=MONTH          MOND 620
LOKN=IBLANK        MOND 630
IWRT=0             MOND 640
IKMPLT=0           MOND 650
IREC=NXREC         MOND 660
DO 40 I=1,3064     MOND 670
40 ZERO(I)=0       MOND 680
NUMDYS=LASDAY(IYR,IMO) MOND 690
JSTART=0           MOND 700
IF(IMO.EQ.1) GO TO 60 MOND 710
IMM=IMO-1          MOND 720
DO 50 I=1,IMM      MOND 730
50 JSTART=JSTART+LASDAY(IYR,I) MOND 740
C      END OF BLOCK TO INITIALIZE NEW HOURLY DATA MOND 750
C
C      IS DATA COMPLETE? MOND 760
60 CONTINUE         MOND 780
C 60 IF(IKMPLT.EQ.1) GO TO 900 MOND 790
II=(IMO-1)*3        MOND 800
C      ARE WE TO FORCE COMPLETION OF MONTH'S DATA? MOND 810
IF(IFFIN.EQ.0) GO TO 150 MOND 820
C
C      BEGIN BLOCK TO ENTER NOMINAL OR MODEL DAILY METEOROLOGICAL MOND 830
C      DATA WHEN INPUT DATA IS NOT AVAILABLE MOND 840
C
DO 140 I=1,3        MOND 850
IS=(I-1)*11+1        MOND 860
IL=IS+10            MOND 870
IF(I.EQ.3) IL=NUMDYS MOND 880
III=II+I            MOND 890
IF(IWND(III).NE.0) GO TO 80 MOND 900
C      SET DAILY WINDSPEED TO NOMINAL VALUE MOND 910
DO 70 J=IS,IL        MOND 920
DY=JSTART+J          MOND 930
70 WINDS(IMO,J)=AAWIND*(1.+.2*SIN(.0172*DY-31.)) MOND 940
IWND(III)=1          MOND 950
80 IF(IRAD(III).NE.0) GO TO 100 MOND 960
C      SET DAILY INCIDENT RADIATION TO NOMINAL VALUES MOND 970
CLOUDS=1.0-CLDF+CLDT*CLDF MOND 980
DO 90 J=IS,IL        MOND 990
DY=JSTART+J          MOND 1000
90 RAD(IMO,J)=SOLRAD(DY,DGLAT)*CLOUDS MOND 1010
IRAD(III)=1          MOND 1020
100 IF (ITEM(III).NE.0) GO TO 120 MOND 1030
ALTITUDE=0            MOND 1040
C      SET DAILY HIGH AND LOW TEMPERATURES TO NOMINAL VALUES MOND 1050
DO 110 J=IS,IL        MOND 1060
DY=JSTART+J          MOND 1070
CALL NATEMP(ALTITUDE,DGLAT,DY,TMPMD,TMPDV) MOND 1080
TEM(1,IMO,J)=TMPMD+TMPDV MOND 1090
110 TEM(2,IMO,J)=TMPMD-TMPDV MOND 1100
ITEM(III)=1           MOND 1110
120 IF(IDEW(III).NE.0) GO TO 140 MOND 1120
C      SET DAILY DEWPOINT TO NOMINAL VALUES (DAILY MIN TEMP) MOND 1130
DO 130 J=IS,IL        MOND 1140
130 DEW(IMO,J)=TEM(2,IMO,J) MOND 1150
IDEW(III)=1           MOND 1160
140 CONTINUE          MOND 1170
C      END NOMINAL DAILY DATA BLOCK MOND 1180
C
C      ANY NEW HOURLY DATA TO BE ENTERED? MOND 1190
MOND 1200
MOND 1210
MOND 1220

```

## APPENDIX B (continued)

```

150 DO 160 I=1,3                               MOND1230
    III=III+1                                 MOND1240
    IF(IWND(III).EQ.1) GO TO 170               MOND1250
    IF(IRAD(III).EQ.1) GO TO 170               MOND1260
    IF(ITEM(III).EQ.1) GO TO 170               MOND1270
160 IF(IDEW(III).EQ.1) GO TO 170               MOND1280
    GO TO (900,16), JRETRN                     MOND1290
C
C      BEGIN BLOCK TO ENTER NOMINAL OR MODEL HOURLY   MOND1300
C      METEOROLOGICAL DATA INFERED FROM DAILY DATA WHEN   MOND1310
C      HOURLY INPUT DATA IS NOT AVAILABLE             MOND1320
C
C
170 DO 260 I=1,3                               MOND1330
    III=III+1                                 MOND1340
    IS=(I-1)*11+1                            MOND1350
    IL=IS+10                                MOND1360
    IF(I.EQ.3) IL=NUMDYS                      MOND1370
C      DO WE HAVE NEW TEMPERATURE DATA?          MOND1380
    IF(ITEM(III).NE.1) GO TO 230               MOND1390
    THI=TEM(1,IMO,IS)                         MOND1400
    TLO=TEM(2,IMO,IS)                         MOND1410
    IF(I.GT.1) GO TO 190                       MOND1420
    IYRR=IYR                                  MOND1430
    IIL=III-1                                MOND1440
    IMM=MOD(IMO+10,12)+1                      MOND1450
    IF(IIL.GT.0) GO TO 180                     MOND1460
    IYRR=IYRR-1                              MOND1470
    IMM=12                                    MOND1480
    IIL=36                                    MOND1490
    MOND1500
    IIL=36                                    MOND1510
180 IF(ITEM(IIL).LE.0) GO TO 190               MOND1520
    LAS=LASDAY(IYRR,IMM)                      MOND1530
    THI=TEM(1,IMM,LAS)                        MOND1540
190 TDIF=THI-TLO                             MOND1550
    DO 228 ID=IS,IL                           MOND1560
    DO 210 IH=1,7                           MOND1570
210 HTEM(IH,ID)=TLO+TEMPF(IH)*TDIF           MOND1580
    THI=TEM(1,IMO,ID)                        MOND1590
    TDIF=THI-TLO                           MOND1600
    DO 220 IH=8,17                           MOND1610
220 HTEM(IH,ID)=TLO+TEMPF(IH)*TDIF           MOND1620
    IF(ID.GE.IL) GO TO 222                  MOND1630
    TLO=TEM(2,IMO,ID+1)                      MOND1640
    GO TO 224                                MOND1650
222 IF(IMO.NE.12) TLO=TEM(2,IMO+1,1)        MOND1660
224 TDIF=THI-TLO                           MOND1670
    DO 226 IH=18,24                          MOND1680
226 HTEM(IH,ID)=TLO+TEMPF(IH)*TDIF           MOND1690
228 CONTINUE                                MOND1700
    ITEM(III)=2                               MOND1710
C      HOURLY DEWPONT; DAILY HIGH-LOW TEMPERATURE SHOULD BE   MOND1720
C      ENTERED BEFORE ENTERING HOURLY DEWPONT                 MOND1730
230 IF(IDEW(III).NE.1) GO TO 240               MOND1740
    IF(ITEM(III).NE.2) GO TO 236               MOND1750
C      DISTRIBUTE HOURLY DEWPONT (FOR VAPOR PRESSURE) WHILE PRESERVINGMOND1760
C      AVERAGE, I.E. ENFORCE "CONSERVATION" OF "DEGREE-HOURS"   MOND1770
    DO 235 ID=IS,IL                           MOND1780
    CALL INDEX(LOC,HTEM(1,ID),24)              MOND1790
    DIV=24.                                  MOND1800
C      TOTAL NUMBER OF DEWPONT "DEGREE-HOURS" LEFT IN THIS DAY   MOND1810
    TDH=DEW(IMO,ID)*DIV                      MOND1820
    DO 234 J=1,24                            MOND1830

```

## APPENDIX B (continued)

```

ADP=TDH/DIV                               MOND1840
DIV=DIV-1.                                 MOND1850
IH=LOC(J)                                 MOND1860
IF(HTEM(IH,ID).LT.ADP) GO TO 232        MOND1870
HDEW(IH,ID)=ADP                           MOND1880
GO TO 234                                 MOND1890
232 HDEW(IH,ID)=HTEM(IH,ID)              MOND1900
234 TDH=TDH-HDEW(IH,ID)                 MOND1910
235 CONTINUE                             MOND1920
IDEW(III)=2                                MOND1930
GO TO 240                                 MOND1940
C     DONT HAVE HOURLY TEMPERATURES BUT ASSIGN HOURLY DEWPOINT    MOND1950
C     ANYWAY. MAY LEAD TO SUPERSATURATED CONDITIONS             MOND1960
236 DO 238 ID=IS,IL                      MOND1970
ADEW=DEW(IMO,ID)                         MOND1980
DO 238 IH=1,24                           MOND1990
238 HDEW(IH,ID)=ADEW                     MOND2000
IDEW(III)=2                                MOND2010
C     HOURLY WINDSPEED (CM/SEC)                  MOND2020
240 IF(IWND(III).NE.1) GO TO 250          MOND2030
DO 246 ID=IS,IL                          MOND2040
WNDSPD=WINDS(IMO,ID)                     MOND2050
DO 246 IH=1,24                           MOND2060
246 HWND(IH,ID)=WNDSPD                   MOND2070
IWND(III)=2                                MOND2080
C     HOURLY INCIDENT SOLAR RADIATION           MOND2090
250 IF(IRAD(III).NE.1) GO TO 260          MOND2100
DO 258 ID=IS,IL                          MOND2110
DY=JSTART+ID                            MOND2120
C     HOURLY RADIATION INCIDENT ON HORIZONTAL SURFACE      MOND2130
CALL RADIST(DY,RAD(IMO,ID),DGLAT,DLONG,HRAD(1,ID))  MOND2140
258 CONTINUE                             MOND2150
IRAD(III)=2                                MOND2160
260 CONTINUE                             MOND2170
IWRT=1                                    MOND2180
C     IF(IFSAVE.NE.0) IWRT=1                    MOND2190
C     IF(IFSAVE.EQ.1) IFSAVE=0                  MOND2200
C     IS HOURLY UPDATE COMPLETE?            MOND2210
DO 270 I=1,3                                MOND2220
III=II+I                                  MOND2230
IF(IWND(III).NE.2) GO TO 280              MOND2240
IF(IRAD(III).NE.2) GO TO 280              MOND2250
IF(ITEM(III).NE.2) GO TO 280              MOND2260
270 IF(IDEW(III).NE.2) GO TO 280          MOND2270
IKMPLT=1                                    MOND2280
280 CONTINUE                             MOND2290
C     END OF BLOCK TO ENTER NOMINAL HOURLY METEOROLOGICAL DATA MOND2300
C     GO TO (900,16), JRETRN                  MOND2310
900 RETURN                                 MOND2320
END                                     MOND2330
                                         MOND2340

```

```

SUBROUTINE NATEMP(ALTITUDE,DGLAT,DAYJ,TMPMD,TMPDV)          NATE 10
C
C     MODEL FOR MEAN DAILY TEMPERATURES IN NORTH AMERICA.      NATE 20
C     DAYJ IS JULIAN DATE, DGLAT IS LATITUDE IN DEGREES,       NATE 30
C     ALTITUDE IS ALTITUDE ABOVE MEAN SEA LEVEL IN FEET,      NATE 40
C     ".0035" IS AVERAGE LAPSE RATE IN DEG. F/FOOT.          NATE 50
C     MODEL MAY BE USED BETWEEN 25N AND 55N LATITUDE.         NATE 60
C
C     TMPMD=(12.2-.925*DGLAT)*COS(.0172*(DAYJ-21.))-1.8*DGLAT   NATE 70
& +124.-.0035*ALTITUDE                                     NATE 80
C     TMPDV=20.+.175*SQRT(ALTITUDE)                         NATE 90
TMPDV=20.                                                 NATE 100
RETURN                                              NATE 110
END                                                NATE 120
                                         NATE 130
                                         NATE 140

```

## APPENDIX B (continued)

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SUBROUTINE PEVSRF(SOLHR,TTE,VAPOR,ETCNPY,RASOL)
COMMON/HUMID/FOLTY,PAIR,CPO,RB,RX,SIGMA,XL,GM,GV,HT,ALEAF
COMMON/MISC/ SIMP,SSUR,SAR1,SAR2,SBAS,STOT,SRCH,SLTO,SRA,SIEN,
> SPRS,SOILEV, TOTELH,SNEVAP,SNET,SPET,STSNO,SCEP,RES,STDEP,STUS,
> STDS1,STDS2,STGW,STBT
COMMON/PEV/CNPE,DSEQL,DSOLOS
COMMON/LOCALS/RU,SCI,F1,F1A,GWF,LOS,EP,RECE,ROS,HRLYRN,EPHRLI,
> AETR
REAL*8 TTE,DEDT,ESTAR,VAPOR, RASOL,
> FOLTY,PAIR,CPO,RB,RX,SIGMA,XL,GM,GV,HT,ALEAF
REAL*4 LOS

C
C
C
CALL SATVP(TTE,ESTAR,DEDT)
ESTAR=ESTAR*1.0132
DEDT=DEDT*1.0132
DELTA=.1*DEDT/(0.461*TTE)
IF (VAPOR.GT.ESTAR) VAPOR=ESTAR
WARNING--- THERE IS NO INDICATION IF ESTAR.LT.VAPOR
C
REL=VAPOR*(PAIR-ESTAR)/(ESTAR*(PAIR-VAPOR))
SATMR=0.622*ESTAR/(PAIR-ESTAR)
RMR=REL*SATMR
CP=CPO*(1.+.8*RMR)
RHOAIR=.1*PAIR*(1.+RMR)/(287.D-3*(1.+1.61*RMR)*TTE)
RHODIF=0.1*(ESTAR-VAPOR)/(0.461*TTE)
ECNP1 = SOLHR*DELTA/(2.*CP*RHOAIR)
ECNP2 = 3.6D3*(RHODIF)/RB
IF ((ECNP1+ECNP2).LE.0.) GO TO 20
ETCNPY = (ECNP1+ECNP2)/(1.+HT*DELTA/(2.*CP*RHOAIR))
ETCNPY=ETCNPY/2.54
IF (ETCNPY.GE.0.) GO TO 30
20 ETCNPY=0.
30 EPHRLI=ETCNPY
IF (EPHRLI.LE.0.000001) GO TO 60
IF (SCEP.LE.0.0) GO TO 70
IF (SCEP.LE.EPHRLI) GO TO 40
SCEP = SCEP - EPHRLI
C
CNPE IS EVAPORATION FROM INTERCEPTION STORAGE
CNPE=CNPE+EPHRLI
SNET = SNET + EPHRLI
SOLOS=SOLHR
EPHRLI = 0.0
GO TO 60
40 EPHRLI = EPHRLI - SCEP
CNPE=CNPE+SCEP
SNET = SNET + SCEP
C
CONVERT ET LOSS TO REDUCED SOLAR RADIATION
SOLOS = 0.0
IF (ETCNPY.GT.0.) SOLOS=SOLHR*SCEP/ETCNPY
SCEP = 0.0
RASOL=SOLHR-SOLOS
GO TO 70
60 RASOL=0.0
70 RETURN
END

