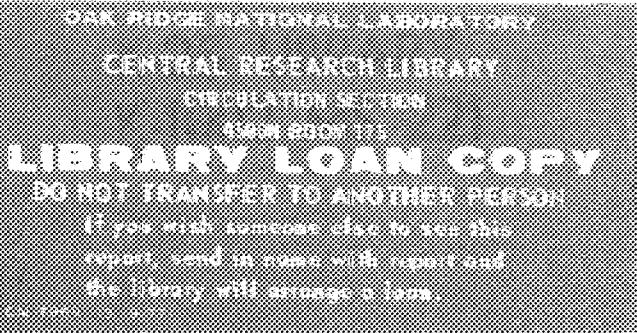


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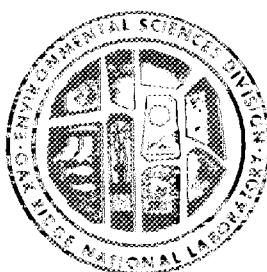
**AT123D: Analytical Transient
One-, Two-, and Three-Dimensional
Simulation of Waste Transport
in the Aquifer System**

G. T. Yeh



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ENVIRONMENTAL SCIENCES DIVISION
Publication No. 1439



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SIMULATION OF WASTE TRANSPORT IN THE AQUIFER SYSTEM

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NUCLEAR WASTE PROGRAMS
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ABSTRACT

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A generalized analytical transient, one-, two-, and/or three-dimensional (AT123D) computer code is developed for estimating the transport of wastes in a groundwater aquifer system. It contains 450 options: 288 for the three-dimensional case, 72 for the two-dimensional case in the x-y plane, 72 for the two-dimensional case in the x-z plane, and 18 for the one-dimensional case in the longitudinal direction. These are the combinations of three types of wastes, eight sets of source configurations, three kinds of source releases, and four variations of the aquifer dimensions. Three types of the wastes are radioactive waste, chemicals, and heat. The eight types of source configurations are a point source, a line source parallel to the x-axis, a line source parallel to the y-axis, a line source parallel to the z-axis, an area source perpendicular to the x-axis, an area source perpendicular to the y-axis, an area source perpendicular to the z-axis, and a volume source. Three kinds of source releases are instantaneous, continuous, and finite duration releases. Four variations of the aquifer dimensions are finite depth and finite width, finite depth and infinite width, infinite depth and finite width, and infinite depth and infinite width. The mechanisms of transport included in the analysis are advection, hydrodynamic dispersion, adsorption, decay/degeneration, and waste losses to the

atmosphere. Boundary conditions included Dirichlet, Neumann, mixed type, and/or radiation boundaries. Fifty sample cases are provided to illustrate the application of AT123D to various situations.

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I. INTRODUCTION

Since the early seventies there has been an accelerating interest in the area of groundwater pollution. In recent years, several vigorous environmental monitoring programs have resulted in the identification of hundreds of sites throughout the country where groundwater resources have been polluted by hazardous wastes or are in imminent danger of contamination. A particularly tragic example is the Love Canal case near Niagara Falls, New York, where a variety of discarded hazardous chemicals entered the basements of nearby homes after traveling through the ambient groundwater (ABC News Close Up: The Killing Ground, March 29, 1979). Many Federal EPA-sponsored studies of hazardous waste disposal sites throughout the United States have shown that potentially dangerous situations are not rare, as thousands of similar sites in the United States are simply waiting for public discovery (ABC News Close Up: The Killing Ground, March 29, 1979).

Increasing public concerns of the above problems and the legal provisions of the Resource Conservation and Recovery Act of 1976, the 1974 Safe Drinking Water Act, and the 1972 amendments to the Federal Pollution Control Act have compelled industry, the public sector, and private business to carefully formulate waste management plans and evaluate disposal sites for hazardous wastes. Adequate but less time-consuming techniques are therefore needed to provide good initial estimates of the dispersion, advection, and adsorption characteristics of a specific disposal site because waste management planning is becoming less conceptual and more quantitative as the volume of wastes

increases and concern is expressed of their environmental compatibility. Complete analysis of a given site requires extensive investigation, including boring, pumping tests, physical model simulations, and sophisticated numerical models, which are considered too expensive and impractical during the preliminary disposal site-selection stage. More often than not, an adequate analytical model is highly desirable and useful not only for screening alternative waste disposal sites but also for detailed planning and design of field measurements and monitoring programs. It must be emphasized that a considerable amount of time and expense would undoubtedly be saved by utilizing analytical predictive models in planning field surveys and establishing monitoring programs.