```

## APPENDIX B (continued)

## APPENDIX B (continued)

```

RUNO=0.
DET=0.
FLLAT=0.
DDRAIN=0.
DPTOT=0.

C      INITIALIZE HOURLY OR QUARTER HOURLY VARIABLES
20 XDIS=96.
   IF (ITER.GT.1) XDIS=24.
   TE=(TEMP-32.)*C59
   TTT=TE
   DO 30 K=1,NSL
   RLAT(K)=0.0D0
30 SWFBL(K)=0.
   EV=VAPOR
   VEL=V
   TRUNO=0.
   TDRAIN=0.
   WT=0.
   SWRF1=0.
   SWRF2=0.
   ETOTAL=0.
   TFLNET=0.
   SEVTOT=0.
   REMWAT=0.0
   WATOVR=0.0
   T=JDATE
   TM=TMW
   IF (T.LT.T4.AND.T.GT.T1) TM=TMS
   IF (.NOT.CEROPT) GO TO 60
   ALEAF=LAI(1)
   IF (ALEAF.GT.ALMIN) GO TO 60
   ALBVEG=ALBW
   SIGMA=SIGW
   PWPMAX=PWPW
   RESMAX=RESW
   POWER=POWW
   TM=TMW
60 RN=24.*HSOLAR
   NRAD=0
   IF ((RN.LT.0.).OR.(SCEP.GT.0.)) NRAD=1
   IF (HSOLAR.LT.0.01) TM=RESMAX
   NT=1+NB
   NP=P*100.*SPIN
   IF (NP.GT.NVP) NT=NT+(NP/NVP)**2
   IF (NDRN.GT.NVPN) NT=NT+(NDRN/NVPN)**2
   NT=MINO(NT,30)
   XNT=NT
   PRE=P/XNT
   DTIM=1./(XDIS*XNT)
   TCL=CUTL*PERHR
   TC=CUT*PERHR
   IF(NT.LT.3) GO TO 68
68 CONTINUE
   DO 260 IDIS=1,NT
   IF PONDING, CONSIDER MACROPORE FLOW EFFECTS -----
   THETA(1)=THETA(1)+PRE+REMWAT
   PRE1=PRE+REMWAT
   REMWAT=0.0
   IF (YESMAC.GT.0.) GO TO 69
   GO TO 67
69 IF (POND.EQ.0.0 .AND. TBET(1).LT.1.D-12) GO TO 67

```

## APPENDIX B (continued)

```

C      WRITE(6,111)POND,TBET(1)                               PROS1230
C 111    FORMAT(' POND OR TBET >0.0: CALLED SWIFT',2D16.7) PROS1240
        THETA(1)=THETA(1)-PRE1                                PROS1250
        CALL SWIFT(1,DTIM)                                     PROS1260
67    CONTINUE                                              PROS1270
        DO 70 K=1,NSL                                         PROS1280
70    CHETA(K)=THETA(K)/DL(K)                                PROS1290
        CALL TABLOK(CHETA,PSM,ZS)                             PROS1300
C      PRINT 24, CHETA,DL,PSM,ZS'1X,8G15.7)                  PROS1310
C 24    FORMAT(1H ,CHETA,DL,PSM,ZS'1X,8G15.7)
        XXX=0.                                                 PROS1320
        DO 80 K=1,NSL                                         PROS1330
        PSI(K)=PSM(K)-DL(K)/2.-XXX                           PROS1340
80    XXX=XXX+DL(K)                                         PROS1350
        DO 90 K=1,NSL                                         PROS1360
90    RS(K)=DL(K)/(2.*ZS(K))                                PROS1370
        ZR1=RTCON1*ZS(1)                                     PROS1380
        ZR2=RTCON2*ZS(2)                                     PROS1390
        RR1 = DL(1)/(AT(1)*ZR1)/2.                            PROS1400
        RR2 = DL(2)/(AT(2)*ZR2)/2.                            PROS1410
        RSR1 = DL(1)*AT(1)/(ZS(1)*ALEAF*ARAT(1))          PROS1420
        RSR2 = DL(2)*AT(2)/(ZS(2)*ALEAF*ARAT(2))          PROS1430
        RSBL(1) = RS(1)                                       PROS1440
        DO 218 K=2,NBL                                         PROS1450
        IF(PSI(K) .GT. PSI(K+1)) GO TO 2175                 PROS1460
        RSBL(K)=RS(K+1) + RS(K)*ZS(K)/ZS(K+1)               PROS1470
        GO TO 218                                             PROS1480
2175  RSBL(K)=RS(K)+RS(K+1)*ZS(K+1)/ZS(K)                PROS1490
218   CONTINUE                                              PROS1500
        R1=RSBL(1)                                           PROS1510
        FAC=9.*(.+ALEAF**2/3.8)/ALEAF**2                   PROS1520
C      IF(AGGIE.EQ.1.) FAC=FAC/9.                          PROS1530
        R2=(RSR2+(RR2+RR1/2.))*FAC                         PROS1540
        R3=RS(1)                                            PROS1550
        R4=(RSTEM+RR1/2.)*FAC                                PROS1560
        R5=RSR1*FAC                                         PROS1570
        CALL SOLVO1(Y)
        PWP=Y                                               PROS1580
        IF (NRAD.EQ.1) GO TO 140                            PROS1590
        IF (PWP.GT.PSI(1)) GO TO 120                         PROS1600
        CALL SUBEV(Y,B)
        ET=B                                                 PROS1610
        GO TO 130                                            PROS1620
120   PWP=PSI(1)-DELPsi                                    PROS1630
        CALL EVAPOR(EV,RN,GND,TTT,ET,ETGW)                  PROS1640
130   IF (ET.GT.0.DO) GO TO 150                            PROS1650
140   ET=0.DO                                              PROS1660
        SEV=0.DO                                             PROS1670
        ETGW=0.DO                                             PROS1680
        ETRF1=0.                                              PROS1690
        ETRF2=0.                                              PROS1700
        GO TO 160                                            PROS1710
150   CONTINUE                                              PROS1720
        ET=ET*DTIM                                           PROS1730
        SEV=(PSI(1)-PWP)/(R3+RLIT)*DTIM                    PROS1740
        ET=ET-SEV                                            PROS1750
        ETRF1=ET*R2/(R2+R5)                                 PROS1760
        ETRF2=ET-ETRF1                                      PROS1770
        SEVTOT=SEVTOT+SEV                                    PROS1780
        ETOTAL=ETOTAL+ET                                     PROS1790
        SWRF1=SWRF1+ETRF1                                   PROS1800
        PROS1810
        PROS1820
        PROS1830

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## APPENDIX B (continued)

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      SWRF2=SWRF2+ETRF2          PROS1840
160  CONTINUE                  PROS1850
      DO 170 K=1,NBL             PROS1860
      SWFLUX(K)=(PSI(K)-PSI(K+1))/RSBL(K)*PERHR   PROS1870
170  DSWFBL(K)=SWFLUX(K)*(DTIM/PERHR)           PROS1880
      FFF=ZS(NSL)*DTIM            PROS1890
      IF(RIRRG.GT.0.0)GO TO 175        PROS1900
      IF(IRT.GE.2.AND.QHIRRG.GT.0.0)GO TO 175    PROS1910
C     AREA1 IS THE LOWER LIMIT OF SOURCE AREA EXTENT (FRACTION)    PROS1920
C     CUTL  IS THE LOWER DRAINAGE THRESHOLD FOR EXPANSION OF SOURCE AREAS    PROS1930
C     CUT   IS THE UPPER DRAINAGE LEVEL FOR MAXIMUM SOURCE AREA EXPANSION    PROS1940
C     W     IS THE FRACTION OF PVIOUS AREAS ACTING AS SOURCE AREAS.    PROS1950
      SRCE1=0.                      PROS1960
      W=AREA1                       PROS1970
      IF (SWFLUX(1).LE.0.0D0) GO TO 190        PROS1980
C     W=AREA11                      PROS1990
      IF (SWFLUX(1).GT.TCL) W=DMIN1(WUP,W+(WUP-W)*
      & (SWFLUX(1)-TCL)/(TC-TCL))           PROS2000
C     SIAV = (PSI(2)+PSI(3))/2.0           PROS2010
C     SIAV IS THE TOTAL POTENTIAL, AND INCLUDES DEPTH AND MATRIC POT.    PROS2020
C     IF(SIAV.GT.-320.) SRCE1 = W*DSWFBL(1)           PROS2030
      DSWFBL(1)=DSWFBL(1)-SRCE1           PROS2040
190  THETA(1)=THETA(1)-DSWFBL(1)-ETRF1-SEV-SRCE1          PROS2050
      THETA(2)=THETA(2)+(DSWFBL(1)-DSWFBL(2))-ETRF2          PROS2060
      WT=WT+W                     PROS2070
      IF (NSL.LT.3) GO TO 220           PROS2080
      DO 210 K=3,NSL                 PROS2090
210  THETA(K)=THETA(K)+(DSWFBL(K-1)-DSWFBL(K))           PROS2100
220  IF ((THETA(1).GE.WP1).AND.(THETA(2).GE.WP2)) GO TO 230    PROS2110
      DIFF=THETA(1)+THETA(2)-WP1-WP2           PROS2120
      THETA(1)=WP1+DIFF*WP1/(WP1+WP2)           PROS2130
      THETA(2)=WP2+DIFF*WP2/(WP1+WP2)           PROS2140
230  CONTINUE                  PROS2150
      DO 232 K=1,NSL                 PROS2160
232  SWFBL(K)=DSWFBL(K)+SWFBL(K)           PROS2170
      TFLNET=TFLNET+DSWFBL(2)           PROS2180
      IF (THETA(1).LE.S(1)) GO TO 240           PROS2190
      TRUNO=TRUNO+THETA(1)-S(1)           PROS2200
      THETA(1)=S(1)                      PROS2210
240  IF(YESMAC.GT.0.)GO TO 245           PROS2220
      DO 250 K=2,NSL                 PROS2230
      IF (THETA(K).LE.S(K)) GO TO 250           PROS2240
      RLAT(K)=RLAT(K)+THETA(K)-S(K)           PROS2250
      THETA(K)=S(K)                      PROS2260
250  CONTINUE                  PROS2270
      GO TO 249                      PROS2280
C     MACROPORE FLOW BETWEEN LAYERS -----MIT          PROS2290
245  DO 247 K=2,NSL                 PROS2300
C     NOTE MACROPORES OF BOTTOM LAYER(NSL) LOOSE WATER    PROS2310
C     BY FLOW TO MESOPORES(NSL) ONLY           PROS2320
      DMEME(K-1)=DMEME(K-1)+DSWFBL(K-1)           PROS2330
      IF(K.LT.NSL)GO TO 246           PROS2340
      IF(REMAIN.GT.0.0) GO TO 248           PROS2350
      IF(TBET(NSL).GT.1.D-12)GO TO 248           PROS2360
      GO TO 247                      PROS2370
246  IF(REMAIN.GT.0.0) GO TO 248           PROS2380
      IF (THETA(K).GT.S(K) .OR. TBET(K-1).GT.1.D-12)GO TO 248    PROS2390
      GO TO 247                      PROS2400
248  CALL SUBONE(K,DTIM)           PROS2410
C     WRITE(6,2480) THETA(K),S(K),TBET(K-1),K           PROS2420
C 2480 FORMAT(' SUBONE CALLED - THETA,S,TBET,K',3D16.7,5X,I5)    PROS2430
C                                         PROS2440

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## APPENDIX B (continued)

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247 CONTINUE                               PROS2450
249 CONTINUE                               PROS2460
C      THE SOURCE AREA RUNOFF IS ADDED TO EXCESS INPUT HERE.    PROS2470
      TRUNO=TRUNO+SRCE1                      PROS2480
      RLAT(1)=RLAT(1)+TRUNO                  PROS2490
      TDRAIN=TDRAIN+FFF                      PROS2500
      THETA(NSL)=THETA(NSL)-FFF              PROS2510
      GO TO 260                                PROS2520
175   DSWFBL(NSL)=0.0                      PROS2530
      TDRAIN=TDRAIN+FFF                      PROS2540
      THETA(NSL)=THETA(NSL)-FFF              PROS2550
      IF(YESMAC.LT.1.) GO TO 181            PROS2560
      DO 182 IK=2,NSL                         PROS2570
182   CALL SUBONE(IK,DTIM)                  PROS2580
      THETA(NSL)=THETA(NSL)+RLAT(NSL)        PROS2590
      RLAT(NSL)=0.                           PROS2600
181   IF(NSL.LT.3)GO TO 185                PROS2610
      DO 180 K=3,NSL                         PROS2620
      NLYR=NSL-(K-3)                        PROS2630
      DSWFBL(NLYR-1)=DMIN1(DSWFBL(NLYR-1),S(NLYR)-THETA(NLYR)+    PROS2640
      & DSWFBL(NLYR))                      PROS2650
      IF(YESMAC.GT.0.0) DMEME(NLYR-1)=DMEME(NLYR-1)+DSWFBL(NLYR-1)  PROS2660
180   THETA(NLYR)=THETA(NLYR)+DSWFBL(NLYR-1)-DSWFBL(NLYR)          PROS2670
185   DSWFBL(1)=DMIN1(DSWFBL(1),S(2)-THETA(2)+DSWFBL(2)+ETRF2)    PROS2680
      IF(YESMAC.GT.0.0) DMEME(1)=DMEME(1)+DSWFBL(1)                  PROS2690
      THETA(2)=THETA(2)+DSWFBL(1)-DSWFBL(2)-ETRF2                  PROS2700
      THETA(1)=THETA(1)-DSWFBL(1)-SEV-ETRF1                         PROS2710
      IF(THETA(1).LE.S(1))GO TO 260                      PROS2720
      REMWAT=THETA(1)-S(1)                            PROS2730
      THETA(1)=S(1)                                 PROS2740
      DO 255 K=1,NSL                         PROS2750
255   SWFBL(K)=DSWFBL(K)+SWFBL(K)           PROS2760
260   CONTINUE                               PROS2770
      WT=WT/XNT                            PROS2780
      WT=(WT+WT1+WT2)/3.0                  PROS2790
      WT2=WT1                                PROS2800
      WT1=WT                                PROS2810
      WATOVR=REMWAT                         PROS2820
      IF(IRT.EQ.3)REMWAT=0.0                 PROS2830
      RIRRG=RIRRG+REMWAT/C254               PROS2840
      IF(I96.NE.52) GO TO 270                PROS2850
C      IF(HOUR.NE.13 .OR. MIN.NE.0) GO TO 270          PROS2860
      RM=RX                                  PROS2870
      POT=PWP                                PROS2880
      SW1M=THETA(1)                          PROS2890
      SW2M=THETA(2)                          PROS2900
      SWNM=THETA(NSL)                         PROS2910
C      COMBINE PLANT AND SOIL ET             PROS2920
270   TET=ETOTAL+SEVTOT                   PROS2930
      IF (PSI(1).GT.PWP) DELPSI=PSI(1)-PWP  PROS2940
C      DETERMINE DAILY TOTALS               PROS2950
      NB=NT/2                                PROS2960
      NDRN=TDRAIN*100.*SPIN                 PROS2970
      DET=DET+TET                            PROS2980
      FLNET=FLNET+TFLNET                   PROS2990
      RUNO=RUNO+TRUNO                       PROS3000
      DO 280 K=2,NSL                         PROS3010
      FLLAT=FLLAT+RLAT(K)                  PROS3020
280   CONTINUE                               PROS3030
      DDRAIN=DDRAIN+TDRAIN                 PROS3040
      DPTOT=DPTOT+P                         PROS3050

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## APPENDIX B (continued)

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C      DPTOT=DPTOT-WATOVR          PROS3060
      DETERMINE MONTHLY TOTALS    PROS3070
      RF1MON=RF1MON+SWRF1         PROS3080
      RF2MON=RF2MON+SWRF2         PROS3090
      ROFF=ROFF+TRUNO            PROS3100
      TDRN=TDRN+TDRAIN           PROS3110
      DO 290 K=2,NSL              PROS3120
      PSEUDO=PSEUDO+RLAT(K)       PROS3130
290  CONTINUE                     PROS3140
      ETOT=ETOT+TET               PROS3150
      PTOT=PTOT+P                 PROS3160
      PTOT=PTOT-WATOVR            PROS3170
      IF(RX.EQ.0.)RX=0.00001       PROS3180
      PCONL=1./RX                 PROS3190
      PPBAR=PWP*9.81D-4           PROS3200
C***SPECIAL PRINT FOR FLORENCE CORN STUDY***   PROS3210
      IF(JDATE.EQ.137.OR.JDATE.EQ.140.OR.JDATE.EQ.153.OR.JDATE.EQ.158   PROS3220
      >.OR.JDATE.EQ.167.OR.JDATE.EQ.175) PRINT 700, JDATE,HOUR,MIN,PPBAR   PROS3230
      >,PCONL,SEVTOT,ETOTAL,SWRF1,SWRF2,TFLNET,TDRAIN                  PROS3240
      700 FORMAT(' DHM-PCST12BD',3I4,8G13.4)                           PROS3250
      IF (MONTH.EQ.LMONTH) GO TO 310                                     PROS3260
      I1=0                                         PROS3270
      I2=0                                         PROS3280
      LMONTH=MONTH                         PROS3290
      NMONT=1                                         PROS3300
      NSMONT=1                                         PROS3310
      NDAY=LASDAY(YEAR,MONTH)                   PROS3320
C----THIS IS WHERE THE CALCULATIONS ARE DONE FOR PROSPER PLOTS FOR 1/3  PROS3330
C OF A MONTH.                                PROS3340
      310 IF (NPRPLT.EQ.0.OR.NMONTH.EQ.0) GO TO 410                  PROS3350
      IF (NT1.NE.0) GO TO 350                                     PROS3360
      IF (I1.NE.0) GO TO 340                                     PROS3370
      DO 320 I=1,NMPLT                                         PROS3380
      IF (MONTH.EQ.MONPLT(I)) GO TO 330                         PROS3390
      I1=I                                         PROS3400
      320 CONTINUE                                         PROS3410
      NMONT=0                                         PROS3420
      GO TO 410                                         PROS3430
      330 I1=I1*3+1                                         PROS3440
      340 IF (PORPLT(I1).EQ.0) PORPLT(I1)=4                  PROS3450
      NDAY=LASDAY(YEAR,MONTH)                   PROS3460
      INC2=PORPLT(I1)                                         PROS3470
      350 GO TO (360,370,380,390), INC2                      PROS3480
C----FIRST THIRD OF THE MONTH                    PROS3490
      360 IDAY=DAY                                         PROS3500
      IF (DAY.LT.10.OR.HOUR.NE.23) GO TO 400                  PROS3510
      IF (MIN.NE.45) GO TO 400                               PROS3520
      NQUES=1                                         PROS3530
      XMIN=1                                         PROS3540
      XMAX=11                                         PROS3550
      I1=I1+1                                         PROS3560
      GO TO 400                                         PROS3570
C----SECOND THIRD OF THE MONTH                  PROS3580
      370 IDAY=DAY-10                                         PROS3590
      IF (DAY.LT.20.OR.HOUR.NE.23) GO TO 400                  PROS3600
      IF (MIN.NE.45) GO TO 400                               PROS3610
      NQUES=1                                         PROS3620
      XMIN=11                                         PROS3630
      XMAX=21                                         PROS3640
      I1=I1+1                                         PROS3650
      GO TO 400                                         PROS3660

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## APPENDIX B (continued)

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C----LAST THIRD OF THE MONTH                                PROS3670
380 IDAY=DAY-20                                         PROS3680
  IF (DAY.LT.NDAY.OR.HOUR.NE.23) GO TO 400               PROS3690
  IF (MIN.NE.45) GO TO 400                               PROS3700
  NQUES=1                                                 PROS3710
  XMIN=21.                                                PROS3720
  XMAX=NDAY                                              PROS3730
  I1=I1+1                                                 PROS3740
  GO TO 400                                              PROS3750
C----TO HERE IF NO PLOTS FOR THIS PORTION OF THE MONTH.   PROS3760
390 IF (((DAY.EQ.10).OR.(DAY.EQ.20).OR.(DAY.EQ.NDAY))    PROS3770
> .AND.HOUR.EQ.23.AND.MIN.EQ.45) I1=I1+1               PROS3780
  GO TO 500                                              PROS3790
400 NT1=1                                                 PROS3800
  CK=FLOAT(HOUR+1)/4.                                    PROS3810
  ID=(IDAY-1)*6                                         PROS3820
  INC1=0                                                 PROS3830
  IF (CK.EQ.1.) INC1=ID+1                               PROS3840
  IF (CK.EQ.2.) INC1=ID+2                               PROS3850
  IF (CK.EQ.3.) INC1=ID+3                               PROS3860
  IF (CK.EQ.4.) INC1=ID+4                               PROS3870
  IF (CK.EQ.5.) INC1=ID+5                               PROS3880
  IF (CK.EQ.6.) INC1=ID+6                               PROS3890
  GO TO 460                                              PROS3900
C----THIS IS WHERE CALCULATIONS ARE DONE FOR SPECIAL PLOTS.  PROS3910
410 IF (NSPLTS.EQ.0.OR.NSMONT.EQ.0) GO TO 500            PROS3920
  IF (NST.NE.0) GO TO 440                               PROS3930
  IF (I2.NE.0) GO TO 440                               PROS3940
  DO 420 I1=NMSPLT                                      PROS3950
    IF (MONTH.EQ.MONSPL(I1)) GO TO 430                  PROS3960
    I2=I                                                 PROS3970
420 CONTINUE                                             PROS3980
  NSMONT=0                                              PROS3990
  GO TO 500                                              PROS4000
430 I2=I2+1                                              PROS4010
440 IF (DAY.LT.NBEG(I2).OR.DAY.GT.NEND(I2)) GO TO 500   PROS4020
  NST=1                                                 PROS4030
  NDIFF=DAY-NBEG(I2)                                    PROS4040
  IF (NDIFF.NE.3.OR.HOUR.NE.23) GO TO 450              PROS4050
  IF (MIN.NE.45) GO TO 450                            PROS4060
  XMIN=NBEG(I2)                                         PROS4070
  NBEG(I2)=NBEG(I2)+4                                 PROS4080
  XMAX=NBEG(I2)                                         PROS4090
  NQUES=1                                               PROS4100
450 INC1=(NDIFF)*24+HOUR+1                            PROS4110
460 DIVP=DIVP+1.                                         PROS4120
  HPA=HPA+P                                           PROS4130
  HPA=HPA-WATOVR                                     PROS4140
  IF (INC1.EQ.0) GO TO 500                            PROS4150
C----FILL THE 'HOLD' ARRAYS FOR PLOTTING.                PROS4160
  DO 470 J=1,NSL                                         PROS4170
    HSW(INC1,J)=THETA(J)/DL(J)                         PROS4180
470 CONTINUE                                             PROS4190
  HTET(INC1)=TET+HTET(INC1)                           PROS4200
  HTDRAN(INC1)=TDRAIN+HTDRAN(INC1)                     PROS4210
  HTFLNT(INC1)=TFLNET+HTFLNT(INC1)                     PROS4220
  HCONL(INC1)=PCONL                                     PROS4230
  HPBAR(INC1)=PPBAR                                     PROS4240
  HP(INC1) = HPA/DIVP                                  PROS4250
  IF (MIN.EQ.45) HPA=0.0                                PROS4260
  IF (HP(INC1).GT.1.E-6) IPLTP=1                      PROS4270

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## APPENDIX B (continued)

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C----CALL PRSPLT IF IT IS THE LAST LOOP THROUGH FOR THE PERIOD      PROS4280
C TO BE PLOTTED.          PROS4290
  IF (NQUES.NE.1) GO TO 500          PROS4300
  CALL PRSPLT(HSW,HTET,HTDRAN,HTFLNT,HCONL,HPBAR,HP,IPLTP,INC1,      PROS4310
> XMIN,XMAX,MONTH)          PROS4320
  IF (.NOT.DRYOPT) NQUES=0          PROS4330
  NT1=0          PROS4340
  NST=0          PROS4350
  HPA=0.          PROS4360
  DIVP=0.          PROS4370
  IPLTP=0          PROS4380
  NRQUES=1          PROS4390
  DO 490 JJ=1,120          PROS4400
  HCONL(JJ)=0.0          PROS4410
  HTET(JJ)=0.0          PROS4420
  HTDRAN(JJ)=0.0          PROS4430
  HTFLNT(JJ)=0.0          PROS4440
  HPBAR(JJ)=0.0          PROS4450
  490 CONTINUE          PROS4460
  500 CONTINUE          PROS4470
C   TRNXS BECOMES INTERFLOW IN LAND          PROS4480
  TRLAT=0.ODO          PROS4490
  DO 510 K=2,NSL          PROS4500
  TRLAT=TRLAT+RLAT(K)          PROS4510
  510 CONTINUE          PROS4520
  TRNXS=TRUNO+TRLAT          PROS4530
C   CONVERT DATA TO INCHES FOR LAND          PROS4540
  TDRAIN=TDRAIN/C254          PROS4550
  TRNXS=TRNXS/C254          PROS4560
  TET=TET/C254          PROS4570
  SEVTOT=SEVTOT/C254          PROS4580
  RETURN          PROS4590
  END          PROS4600

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## APPENDIX B (continued)

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SUBROUTINE RAATS(TSTEP,TIMIN,CIFLAS,IRT,QHIRRG,RIRRG,
> P4,RRX,DFILT,CIF,RTIM,NRAATS)
      INFILTRATION BY TIME COMPRESSION APPROXIMATION
      IMPLICIT REAL*8 (A-H,O-Z)
COMMON/AREAIR/FIRRG
REAL*4 QHIRRG,FIRRG,RIRRG,X,SPFILT
DIMENSION CIF(1),RTIM(1)
DATA IDQ,ITM/'DQ','TM'/
M=3
RCIF=CIFLAS
C      COMPUTE POTENTIAL INFILTRATION FOR TIME STEP TSTEP
TM=TIMIN+TSTEP
Q=YLAG(TM,RTIM,CIF,0,M,NRAATS,IEX)
IF (IEX.NE.0) PRINT 10000, IEX, IDQ
DQ=Q-RCIF
IF (RIRRG.GT.0.0)GO TO 5
IF (IRT.LT.2 .OR.(QHIRRG.EQ.0. .AND. RIRRG.EQ.0.)) GO TO 30
      IRRIGATION BY FLOODING, A FRACTION FIRRG OF THE
C      LAND SURFACE IS FLOODED.
5   X=DMIN1(DQ,P4)
DFILT=X+FIRRG*(DQ-X)
RRX=0.
IF (IRT.EQ.2) GO TO 10
IF (IRT.LE.1.AND.RIRRG.GT.0.0)GO TO 10
      FLOOD IRRIGATION WHERE FLOODING TIME IS SPECIFIED
CIFLAS=Q
RIRRG=0.
GO TO 60
C      FLOOD IRRIGATION WHERE AMOUNT OF WATER IS SPECIFIED.
10  RIRRG=RIRRG+QHIRRG+P4
SPFILT=DFILT
DFILT=AMIN1(SPFILT,RIRRG)
CIFLAS=AMIN1(RIRRG/FIRRG,DQ-X)+RCIF
RIRRG=RIRRG-DFILT
GO TO 50
C      FOLLOWING INCLUDES ANY SPRINKLER IRRIGATION
30  IF (DQ.GE.P4) GO TO 40
C      THRUFAUL EXCEEDS INFILTRATION, GENERATE RUNOFF (RRX).
RRX=P4-DQ
CIFLAS=Q
DFILT=DQ
GO TO 60
C      POTENTIAL INFILTRATION EXCEEDS THRUFAUL, NO RUNOFF.
40  DFILT=P4
RRX=0.
CIFLAS=RCIF+DFILT
50  TM=YLAG(CIFLAS,CIF,RTIM,0,M,NRAATS,IEX)
IF (IEX.NE.0) PRINT 10000, IEX, ITM
60  TIMIN=TM
RETURN
10000 FORMAT(' EXTRAPOLATION IN RAATS/YLAG, IEX = ',I3,' FOR ',A2)
END

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## APPENDIX B (continued)

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C      SUBROUTINE RADIST(DY,DLYRAD,DLAT,DLONG,HRAD)          RADI 10
C      MODEL THE DIURNAL VARIATION OF THE SOLAR             RADI 20
C      RADIATION INCIDENT ON A HORIZONTAL SURFACE.          RADI 30
C      RADI 40
C      RADI 50
C      RADI 60
C      RADI 70
C      RADI 80
C      RADI 90
C      RADI 100
C      RADI 110
C      RADI 120
C      RADI 130
C      RADI 140
C      RADI 150
C      RADI 160
C      RADI 170
C      RADI 180
C      RADI 190
C      RADI 200
C      RADI 210
C      RADI 220
C      RADI 230
C      RADI 240
C      RADI 250
C      RADI 260
C      RADI 270
C      RADI 280
C      RADI 290
C      RADI 300
C      RADI 310
C      RADI 320
C      RADI 330
C      RADI 340
C      RADI 350
C      RADI 360
C      RADI 370
C      RADI 380
C      RADI 390
C      RADI 400
C      RADI 410
C      RADI 420
C      RADI 430
C      RADI 440
C      RADI 450
C      RADI 460
C      RADI 470
C      RADI 480
C
C      DIMENSION HRAD(24)
C      DATA ALFA,HA/-106.,.002/
C
C      DO 10 IH=1,24
C      10 HRAD(IH)=0.
C      EQUATION OF TIME
C      AT=.01720242*DY-1.41430
C      BT=.033446*SIN(.01720242*DY-.059075)
C      SINET=SIN(AT+BT)
C      EQUATI=229.1831*ATAN2(SIN(BT)-.082549*SINET*COS(AT),
C      & COS(BT)-.082549*SINET*SIN(AT))
C      SNOON=12.-(AINT(DLONG/15.+5)-DLONG/15.)+EQUATI/60.
C      SINDEC=.39785*SINET
C      DEC=ARSIN(SINDEC)
C      COSDEC=COS(DEC)
C      RLAT=.01745329*DLAT
C      SINLAT=SIN(RLAT)
C      COSLAT=COS(RLAT)
C      DAYL=ARCCOS(AMAX1(-1.,AMIN1(1.,-SINLAT/COSLAT*SINDEC/COSDEC)))/.261RADI
C      TH1=-DAYL
C      I1=-DAYL+SNOON+1.
C      TH2=I1-SNOON
C      TL=DAYL
C      I2=SNOON+TL+2.
C      SUM=0.
C      DO 20 IH=I1,I2
C      T1=.2617994*TH1
C      T2=.2617994*TH2
C      PRAD=SINDEC*SINLAT*(T2-T1)+COSDEC*COSLAT*(SIN(T2)-SIN(T1))
C      ATMOSPHERIC TRANSMISSION FACTOR
C      TM=(T1+T2)*.5
C      COSI=SINLAT*SINDEC+COSLAT*COSDEC*COS(TM)
C      TRAD=EXP(ALFA*(2.+HA)/(COSI+SQRT(COSI**2+HA*(2.+HA))))
C      HRAD(IH)=PRAD*TRAD
C      SUM=SUM+HRAD(IH)
C      TH1=TH2
C      20 TH2=AMIN1(TH2+1.,TL)
C      RNORM=DLYRAD/SUM
C      DO 30 IH=I1,I2
C      30 HRAD(IH)=HRAD(IH)*RNORM
C      RETURN
C      END

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## APPENDIX B (continued)

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C      SUBROUTINE RDIRIG
      READ IRRIGATION DATA
      COMMON /HRLYS/ IYR,IMO,LOKN,IWRT,IKMPLT,IREC,JSTART,NUMDYS,
> HDEW(24,31),HRAD(24,31),HWND(24,31),HTEM(24,31),
> IRIG,PKIRIG(87)
      COMMON/AREAIR/FIRRG
      DIMENSION AH(11),EM(11)
      INTEGER X,Y,D
      DATA IDOL/'$'/,ER,BL/4H****,4H      /,EM/11*4H      /
C      READ 1030,FIRRG
10     READ 1000,X,Y,M,K,AH
      IF(X.EQ.IDOL) RETURN
      D=AH(1)/10000.
      PRINT 1010,M,D,Y,AH
      IF(Y.NE.IYR .OR. M.NE.IMO) CALL MONDAT(Y,M,0)
      IP=1
20     IF(AH(IP).EQ.0.) GO TO 10
      IN=AH(IP)
      D=IN/10000
      IF(D.LT.1 .OR. D.GT.NUMDYS) GO TO 40
      IN=IN-10000*D
      IH=IN/100
      IF(IH.LT.1 .OR. IH.GT.24) GO TO 40
      IN=IN-100*IH
      IF(IN.EQ.0 .OR. IH+IN.GT.25) GO TO 40
      IL=1
      IF(K.EQ.3) GO TO 25
      IF(IP+IN.GT.11) GO TO 40
      IL=IN+1
25     AH(IP)=10.*AH(IP)+K
      DO 30 I=1,IL
      IRIG=IRIG+1
      PKIRIG(IRIG)=AH(IP)
30     IP=IP+1
      IWRT=1
      IF(IP.LE.10) GO TO 20
      GO TO 10
40     EM(IP)=ER
      PRINT 1020,EM
      EM(IP)=BL
      GO TO 10
1000  FORMAT(A1,6X,2I2,I1,11F6.0)
1010  FORMAT(' IRRIGATION FOR ',I2,'/',I2,'/',I2,' - ',11F8.0)
1020  FORMAT(' *** ERROR ***',12X,11A8)
1030  FORMAT(F6.0)
      END

```

## APPENDIX B (continued)

```

SUBROUTINE READIN                                         READ  10
IMPLICIT REAL*8 (A-H,O-Z)                               READ  20
DIMENSION FILTID(20),ARBOR(20),HYCOND(8,8),SMPPAR(8,8) READ  30
COMMON/THINGS/ALBVEG,CANON,CANOFF,SIMIN,SIMAX,ALMIN,ALMAX,SLOPE
COMMON/PORES/VP(8),F,S(8),SEV,ETGW,DNFAC,WP1,WP2,NSL,NBL,NS
COMMON/HUMID/FOLTYC,PAIR,CPO,RB,RX,SIGMA,XL,GM,GV,HT,ALEAF
COMMON/RESIST/R1,R2,R3,R4,R5,RR1,RRA,RRB,RRC,RRR,TM,RLIT
COMMON/SURF/PWPS,PWPW,PWPWMAX,RESS,RESW,RESMAX,POWS,POWW,POWER ,
> LRMODL                                               READ  80
COMMON/GEOMET/DL(8),AT(2),ARAT(2),FC(8),THETA(8),SWT(8) READ  90
COMMON/TIMES/T1,T2,T3,T4,TMS,TMW,SIGS,SIGW,ALBS,ALBW
COMMON/PLACE/ CASEID(19),LASTDY(12),MOBEG
COMMON/PETRUS/TSTEP,TIMST,CIFLAS,CIF(50),RTIM(50),NRAATS
COMMON/DRAG/SDRAG,WDRAG
COMMON/PHOTO/CAIR,CCHL,P1,A1,B1,A2,B2,C2SEC,P3,F13
COMMON/BIODAT/TL1,TL2,TL3,C6,P12,P13,PSMA,PSMB,PA,PB,PC,PD
COMMON/SULU/RTCON1,RTCON2,RSTEM,AGGIE
COMMON/FORMUL/HYCOND,SMPPAR,LFORM
COMMON/PLTALL/XMIN,XMAX,INC1,ISTRA,NQUES
COMMON/PIECES/TRUNO,ZS(8),PRE1,POND,TBET(8),YESMAC,PSM(8),REMAIN
COMMON/FONG/DAYMAC
DATA KFORM/'FORM'/
REAL*4 CAIR,CCHL,P1,A1,B1,A2,B2,C2SEC, TL1,TL2,TL3,C6,P12,P13,
> PSMA,PSMB,PA,PB,PC,PD,P3,F13
READ(5,10000) NERR,CASEID
C NERR=1 WHEN NEW SEGMENT PROPERTIES ARE READ, 0 OTHERWISE
WRITE(6,10100) NERR, CASEID
IF (NERR.LT.1) GO TO 100
READ(5,10200) DL,THETA,F
WRITE(6,10400) DL,THETA,F
READ(5,10200) PAIR,CPO,XL,V,FOLTYC
WRITE(6,10500) PAIR,CPO,XL,V,FOLTYC
READ(5,10200) AT,ARAT,RTCON1,RTCON2,RSTEM
WRITE(6,10600) AT,ARAT,RTCON1,RTCON2,RSTEM
READ(5,10200) ALMIN,ALMAX,GM,GV
WRITE(6,10700) ALMIN,ALMAX,GM,GV
READ(5,10200) RLIT,WP1,WP2,AGGIE
WRITE(6,10800) RLIT,WP1,WP2,AGGIE
READ(5,10200) T1,T2,T3,T4
PRINT 10900, T1,T2,T3,T4
READ(5,10200) TMS,TMW,SIGS,SIGW,ALBS,ALBW
PRINT 11000, TMS,TMW,SIGS,SIGW,ALBS,ALBW
READ 10300, SDRAG,WDRAG,NSL,NS,YESMAC,DAYMAC
PRINT 11100, SDRAG,WDRAG,NSL,NS,YESMAC,DAYMAC
READ(5,11200) PWPS,PWPW,RESS,RESW,POWS,POWW,LRMODL
PRINT 11300, PWPS,PWPW,RESS,RESW,POWS,POWW,LRMODL
NBL=NSL-1
DO 10 K=1,NSL
THETA(K)=THETA(K)*DL(K)
10 SWT(K)=THETA(K)
CALL ASPECT
READ 11400,LFORM
IF (LFORM.NE.KFORM) GO TO 60
C READ IN PARAMETERS IN ORDER TO USE FORMULAS FOR ZS & PSM INSTEAD
C OF INTERPOLATION
C TO CHANGE FORMULAS USED: CHANGE FORLOK
DO 20 J=1,NS
READ 11500,ST,ST1,ST2,ST3,ST4,ST5,ST6,ST7,ST8,ST9
PRINT 11600,ST,ST1,ST2,ST3,ST4,ST5,ST6,ST7,ST8,ST9
READ 11700,(HYCOND(J,JJ),JJ=1,8)

```

## APPENDIX B (continued)

```

PRINT 11800,(HYCOND(J,JJ),JJ=1,8)          READ 620
READ 11900,(SMPPAR(J,JJ),JJ=1,8)          READ 630
PRINT 12000,(SMPPAR(J,JJ),JJ=1,8)          READ 640
VP(J)=SMPPAR(J,2)                         READ 650
20 CONTINUE                                READ 660
IF (NS.GE.NSL) GO TO 70                  READ 670
NN=NS+1                                    READ 680
DO 40 I=NN,NSL                           READ 690
DO 30 JJ=1,8                             READ 700
HYCOND(I,JJ)=HYCOND(NS,JJ)                READ 710
SMPPAR(I,JJ)=SMPPAR(NS,JJ)               READ 720
30 CONTINUE                                READ 730
40 VP(I)=SMPPAR(NS,2)                    READ 740
DO 50 I=1,NSL                           READ 750
PRINT 11800,(HYCOND(I,JJ),JJ=1,8)          READ 760
PRINT 12000,(SMPPAR(I,JJ),JJ=1,8)          READ 770
50 CONTINUE                                READ 780
GO TO 70                                  READ 790
60 CALL SOIL                               READ 800
70 F=F*DL(NSL)                           READ 810
DO 80 K=1,NSL                           READ 820
80 S(K)=VP(K)*DL(K)                     READ 830
WP1=WP1*DL(1)                           READ 840
WP2=WP2*DL(2)                           READ 850
READ(5,12400) FILTID                   READ 860
READ(5,12100) TSTEP,TIMST,CIFLAS,NRAATS   READ 870
CIFLAS=CIFLAS/2.54                      READ 880
READ(5,12200) (CIF(I),I=1,NRAATS)        READ 890
READ(5,12300) (RTIM(I),I=1,NRAATS)       READ 900
CALL CHKCIF(RTIM,CIF,NRAATS,1)           READ 910
CALL CHKCIF(CIF,RTIM,NRAATS,2)           READ 920
WRITE(6,12500) FILTID                   READ 930
WRITE(6,12600)                          READ 940
WRITE(6,12700) CIF                      READ 950
DO 90 J=1,NRAATS                         READ 960
90 CIF(J)=CIF(J)/2.54                   READ 970
WRITE(6,12800) RTIM                      READ 980
100 CONTINUE                                READ 990
NQUES=0                                     READ1000
IF (YESMAC.EQ.1.0) CALL RSWIFT          READ1010
RETURN                                     READ1020
10000 FORMAT(I1,3X,19A4)                   READ1030
10100 FORMAT(T1,'0',I1,3X,19A4)          READ1040
10200 FORMAT(8G10.3)                      READ1050
10300 FORMAT(2G10.3,2I5,2F10.0)          READ1060
10400 FORMAT(T1,'0 DL ',8G10.3/' THETA ',8G10.3/' F ',G10.3)   READ1070
10500 FORMAT(T1,'0 PAIR,CPO,XL,V AND FOLTYP'/(T1,' ',5G20.8))   READ1080
10600 FORMAT(T1,'0 AT,ARAT,RTCON1,RTCON2,RSTEM'/(T1,' ',7G10.3))   READ1090
10700 FORMAT(T1,'0 RLIN,ALMIN,ALMAX,GM,GV'/(T1,' ',4G10.3))     READ1100
10800 FORMAT(T1,'0 RLIT,WP1,WP2,AGGIE'/(T1,' ',4G20.4))       READ1110
10900 FORMAT(1H , 'T1,T2,T3,T4 ',4G10.3)    READ1120
11000 FORMAT(1H , 'TMS,TW,SIGS,SIGW,ALBS,ALBW ',6G10.4)      READ1130
11100 FORMAT(1H , 'SDRAG,WDRAG,NSL,NS,YESMAC,DAYMAC'
+,1X,2G10.4,5X,2I5,2F10.0)             READ1140
11200 FORMAT(6G10.3,I5)                   READ1150
11300 FORMAT(1H , 'PWPS,PWPW,RESS,RESW,POWS,POWW,LRMODL'/(1X,6G15.2,I5))   READ1170
11400 FORMAT(A4)                         READ1180
11500 FORMAT(10A4)                        READ1190
11600 FORMAT(40X,10A4)                   READ1200
11700 FORMAT(8G10.4)                     READ1210
11800 FORMAT(' HYDRAULIC CONDUCTIVITY PARAMETERS',/,8(2X,G10.4))   READ1220

```

## APPENDIX B (continued)

|   |          |
|---|----------|
| 11900 FORMAT(8G10.4)  | READ1230 |
| 12000 FORMAT(' SOIL MATRIC POTENTIAL PARAMETERS',/,8(2X,G10.4)) | READ1240 |
| 12100 FORMAT(3F10.5,I5)   | READ1250 |
| 12200 FORMAT(16F5.2)  | READ1260 |
| 12300 FORMAT(16F5.0)  | READ1270 |
| 12400 FORMAT(20A4)  | READ1280 |
| 12500 FORMAT(1H ,20A4)  | READ1290 |
| 12600 FORMAT(T1,'0 CUMULATIVE INFILTRATION INPUT CURVE')        | READ1300 |
| 12700 FORMAT(T1,'0 CIF(CM)"/(T1,' ',20F5.2))                    | READ1310 |
| 12800 FORMAT(T1,'0 RTIM(MINUTES)"/(T1,' ',20F5.0))              | READ1320 |
| END   | READ1330 |

|  |          |
|--|----------|
| SUBROUTINE RSWIFT  | RSWI 10  |
| C THIS ROUTINE READS AND INITIALIZES FOR SWIFT                   | RSWI 20  |
| C SWIFT ROUTINE ACCOUNTS FOR MACROPORE FLOW EFFECTS              | RSWI 30  |
| IMPLICIT REAL*8 (A-H,O-Z)  | RSWI 40  |
| REAL*8 MCPOR,NPOR,MFB,L,MACEX,MMACEX,MMEME                       | RSWI 50  |
| REAL*8 MMEMA,MMAME,MMMA  | RSWI 60  |
| COMMON/INPTS/MCPOR(8),RP(8),WP(8),PL(8),PERC(8),AGSIZE(8)        | RSWI 70  |
| COMMON/BITS/ B(8),HWAT(8),FLOW(8),NPOR(8),DX(8)                  | RSWI 80  |
| 1,DFLOW(8),DHWAT(8),BD(8),IATOB                                  | RSWI 90  |
| COMMON/BOOKS/DMEMA(8),DMAME(8),DMAMA(8),MACEX(8),BETA(8),DBET(8) | RSWI 100 |
| COMMON/GEOMET/DL(8),AT(2),ARAT(2),FCC(8),THETA(8),SWT(8)         | RSWI 110 |
| COMMON/PORES/VP(8),F(8),SEV,ETGW,DNFAC,WP1,WP2,NSL,NBL,NS        | RSWI 120 |
| COMMON/CHMMOS/SWFBL(8),CHETA(8),SWRF1,SWRF2,RLAT(8)              | RSWI 130 |
| COMMON/PIECES/TRUNO,ZS(8),PRE1,POND,TBET(8),YESMAC,PSM(8),REMAIN | RSWI 140 |
| COMMON/MONTHS/MMAME(8),MMEMA(8),MMAMA(8),MMACEX(8),MMEME(8)      | RSWI 150 |
| COMMON/MESOP/DMEME(8)  | RSWI 160 |
| C VARIABLES IN COMMONS BOOKS & MONTHS DEFINED IN WSWIFT          | RSWI 170 |
| DATA PI/3.14159265358979/  | RSWI 180 |
| DATA FRAC/1.414213562/   | RSWI 190 |
| C DATA INPUTS  | RSWI 200 |
| C VALUES ARE FOR A 1-CM**2 CROSS SECTION                         | RSWI 210 |
| C FRAC=COSEC(ANGLE OF A PORE TO THE VERTICAL)                    | RSWI 220 |
| C I REFERS TO A SOIL LAYER                                       | RSWI 230 |
| C MCPOR(I)=TOTAL MACROPOROSITY (ML/ML)                           | RSWI 240 |
| C RP(I)=RADIUS OF CYLINDRICAL PORE (CM)                          | RSWI 250 |
| C WP(I)=WIDTH OF RECTANGULAR CRACK (CM)                          | RSWI 260 |
| C PL(I)=BREATH OF RECTANGULAR CRACK (CM)                         | RSWI 270 |
| C AGSIZE(I)=AVG LENGTH OF AGGREGATE (CM)                         | RSWI 280 |
| C PERC(I)=FRACTION OF MACROPORES WHICH ARE DEAD END              | RSWI 290 |
| C BETA(I)=WATER CONTENT OF CONTINUOUS MACROPORES (CM/LAYER)      | RSWI 300 |
| C B(I)=MAX CAPACITY OF CONTINUOUS MACROPORES(SATURATED CM/LAYER) | RSWI 310 |
| C DBET(I)=WATER CONTENT OF DEAD END MACROPORES (CM/LAYER)        | RSWI 320 |
| C BD(I)=MAX CAPACITY OF DEAD END MACROPORES (CM/LAYER)           | RSWI 330 |
| C HWAT(I)=HEAD OF WATER IN CONT. MACROPORES (CM OF WATER)        | RSWI 340 |
| C DHWAT(I)=HEAD OF WATER IN DEAD END MACROPORES (CM OF WATER)    | RSWI 350 |
| C NPOR(I)=TOTAL NUMBER OF MACROPORES (#/LAYER)                   | RSWI 360 |
| C TBET(I)=TOTAL WATER CONTENT OF MACROPORES(CM/LAYER)            | RSWI 370 |
| C DX(I)=DISTANCE FROM MACROPORES TO MESOPORES (CM)               | RSWI 380 |
| C FOLLOWING VARIABLES ORIGINATE IN PROSPR                        | RSWI 390 |
| C DL(I)=DEPTH OF SOIL LAYER (CM)                                 | RSWI 400 |
| C THETA(I)=WATER CONTENT OF MESOPORES (CM/LAYER)                 | RSWI 410 |
| C S(I)=MAX CAPACITY OF MESOPORES (CM/LAYER)                      | RSWI 420 |
| C NSL=NUMBER OF SOIL LAYERS                                      | RSWI 430 |
| C RLAT(I)=LATERAL FLOW (CM/TIME STEP)                            | RSWI 440 |
| C TRUNO=SURFACE RUNOFF (CM/TIME STEP)                            | RSWI 450 |
| C ZS(I)=HYDRAULIC CONDUCTIVITY (CM/DAY)                          | RSWI 460 |
| C DTIM=TIME STEP (FRACTIONAL DAYS)                               | RSWI 470 |
| C PRE=PRECIPITATION (CM/TIME STEP)                               | RSWI 480 |
| C POND=SWITCH SET TO 1 IF THERE IS SURFACE PONDING               | RSWI 490 |
| C YESMAC=SWITCH SET TO 0 IF NEGLECTING MACROPORES                | RSWI 500 |

## APPENDIX B (continued)

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C      PSM(I)=MATRIC POTENTIAL IN MESOPORES (CM OF WATER)          RSWI 510
C      IATOB=NUMBER OF SOIL LAYERS IN A HORIZON                   RSWI 520
C      NOMINAL VALUES ARE USED FOR ZERO INPUT DATA OF MCPOR,RP,WP,   RSWI 530
C      PL,PERC AND AGSIZE                                         RSWI 540
C      PL,PERC AND AGSIZE                                         RSWI 550
C      IATOB=0                                                 RSWI 560
C      POND=0                                                 RSWI 570
C      WRITE(6,100)
100   FORMAT(' LEVEL POROSITY    PORE RADIUS    WIDTH    LENGTH        RSWI 580
1PERCENTAGE    AGSIZE ')
DO 170 I=1,NSL
READ(5,150)MCPOR(I),RP(I),WP(I),PL(I),PERC(I),AGSIZE(I)
150   FORMAT(6F10.4)                                         RSWI 590
C      IATOB=NUMBER OF LAYERS IN "A" HORIZON                   RSWI 600
IF(PL(I).LE.1.0D-10) IATOB=IATOB+1                         RSWI 610
C      SET NOMINAL VALUES FOR ZERO INPUT DATA                 RSWI 620
IF (MCPOR(I).EQ.0.) MCPOR(I)=1.D-12                         RSWI 630
IF (RP(I).EQ.0.)  RP(I)=1.D-12                            RSWI 640
IF (WP(I).EQ.0.)  WP(I)=1.D-12                            RSWI 650
IF (PL(I).EQ.0.)  PL(I)=1.D-12                            RSWI 660
IF (PERC(I).EQ.0.) PERC(I)=1.D-12                          RSWI 670
IF (AGSIZE(I).EQ.0.) AGSIZE(I)=1.D-12                      RSWI 680
IF (AGSIZE(I).EQ.0.) AGSIZE(I)=1.D-12                      RSWI 690
IF (AGSIZE(I).EQ.0.) AGSIZE(I)=1.D-12                      RSWI 700
IF (AGSIZE(I).EQ.0.) AGSIZE(I)=1.D-12                      RSWI 710
WRITE(6,160)I,MCPOR(I),RP(I),WP(I),PL(I),PERC(I),AGSIZE(I) RSWI 720
160   FORMAT(2X,I2,2X,6F10.4)                                 RSWI 730
170   CONTINUE
REMAIN=0.0
DO 200 I=1,NSL
C      INITIALIZING WATER BUDGET ACCOUNTS                    RSWI 740
BETA(I)=0.0
DBET(I)=0.0
TBET(I)=0.0
DMEME(I)=0.0
DMEMA(I)=0.0
DMAME(I)=0.0
DMAMA(I)=0.0
MACEX(I)=0.0
MMEME(I)=0.0
MMEMA(I)=0.0
MMAME(I)=0.0
MMAMA(I)=0.0
MMACEX(I)=0.0
B(I)=MCPOR(I)*DL(I)*(1.-PERC(I))                         RSWI 750
BD(I)=MCPOR(I)*DL(I)*PERC(I)                                RSWI 760
IF(I.GT.IATOB)GO TO 190
C      NO. OF CYLINDERS IN "A" HORIZON LAYER                RSWI 770
NPOR(I)=MCPOR(I)/(PI*RP(I)**2.*FRAC)                      RSWI 780
C      ASSUMES MACROPORE LENGTH=FRAC*DL(I)                  RSWI 790
DX(I)=DL(I)/(NPOR(I)*2.*FRAC)                             RSWI 800
RSWI 810
RSWI 820
RSWI 830
RSWI 840
RSWI 850
RSWI 860
RSWI 870
RSWI 880
RSWI 890
RSWI 900
RSWI 910
RSWI 920
RSWI 930
RSWI 940
RSWI 950
RSWI 960
RSWI 970
RSWI 980
RSWI 990
RSWI 1000
RSWI 1010
RSWI 1020
RSWI 1030
RSWI 1040
C      NO. OF CRACKS IN "B" HORIZON LAYER
190   NPOR(I)=MCPOR(I)*DL(I)/(WP(I)*PL(I)*AGSIZE(I))
DX(I)=(2.*PL(I)+AGSIZE(I))/6.
200   CONTINUE
RETURN
END

```

## APPENDIX B (continued)

```

FUNCTION SOLRAD(DJULN,DGLAT)
      CALCULATION OF DAILY POTENTIAL SOLAR RADIATION
      ALGORITHM PREPARED BY LLOYD W. SWIFT JR. CHL
C      DJULN IS JULIAN DATE
C      DGLAT IS NORTH LATITUDE IN DEGREES
C      SOLRAD IS POTENTIAL DAILY DIRECT SOLAR RADIATION
C      SUNRN=SOLR CONSTANT(CAL/CM2/2/MIN)
C      TO=TRANSMISSION OF RADIATION WHEN THE SUN IS AT ZENITH
C      ALFA=NATURAL LOGRITHM OF TRANSMISSION TO
C          HA=EFFECTIVE HEIGHT OF THE ATMOSPHERE/EARTH RADIUS
C      DATA SUNRN/1.95/,ALFA,HA/-106,.002/
C      SOLAR DECLINATION
C      SINDEC=.39785*SIN(4.868961+.0172024*DJULN+.033446*
+        SIN(6.22411+.0172024*DJULN))
C      COSDEC=SQRT(1.-SINDEC*SINDEC)
C      ECCENTRICITY CORRECTION TO EARTH ORBITAL RADIUS
C      E=1.0-0.0167*COS((DJULN-3.)*0.0172024)
C      HOURLY RADIATION INCIDENT ON UPPER ATMOSPHERE
C      RI=60.*SUNRN/(E*E)
C      RADLAT=DGLAT*.01745329
C      SINLAT=SIN(RADLAT)
C      COSLAT=COS(RADLAT)
C      COSDYL=-SINLAT/COSLAT*SINDEC/COSDEC
C      IF(COSDYL.GT.-1.0) GO TO 10
C      DAYL=3.1415926
C      GO TO 20
10 DAYL=0.
      IF(COSDYL.LT.1.0) DAYL=ARCOS(COSDYL)
C      DAILY RADIATION INCIDENT ON UPPER ATMOSPHERE
20 SOLRAD=RI*.63944*(SINDEC*SINLAT*DAYL+COSDEC*COSLAT*SIN(DAYL))
C      TRANSMISSION OF DIRECT RADIATION BY CLEAR ATMOSPHERE
COSI=COSDEC*COSLAT+SINDEC*SINLAT
XMIT=EXP(ALFA*(2.+HA)/(COSI+SQRT(HA*(2.+HA)+COSI*COSI)))
C      POTENTIAL DIRECT RADIATION AT EARTHS SURFACE
SOLRAD=SOLRAD*XMIT
RETURN
END

```

## APPENDIX B (continued)

|     |  |          |
|-----|--|----------|
|     | SUBROUTINE SWIFT(K,DTIM)   | SWIF 10  |
| C   | THIS ROUTINE ACCOUNTS FOR MACROPORE FLOW EFFECTS                 | SWIF 20  |
|     | IMPLICIT REAL*8 (A-H,O-Z)  | SWIF 30  |
|     | REAL*8 MCPOR,NPOR,MAFBL,MACEX                                    | SWIF 40  |
|     | COMMON/INPTS/MCPOR(8),RP(8),WP(8),PL(8),PERC(8),AGSIZE(8)        | SWIF 50  |
|     | COMMON/BITS/B(8),HWAT(8),FLOW(8),NPOR(8),DX(8)                   | SWIF 60  |
| 1,  | DFLOW(8),DHWAT(8),BD(8),IATOB                                    | SWIF 70  |
|     | COMMON/BOOKS/DMEMA(8),DMAME(8),DMAMA(8),MACEX(8),BETA(8),DBET(8) | SWIF 80  |
|     | COMMON/GEOMET/DL(8),AT(2),ARAT(2),FC(8),THETA(8),SWT(8)          | SWIF 90  |
|     | COMMON/PORES/VP(8),F,S(8),SEV,ETGW,DNFAC,WP1,WP2,NSL,NBL,NS      | SWIF 100 |
|     | COMMON/CHMMOS/SWFBL(8),CHETA(8),SWRF1,SWRF2,RLAT(8)              | SWIF 110 |
|     | COMMON/PIECES/TRUNO,ZS(8),PRE1,POND,TBET(8),YESMAC,PSM(8),REMAIN | SWIF 120 |
|     | DATA TWOPI/6.28318531/,EXCESS/0.0/,FLXMAX/0.0/                   | SWIF 130 |
|     | DATA BYPS/.5./,FRAC/1.414213562/                                 | SWIF 140 |
| C   | DTIM=TIME STEP IN FRACTIONAL DAYS                                | SWIF 150 |
| C   | DATA, AS IN PROSPR, ARE PER CM**2 LAND AREA                      | SWIF 160 |
| C   |  | SWIF 170 |
| C   | FIRST LAYER MACROPORES   | SWIF 180 |
| C   | SURFACE INFILTRATION AND RUNOFF ACCOUNTED FOR                    | SWIF 190 |
|     | RAIN=PRE1  | SWIF 200 |
| C   | FLXMAX=MAX INFILTRATION RATE (CM/TIME STEP)                      | SWIF 210 |
|     | FLXMAX=12250.*RP(1)**2*MCPOR(1)*86400.*DTIM                      | SWIF 220 |
|     | IF(POND.EQ.0.0)RAIN=0.0  | SWIF 230 |
| C   | IF FLXMAX EXCEEDED ALLOW RUNOFF                                  | SWIF 240 |
|     | IF(RAIN.LE.FLXMAX)GO TO 250                                      | SWIF 250 |
| C   | ASSUME ALL DEAD END MACROPORES IN FIRST LAYER OPEN TO SURFACE    | SWIF 260 |
|     | BETA(1)=BETA(1)+FLXMAX*(1.-PERC(1))                              | SWIF 270 |
|     | DBET(1)=DBET(1)+FLXMAX*PERC(1)                                   | SWIF 280 |
|     | THETA(1)=THETA(1)+RAIN-FLXMAX                                    | SWIF 290 |
|     | GO TO 300  | SWIF 300 |
| 250 | DBET(1)=DBET(1)+RAIN*PERC(1)                                     | SWIF 310 |
|     | BETA(1)=BETA(1)+RAIN*(1.-PERC(1))                                | SWIF 320 |
| 300 | HWAT(1)=BETA(1)/(MCPOR(1)*(1.-PERC(1)))                          | SWIF 330 |
|     | DHWAT(1)=DBET(1)/(MCPOR(1)*PERC(1))                              | SWIF 340 |
|     | HGRAD1=(PSM(1)+HWAT(1)/2.)/(RP(1)*DLOG(DX(1)/RP(1)))             | SWIF 350 |
|     | DHGRAD=(PSM(1)+DHWAT(1)/2.)/(RP(1)*DLOG(DX(1)/RP(1)))            | SWIF 360 |
| C   | DMEMA KEEPS TRACK OF DAILY MESO TO MACROPORE FLOW                | SWIF 370 |
|     | IF(THETA(1).LE.S(1))GO TO 302                                    | SWIF 380 |
|     | DMEMA(1)=DMEMA(1)+(THETA(1)-S(1))                                | SWIF 390 |
|     | FLOW(1)=0.0  | SWIF 400 |
|     | DFLOW(1)=0.0   | SWIF 410 |
|     | GO TO 305  | SWIF 420 |
| C   | CALCULATE MACROPORE TO MESOPORE FLOW                             | SWIF 430 |
| 302 | FLOW(1)=TWOPI*RP(1)*FRAC*HWAT(1)*ZS(1)*DTIM*HGRAD1*NPOR(1)       | SWIF 440 |
|     | 1*(1.-PERC(1))   | SWIF 450 |
|     | DFLOW(1)=TWOPI*RP(1)*FRAC*DHWAT(1)*ZS(1)*DTIM*DGRAD*NPOR(1)      | SWIF 460 |
|     | 1*PERC(1)  | SWIF 470 |
|     | IF(FLOW(1).GT.BETA(1))FLOW(1)=BETA(1)                            | SWIF 480 |
|     | IF(DFLOW(1).GT.DBET(1))DFLOW(1)=DBET(1)                          | SWIF 490 |
| C   | DMAME KEEPS TRACK OF DAILY MACRO TO MESOPORE FLOW                | SWIF 500 |
|     | DMAME(1)=DMAME(1)+FLOW(1)+DFLOW(1)                               | SWIF 510 |
|     | THETA(1)=THETA(1)+FLOW(1)+DFLOW(1)                               | SWIF 520 |
|     | BETA(1)=BETA(1)-FLOW(1)  | SWIF 530 |
|     | DBET(1)=DBET(1)-DFLOW(1)   | SWIF 540 |
|     | IF(THETA(1).LE.S(1))GO TO 310                                    | SWIF 550 |
|     | DMAME(1)=DMAME(1)-(THETA(1)-S(1))                                | SWIF 560 |
| C   | FLOW FROM MESOPORE TO MACROPORE                                  | SWIF 570 |
| 305 | BETA(1)=BETA(1)+(THETA(1)-S(1))*(1.-PERC(1))                     | SWIF 580 |
|     | DBET(1)=DBET(1)+(THETA(1)-S(1))*PERC(1)                          | SWIF 590 |
|     | THETA(1)=S(1)  | SWIF 600 |
| 310 | CONTINUE   | SWIF 610 |

## APPENDIX B (continued)

```

C IF(BETA(1).LE.B(1))GO TO 315
C IF EXCEED CAPACITY ADD TO SECOND LAYER
C BETA(2)=BETA(2)+BETA(1)-B(1)
C DMAMA(2)=DMAMA(2)+(BETA(1)-B(1))
C BETA(1)=B(1)
315 IF(DBET(1).LE.BD(1))GO TO 320
C IF EXCEED CAPACITY ALLOW RUNOFF
C THETA(1)=THETA(1)+DBET(1)-BD(1)
C DBET(1)=BD(1)
320 IF(BETA(2).LE.B(2))GO TO 350
C THETA(1)=THETA(1)+BETA(2)-B(2)
C BETA(2)=B(2)
350 TBET(1)=BETA(1)+DBET(1)
REMAIN=1.
RETURN
ENTRY SUBONE(K,DTIM)

C MACROPORE FLOW BETWEEN LAYERS (K-1) AND (K)
REMAIN=1.
MAFBL=BETA(K-1)
IF(MAFBL.LE.(B(K)-BETA(K)))GO TO 370
MAFBL=B(K)-BETA(K)
BETA(K-1)=BETA(K-1)-MAFBL
BETA(K)=B(K)
GO TO 380
370 BETA(K)=BETA(K)+MAFBL
BETA(K-1)=0.0
380 CONTINUE
DMAMA(K)=DMAMA(K)+MAFBL
C ACCOUNTING FOR FLOW WITHIN LAYERS
C FLOW(K)=FLOW FROM MACROPORES TO MESOPORES
BETA(K)=BETA(K)+EXCESS
EXCESS=0.0
IF(BETA(K).LE.B(K))GO TO 400
EXCESS=BETA(K)-B(K)
BETA(K)=B(K)
400 HWAT(K)=BETA(K)/(MCPOR(K)*(1.-PERC(K)))
DHWAT(K)=DBET(K)/(MCPOR(K)*PERC(K))
DHGRAD=(PSM(K)+DHWAT(K)/2.)/DX(K)
HGRAD=(PSM(K)+HWAT(K)/2.)/DX(K)
IF(THETA(K).LE.S(K))GO TO 450
FLOW(K)=0.0
DFLOW(K)=0.0
DMEMA(K)=DMEMA(K)+(THETA(K)-S(K))
GO TO 570
450 IF(K.GT.IATOBI) GO TO 500
DHGRAD=(PSM(K)+DHWAT(K)/2.)/(RP(K)*DLOG(DX(K)/RP(K)))
HGRAD=(PSM(K)+HWAT(K)/2.)/(RP(K)*DLOG(DX(K)/RP(K)))
C FLOW FROM MACROPORE CYLINDERS
FLOW(K)=TWOPI*RP(K)*FRAC*HWAT(K)*ZS(K)*DTIM*HGRAD*NPOR(K)*
1*(1.-PERC(K))
DFLOW(K)=TWOPI*RP(K)*FRAC*DHWAT(K)*ZS(K)*DTIM*DGRAD*NPOR(K)*
1*PERC(K)
GO TO 550
500 X=BYPSS*AGSIZE(K)
C FLOW FROM MACROPORE CRACKS
FLOW(K)=2.*((WP(K)+PL(K))*(X*FRAC+(1.-X))
1*HWAT(K)*ZS(K)*DTIM*HGRAD*NPOR(K)*(1.-PERC(K))
DFLOW(K)=2.*((WP(K)+PL(K))*(X*FRAC+1.-X)*NPOR(K)*PERC(K))
1*DHWAT(K)*ZS(K)*DTIM*DGRAD
550 IF(FLOW(K).GT.BETA(K))FLOW(K)=BETA(K)

```

## APPENDIX B (continued)

```

IF(DFLOW(K).GT.DBET(K))DFLOW(K)=DBET(K) SWIF1230
DMAME(K)=DMAME(K)+FLOW(K)+DFLOW(K) SWIF1240
THETA(K)=THETA(K)+FLOW(K)+DFLOW(K) SWIF1250
IF(THETA(K).LT.0.0)CALL ERROR SWIF1260
BETA(K)=BETA(K)-FLOW(K) SWIF1270
DBET(K)=DBET(K)-DFLOW(K) SWIF1280
IF(THETA(K).LE.S(K)) GO TO 590 SWIF1290
DMAME(K)=DMAME(K)-(THETA(K)-S(K)) SWIF1300
C FLOW FROM MESO TO MACROPORE (IF MESOPORES OVERFILLED) SWIF1310
570 BETA(K)=BETA(K)+(THETA(K)-S(K))*(1.-PERC(K)) SWIF1320
DBET(K)=DBET(K)+(THETA(K)-S(K))*PERC(K) SWIF1330
C WRITE(6,707)THETA(K),BETA(K),DBET(K),K SWIF1340
C707 FORMAT(' SWFT121 ',3G16.5,I3) SWIF1350
THETA(K)=S(K) SWIF1360
IF(DBET(K).LE.BD(K))GO TO 580 SWIF1370
EXCESS=EXCESS+DBET(K)-BD(K) SWIF1380
C WRITE(6,750)EXCESS,DBET(K),BD(K),K SWIF1390
C750 FORMAT(' SWFT122 ',3G16.5,I3) SWIF1400
DBET(K)=BD(K) SWIF1410
580 CONTINUE SWIF1420
IF(BETA(K).LE.B(K))GO TO 590 SWIF1430
EXCESS=EXCESS+BETA(K)-B(K) SWIF1440
C WRITE(6,775)EXCESS,BETA(K),B(K),K SWIF1450
C775 FORMAT(' SWFT134 ',3G16.5,I3) SWIF1460
BETA(K)=B(K) SWIF1470
C BETA(NSL) ENTERS MESOPORES SWIF1480
590 MACE(X(K)=MACE(X(K)+EXCESS SWIF1490
C IF(MACE(X(K).GT.0.0) WRITE(6,777) K,MACE(X(K),EXCESS,BETA(K),DBET(K) SWIF1500
C 1,THETA(K),FLOW(K),DFLOW(K),DMAMA(K),DMEMA(K),DMAME(K), SWIF1510
C 2RLAT(K),TRUNO,FLXMAX SWIF1520
C 777 FORMAT(' ',I1,13D10.3) SWIF1530
IF(MACE(X(K).GT.100.) CALL ERROR SWIF1540
IF(K.NE.NSL)GO TO 600 SWIF1550
RLAT(K)=RLAT(K)+EXCESS SWIF1560
EXCESS=0.0 SWIF1570
REMAIN=0.0 SWIF1580
600 TBET(K)=BETA(K)+DBET(K)+EXCESS SWIF1590
RETURN SWIF1600
END SWIF1610

SUBROUTINE WSWIFT WSWI 10
C ROUTINE TO PRINT OUT DAILY/MONTHLY WATER STATUS WSWI 20
IMPLICIT REAL*8 (A-H,O-Z) WSWI 30
REAL*8 MACE,X,MMEMA,MMAME,MMAMA,MMACEX,MMEME WSWI 40
DIMENSION DBETA(8),DDBET(8),DTHT(8) WSWI 50
COMMON/MONTHS/MMAME(8),MMEMA(8),MMAMA(8),MMACEX(8),MMEME(8) WSWI 60
COMMON/MESOP/DMEME(8) WSWI 70
COMMON/GEOMET/DL(8),AT(2),ARAT(2),PC(8),THETA(8),SWT(8) WSWI 80
COMMON/PORES/VP(8),P,S(8),SEV,ETGW,DNPAC,WP1,WP2,NSL,NBL,NS WSWI 90
COMMON/BOOKS/DMEMA(8),DMAME(8),DMAMA(8),MACE(X(8),BETA(8),DBET(8) WSWI 100
COMMON/FONG/DAYMAC WSWI 110
C DMEMA(J)=DAILY MESOPORE TO MACROPORE FLOW WSWI 120
C DMEME(J)=DAILY MESOPORE TO MESOPORE FLOW WSWI 130
C DMAME(J)=DAILY MACROPORE TO MESOPORE FLOW WSWI 140
C DMAMA(J)=DAILY MACROPORE TO MACROPORE FLOW WSWI 150
C MACE(X(J)=DAILY MACROPORE EXCESS WSWI 160
C MMAME(J)=MONTHLY MACROPORE TO MESOPORE FLOW WSWI 170
C MMEMA(J)=MONTHLY MESOPORE TO MACROPORE FLOW WSWI 180
C MMEME(J)=MONTHLY MESOPORE TO MESOPORE FLOW WSWI 190
C MMAMA(J)=MONTHLY MACROPORE TO MACROPORE FLOW WSWI 200
C MMACEX(J)=MONTHLY MACROPORE EXCESS WSWI 210
DO 111 J=1,NSL WSWI 220
DBETA(J)=BETA(J)/DL(J) WSWI 230
DDBET(J)=DBET(J)/DL(J) WSWI 240
DTHT(J)=THETA(J)/DL(J) WSWI 250

```

## APPENDIX B (continued)

```

C DAILY WATER STATUS
111 CONTINUE
    IF(DAYMAC.EQ.0.0) GO TO 799
    WRITE(6,100)(DMAME(I),I=1,NSL)
100  FORMAT(' DMAME (CM/DAY) ',8(E12.4,2X))
    WRITE(6,200)(DMEMA(I),I=1,NSL)
200  FORMAT(' DMEMA (CM/DAY) ',8(E12.4,2X))
    WRITE(6,300)(DMAMA(I),I=1,NSL)
300  FORMAT(' DMAMA (CM/DAY) ',8(E12.4,2X))
    WRITE(6,400)(MACEX(I),I=1,NSL)
400  FORMAT(' MACEX (CM/DAY) ',8(E12.4,2X))
    WRITE(6,450)(DMEME(I),I=1,NSL)
450  FORMAT(' DMEME (CM/DAY) ',8(E12.4,2X))
    WRITE(6,500)(DBETA(I),I=1,NSL)
500  FORMAT(' BETA/DL(ML/ML) ',8(E12.4,2X))
    WRITE(6,600)(DDBET(I),I=1,NSL)
600  FORMAT(' DBET/DL(ML/ML) ',8(E12.4,2X))
    WRITE(6,700)(DTHTET(I),I=1,NSL)
700  FORMAT(' THETA/DL(ML/ML) ',8(E12.4,2X))
C SET UP MONTHLY WATER ACCOUNTS
799 CONTINUE
    DO 800 J=1,NSL
    MMAME(J)=MMAME(J)+DMAME(J)
    DMAME(J)=0.0
    MMEME(J)=MMEME(J)+DMEME(J)
    DMEME(J)=0.0
    MMEMA(J)=MMEMA(J)+DMEMA(J)
    DMEMA(J)=0.0
    MMAMA(J)=MMAMA(J)+DMAMA(J)
    DMAMA(J)=0.0
    MMACEX(J)=MMACEX(J)+MACEX(J)
    MACEX(J)=0.0
800  CONTINUE
    RETURN
C MONTHLY WATER STATUS
ENTRY TMMONTH
    WRITE(6,105)
105  FORMAT(16X,' MONTHLY WATER BUDGETS      ')
    WRITE(6,110)(MMAME(I),I=1,NSL)
110  FORMAT(' MMAME (CM/MTH) ',8(E12.4,2X))
    WRITE(6,210)(MMEMA(I),I=1,NSL)
210  FORMAT(' MMEMA (CM/MTH) ',8(E12.4,2X))
    WRITE(6,310)(MMAMA(I),I=1,NSL)
310  FORMAT(' MMAMA (CM/MTH) ',8(E12.4,2X))
    WRITE(6,410)(MMACEX(I),I=1,NSL)
410  FORMAT(' MMACEX(CM/MTH) ',8(E12.4,2X))
    WRITE(6,510)(MMEME(I),I=1,NSL)
510  FORMAT(' MMEME (CM/MTH) ',8(E12.4,2X))
    DO 900 J=1,NSL
    MMAME(J)=0.0
    MMEME(J)=0.0
    MMEMA(J)=0.0
    MMAMA(J)=0.0
    MMACEX(J)=0.0
900  CONTINUE
    RETURN
END

```

## APPENDIX B (continued)

```

SUBROUTINE XPREC(PRT,PACK,IDSID,SINTC,P3,P4)          XPRE 10
C      ROUTE PRECIPITATION THRU INTERCEPTION STORAGE TO LAND   XPRE 20
C      SURFACE. PRT IS INCIDENT PRECIPITATION AND INCLUDES ANY   XPRE 30
C      SPRINKLER TYPE IRRIGATION.                                XPRE 40
COMMON/SHIFT1/ RADCON,CONMLT,SCF,ELDIF, IDNS,FCI,DGM,WC,MPACK, K1, XPRE 50
> A, LG, SS, NN, K24L, EPXM,SUNCON,CLD,CLDFAC           XPRE 60
C      CONTAMINANT TRANSPORT IS REMOVED TEMPORARILY. 12 19 75-DDH. XPRE 70
C      COMMON/SHIFT2/                                         XPRE 80
C      + BARE, ANOT, KD, LFTOVR, OCRIT, ONCRIT, AZERO, SDPM, SEDMP, XPRE 90
C      + SONE, STWO, STRE, SFOR                            XPRE 100
COMMON/MISC/ SIMP,SSUR,SAR1,SAR2,SBAS,STOT,SRCH,SLTO,SRA,SIEN, XPRE 110
> SPRS,SOILEV, TOTELH,SNEVAP,SNET,SPET,STSNO,SCEP,RES,STDEP,STUS, XPRE 120
> STDS1,STDS2,STGW,STBT                                XPRE 130
COMMON/SURFXP/RZ,PR,ORAIN,FF,FIXM,RGX,SHRD,A3,AUZS,ASDS,AINF XPRE 140
COMMON/LOCALS/RU,SCI,F1,F1A,GWF,LOS,EP,RECE,ROS,HRLYRN,EPHRLI, XPRE 150
> AETR                                              XPRE 160
COMMON/XPRE/DEP,SEP,INDRTS                           XPRE 170
COMMON/INVGA/STANF,WB,NAME(6),ELEV,LAT(3),LONG(3),GTYPE(2) , XPRE 180
> INTRVL, ELEM(5), INITP,DSNAME,STRTYR,ENDYR, INITR, RODSNA,ROSTYR, XPRE 190
> RENDYR, INITD,DDSNAM,DSTYR,DENDYR, INITR, DSDSNA,DSSTYR,DSENDY, XPRE 200
> FRADCN,FCNMLT,FSCF,FELDIF,FIDNS, FFCI,FDGM,FWC,FMPACK, FK1,FA, XPRE 210
> FL, FSS, FNN, FK24L, FEPXM,                         XPRE 220
C      THE FOLLOWING 13 PARAMETERS TEMPORARILY REMOVED 12 19 75 XPRE 230
C      + BARES, ANOTS, KDS, LFTOVS, OCRITS, ONCRTS, AZEROS, XPRE 240
C      + SDPMS, SEDMPS,SONES, STWOS, STRES, SFORS,          XPRE 250
> SGWINV,LZSINV,LIQW,DEPTH,NEMELT,PCK,KEYTIM, DUM1,DUM2, UNUSED(24) XPRE 260
COMMON/AR/AREA1,AREA2,PA                               XPRE 270
REAL LG, IDNS, MPACK, K1, K24L, NN, LZSINV, LIQW, NEMELT, LOS XPRE 280
INTEGER DSNAME,STRTYR,ENDYR,RODSNA,ROSTYR, RENDYR,          XPRE 290
> DSTYR,DENDYR, DSDSNA,DSSTYR,DSENDY                XPRE 300
REAL*8 P4, AREA1, AREA2, PA                          XPRE 310
IDSID=0                                              XPRE 320
IF (PRT.LE.0.0) GO TO 20                            XPRE 330
SEP=SEP+PRT                                         XPRE 340
IF(A.LT.FA)=FA                                       XPRE 350
IF (PACK.GT.0.0) GO TO 40                            XPRE 360
EPX=AMAX1(EPMX-SCEP,0.)                            XPRE 370
C      WILL PRECIPITATION EXCEED INTERCEPTION STORAGE ? XPRE 380
IF (PRT.GT.EPX) GO TO 30                            XPRE 390
SCEP = SCEP + PRT                                     XPRE 400
SINTC=SINTC + PRT                                     XPRE 410
C      NO PRECIP OR PRECIP DOES NOT EXCEED INTERCEPTION STORAGE XPRE 420
20 P3 = 0.0                                           XPRE 430
A3 = 0.0                                              XPRE 440
RU = 0.0                                              XPRE 450
SCI = 0.0                                              XPRE 460
C      AZERO = AZERO + DEP                             XPRE 470
IF (RES.GT.0.0) GO TO 50                            XPRE 480
INDRTS=INDRTS+1                                      XPRE 490
P4=0.0                                              XPRE 500
ROS = 0.0                                              XPRE 510
IDSID=1                                              XPRE 520
GO TO 70                                             XPRE 530
30 P3 = PRT - EPX                                     XPRE 540
C P3 IS RAIN REACHING THE LAND                      XPRE 550
RU = P3 * A                                         XPRE 560
IF(A.EQ.1.0.AND.RES.EQ.0.0)IDSID=1                 XPRE 570
CRU IS IMPERVIOUS AREA RUNOFF                      XPRE 580
SIMP = SIMP + RU                                     XPRE 590
SCEP = SCEP + EPX                                    XPRE 600
SINTC=SINTC + EPX                                    XPRE 610

```

## APPENDIX B (continued)

```

C GDF = 1.0 - EXP(-1.0*P3/EPXM)
C CONTAMINANT SIMULATION REMOVED TEMPORARILY---DDH 12 19 75.
A3 = 0.0
C A3 = AZERO*GDF+DEP*(1.0-EPXM*GDF/P3)
C AZERO = AZERO +DEP - A3
C ORAIN IS RAINFALL ENERGY CONTRIBUTION TO AVAILABLE
C STREAMPOWER FOR PRODUCING EROSION.
ORAIN=0.107*LG*PRT*(1.0-2.718**(-1.08*((4.0*PRT)**0.25)))**2.0
SCI = A3*A
C IMPERVIOUS AREA CHANNEL INPUT
GO TO 50
40 P3=PRT
RU=P3*A
SIMP=SIMP+RU
50 P4 = P3 + RES -RU
C
70 A=0.
PA=1.0
RETURN
END

```



## APPENDIX C

Job Control Language for Submission of AGTEHM  
to IBM System 3033 Computer

```

//DMHMC001 JOB (18310),'XCSD-HETRICK-B216'
//**CLASS CPU91=300S,REGION=550,IO=9,L=45
/*ROUTE PRINT LOCAL
/*ROUTE PUNCH LOCAL
//STP1 EXEC FORTHCLG,REGION.GO=50K
//FORT.SYSIN DD * FORTRAN SOURCE DECK FOLLOWS THIS CARD
    DIMENSION LIST(20)
201 FORMAT (10X,20A4)
100 READ (05,200,END=199) LIST
200 FORMAT (20A4)
    PRINT 201, LIST
    WRITE(50,200) LIST
    GO TO 100
199 END FILE 50
    STOP
    END
/*
//LKED.SYSIN DD *
/*
//GO.FT50F001 DD UNIT=SYSDA,DSNAME=&&TEMP,DISP=(NEW,PASS),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=7280),SPACE=(3200,(20),RLSE)
//GO.FT05F001 DD * CARD DATA INPUT FOLLOWS THIS CARD
=CORNY1.AGR[6137,201]
/*
//STP2 EXEC FORTHCLG,PARM.FORT='XREF,XL,OPT=2,NODECK,SOURCE',
//      REGION.FORT=350K,PARM.LKED='OVLY,MAP,LIST,XREF,SIZE=(200K,36K)',
//      REGION.LKED=230K,
//      PARM.GO='EU=-1,SO=51,SI=50,TIME=5',REGION.GO=550K
//FORT.SYSIN DD * FORTRAN SOURCE DECK FOLLOWS THIS CARD
=CHANGE.NEW
/*
//LKED.SYSLIB DD
// DD
// DD
//          DD DSN=ENVSCI.DDH14268.TEHM,DISP=SHR
//          DD DSN=ENVSCI.DDH14881.WHTM,DISP=SHR
//          DD DSNAME=Z.CWN10332.ORGRAPH,DISP=SHR
//LKED.PROSPER DD DSN=T.DMH18310.PROSPER,DISP=SHR
//LKED.SYSIN DD *
INCLUDE PROSPER
INSERT MAIN
INSERT CLEAR
OVERLAY ZERO
INSERT CLEARO
OVERLAY ZERO
INSERT OLDAI

```

## APPENDIX C (continued)

INSERT CVBCBIDK  
INSERT OPNDSK,RITE,READER  
INSERT PRC  
INSERT IDCODE  
INSERT LASDAY  
INSERT E  
INSERT PARAM  
INSERT HOLNAM  
INSERT UNITS  
INSERT A  
INSERT B  
INSERT C  
INSERT D  
INSERT F  
INSERT FF  
INSERT ITWRD  
INSERT RAC30M  
INSERT SU30M  
INSERT SU30MR  
INSERT PRCRV  
INSERT TOTP  
INSERT TOTPRV  
INSERT IDAY  
INSERT TIME  
INSERT TOTD  
INSERT LSRA  
INSERT LSRNF  
INSERT YLGINT  
INSERT PDTEMP  
INSERT TOTS  
INSERT INVFIL  
INSERT INVGA  
INSERT FLAGS  
INSERT SOISNO  
INSERT SHIFT1  
INSERT SHIFT3  
INSERT MISC  
INSERT T  
INSERT JEJ1  
INSERT CNTRL  
INSERT ROUTS  
INSERT T2  
INSERT CHTMP  
INSERT FLOTMP  
INSERT DEPVAL  
INSERT DAM1  
INSERT SUMS  
INSERT IH2P2  
INSERT PRINT  
INSERT DEPOS  
INSERT BIMON  
INSERT TIMEWD

## APPENDIX C (continued)

INSERT DATIM  
INSERT TAPEO  
INSERT S  
OVERLAY TWO  
INSERT CLEAR2  
OVERLAY TWO  
INSERT PRECIP  
INSERT OUTREC  
INSERT ADDATA  
INSERT OPNSET  
INSERT RDHRLY  
INSERT RDSTOR  
INSERT MODEPS  
INSERT INF ile  
OVERLAY TWO  
INSERT LAND  
INSERT TLYR  
INSERT SSF  
INSERT DAILY  
INSERT HRLYS  
INSERT RAATS  
INSERT YLAG  
INSERT CM  
INSERT AWYPLC  
INSERT PRSPLC  
INSERT INTL  
INSERT QQCPA  
INSERT FIXPLT  
INSERT SETPLT  
INSERT CRT  
INSERT PLOTS  
INSERT CRTNUM  
INSERT CRTSYM  
INSERT NUMBER  
INSERT QQNEWS  
INSERT QQPRIN  
INSERT QQPRTS  
INSERT QQROTE  
INSERT QQINCH  
INSERT QQICON  
INSERT RNDPLT  
INSERT AXIS  
INSERT BOX  
INSERT GRID  
INSERT LABEL  
INSERT QQCPA  
INSERT RANGE  
INSERT SCALE  
INSERT SIGN  
INSERT SYMBOL  
INSERT LINEUP  
INSERT LINPLT

## APPENDIX C (continued)

INSERT LABEL2  
INSERT NUMBCD  
INSERT QQEDIT  
INSERT QQLINE  
INSERT QQQFMT  
INSERT LEGEND  
INSERT ROUNDf  
INSERT STEPf  
INSERT PROSPR  
INSERT TABLOK  
INSERT FORLOK  
INSERT EVAL  
INSERT EVAPOR  
INSERT GROUND  
INSERT RNLONG  
INSERT SATVP  
INSERT SOLVO1  
INSERT SUBEV  
INSERT PHOTO  
INSERT BIODAT  
INSERT SULU  
INSERT FORMUL  
INSERT ANGLES  
INSERT SUBSRF,EQS  
INSERT THSET  
INSERT EQUA  
INSERT PMONTH  
INSERT M30  
INSERT MOSUMS  
INSERT SOLPOT  
INSERT SSRF  
INSERT AR  
INSERT SRFSUM  
INSERT RAIN  
INSERT HUMID  
INSERT GEOMET  
INSERT PIECES,BOOKS,INPTS,MONTHS  
INSERT SWIFT,RSWIFT,WSWIFT,SUBONE,TMONTH  
INSERT THINGS  
INSERT BLOCKE  
INSERT PETRUS  
INSERT PORES  
INSERT RESIST  
INSERT TIMES  
INSERT TOTMON  
INSERT TODAY  
INSERT DRAG  
INSERT SURF  
INSERT DAYMID  
INSERT PLACE  
INSERT HOOKUP  
INSERT LOCALS

## APPENDIX C (continued)

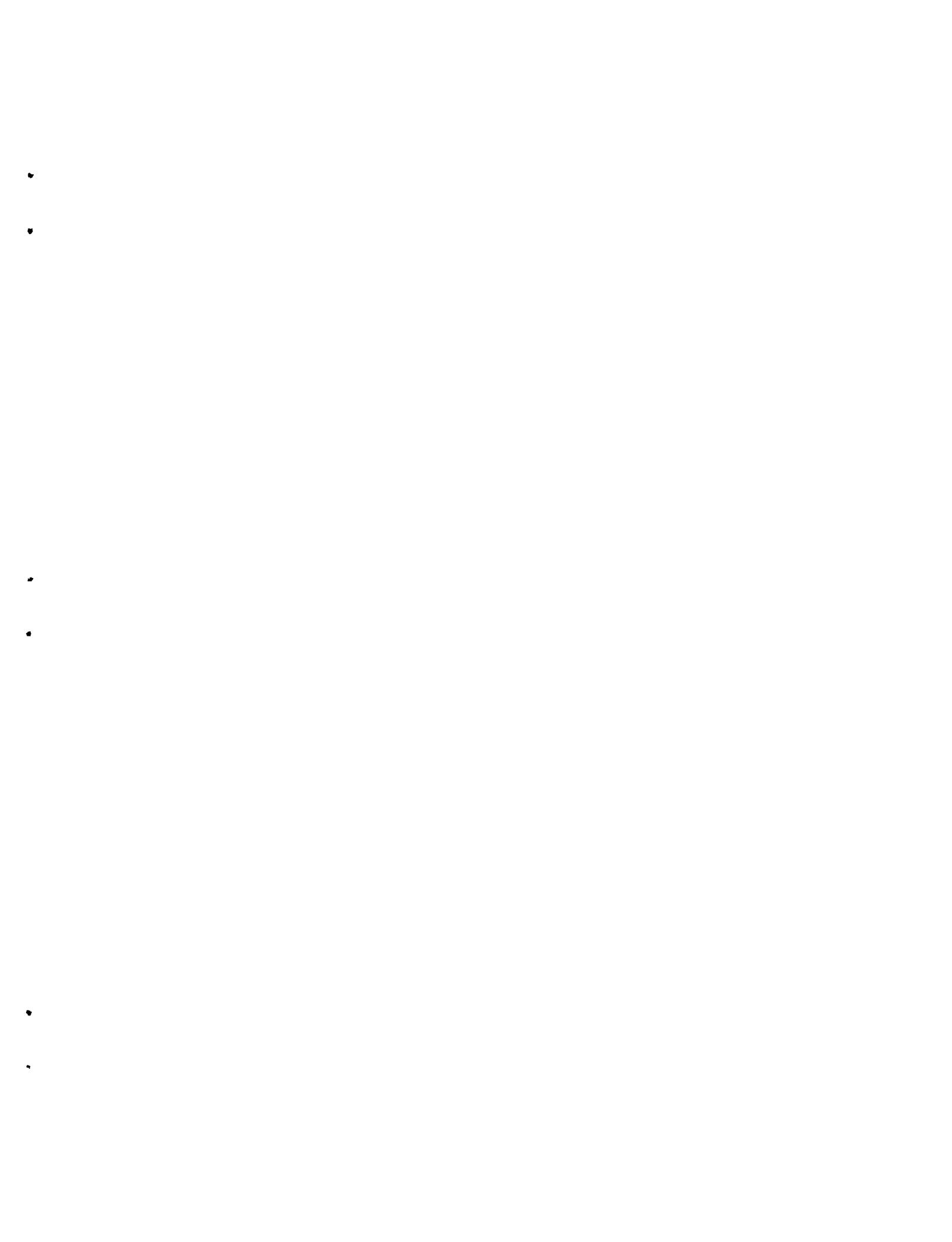
INSERT SURFXP  
INSERT GET  
INSERT NMON  
INSERT XPRE  
INSERT SNO  
INSERT NSEG  
INSERT PEV  
INSERT MONDAT,DEFER,SOLRAD,RADIST  
INSERT NATEMP,INDEX  
INSERT XPREC  
INSERT PEVSRF  
INSERT DLAYIN  
INSERT CERES  
INSERT SCEHM  
INSERT DRYADS  
INSERT DIFMAS  
INSERT CHMEX  
INSERT FLO  
INSERT RKUTT  
INSERT KUTTA  
INSERT ANUSEG  
INSERT ANUMON  
INSERT BELCH  
INSERT ANUDAY,HRADSL  
INSERT SNOMLT  
OVERLAY THREE  
INSERT GETSET,READIN,ASPECT,EVAPO,SOIL  
INSERT RDCCR,RDCHM,EXAMTS,OUTPT,RDDRY  
INSERT RDIRIG  
OVERLAY THREE  
INSERT PUTOUT  
INSERT AWYPLT  
INSERT PRSPLT  
INSERT CERPLT  
INSERT DRYPLT  
INSERT BUF  
OVERLAY TWO  
INSERT CHANL  
INSERT CIRCRN  
INSERT DAMRUN  
INSERT SUM  
INSERT INITCH  
INSERT ITWRD  
INSERT RAC30M  
INSERT SU30M  
INSERT SU30MR  
INSERT PRCRV  
INSERT TOTP  
INSERT TOTPRV  
INSERT IDAY  
INSERT TIME  
INSERT TOTD

## APPENDIX C (continued)

INSERT LSRA  
INSERT LSRNF  
INSERT YLGINT  
INSERT PDTEMP  
INSERT TOTS  
INSERT INVFIL  
INSERT INVGA  
INSERT FLAGS  
INSERT SOISNO  
INSERT SHIFT1  
INSERT SHIFT3  
INSERT MISC  
INSERT T  
INSERT JEJ1  
INSERT CNTRL  
INSERT ROUTS  
INSERT T2  
INSERT CHTMP  
INSERT FLOTMP  
INSERT DEPVAL  
INSERT DAM1  
INSERT SUMS  
INSERT IH2P2  
INSERT PRINT  
INSERT DEPOS  
INSERT BIMON  
INSERT TIMEWD  
INSERT DATIM  
INSERT TAPEO  
INSERT S  
OVERLAY TWO  
INSERT CLEAR2  
OVERLAY TWO  
INSERT PRECIP  
INSERT OUTREC  
INSERT ADDATA  
INSERT OPNSET  
INSERT RDHRLY  
INSERT RDSTOR  
INSERT MODEPS  
INSERT INFILE  
OVERLAY TWO  
INSERT LAND  
INSERT TLYR  
INSERT SSF  
INSERT DAILY  
INSERT HRLYS  
INSERT RAATS  
INSERT YLAG  
INSERT CM  
INSERT AWYPLC

## APPENDIX C (continued)

```
INSERT INFLOS
INSERT LAGRAN
INSERT FLOWIN
INSERT MEANDF
INSERT MSPOL
INSERT PRPLT
INSERT REACHS
INSERT SKIP
INSERT INITIA
INSERT SR25
INSERT RNOFF
INSERT JEJ
INSERT CHANID
INSERT MINI
OVERLAY TWO
INSERT DTRSTR
INSERT CHANGE
/*
//GO.FT01F001 DD UNIT=SYSDA,DSNAME=&TEMP1,DISP=NEW,SPACE=(344,(100))
//GO.FT02F001 DD UNIT=SYSDA,DSNAME=&TEMP2,DISP=NEW,SPACE=(8948,(100)),
//    DCB=RECFM=FT
//GO.FT03F001 DD UNIT=SYSDA,DSNAME=&TEMP3,DISP=NEW,SPACE=(2424,(10))
//GO.FT04F001 DD UNIT=SYSDA,DSNAME=&TEMP4,DISP=NEW,SPACE=(584,(1200))
//GO.FT10F001 DD UNIT=SYSDA,SPACE=(12288,16),
// DCB=(RECFM=FT,BLKSIZE=12288)
//GO.SYSUDUMP DD SYSOUT=A
//GO.FT07F001 DD SYSOUT=B,DCB=(RECFM=FB,LRECL=80,BLKSIZE=3520)
//GO.FT05F001 DD UNIT=SYSDA,DSNAME=&&TEMP,DISP=(OLD,DELETE)
//GO.FT50F001 DD *
/*
//
ENDINPUT
```



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