Numerous analytical models for predicting the transport and migration of hazardous wastes in the subsurface media are available (Lapidus and Amundson 1952, Davidson et al. 1968, Lindstrom and Boersma 1971, Lai and Jurinak 1972, Warrick et al. 1972, Cleary et al. 1973, Lindstrom and Stone 1974, Marino 1974, Kuo 1976, Yeh and Tsai 1976, Van Genuchten and Wierenga 1976, Selim and Mansell 1976, Wang et al. 1977). Each of these deal with a particular problem. All of them involve more or less simplification in order to render possible analytical simulation of the governing equation. For example the simplification in the early analytical solution often involve the assumption of the infinite extent of the media. Recently, progress has been made to relax this assumption by allowing both the depth and width of the aquifer to be finite.

This report presents a generalized analytical transient, one-, two-, and/or three-dimensional model (AT123D) with the computer code to

compute the spatio-temporal distribution of wastes in the aquifer system. In the search for closed-form solution, the application of Green's function is utilized to optimum advantage. There are practically no limitations on the configuration and situation of source releases and types of boundary conditions. This results from the versatility of using Green's functions. The code in fact contains 450 options: 288 for the three-dimensional case, 72 for each of the two-dimensional cases in the x-y and x-z planes, respectively, and 18 for the one-dimensional case in the longitudinal direction. The attached computer program provides the engineering community a ready tool for the preliminary assessment of waste disposal sites.

II. MATHEMATICAL STATEMENTS

As pollutants are released into groundwater, several factors contribute to their migration and transport. First of all, the solutes in the porous media will move with the mean velocity of the solvent. This mechanism is termed advection. If this were the only mechanism governing the transport of solutes, it would behave as an aggregated solid particle traveling through the media without any lengthening or spreading. In reality, the body of solute will spread because the solution does not move uniformly in the porous media, though it does in the average sense. The flow parcel travels slower near the walls of the pore than in the center; it flows faster in larger pores than in small pores; it does not travel in a particular direction but meanders randomly. This mechanism of migration is called hydraulic dispersion. Another process causing the growth in size of the solute patches is molecular diffusion. This is caused by the random Brownian motion of molecules in the solution and occurs whether the solution in the porous media is stationary or has average motion. This diffusion process is normally small compared to the hydraulic dispersion and its effects are usually combined in the term of dispersion.

In addition to advection, hydraulic dispersion and molecular diffusion, the transport and concentration of the solute(s) are affected by reversible ion exchange with the soil grains; the chemical degeneration with other constituents; fluid compression and expansion; and, in the case of radioactive wastes, by the radioactive decay. Neglecting fluid compression and, expansion, the equations governing

the distribution of contaminant is (Robertson 1974, Duguid and Reeves 1976, Yeh and Ward 1981):

$$\frac{\partial n_e C}{\partial t} = \underbrace{v \cdot (n_e \bar{D} v C)}_{a} - \underbrace{\nabla \cdot C \vec{q}}_{b} + \dot{M} - K n_e C - \lambda n_e C \underbrace{- \left\{ \frac{\partial (\rho_b C_s)}{\partial t} + \lambda \rho_b C_s \right\}}_{g} \quad (1)$$

where

g

\vec{q} = Darcy velocity vector (LT^{-1})

\bar{D} = hydraulic dispersion coefficient tensor ($L^2 T^{-1}$)

C = dissolved concentration of the solute (ML^{-3})

C_s = absorbed concentration in the solid (MM^{-1})

ρ_b = bulk density of the media (ML^{-3})

\dot{M} = rate of release of source ($ML^{-3} T^{-1}$)

n_e = effective porosity (L^0)

λ = radioactive decay constant (T^{-1})

K = degradation rate (T^{-1})

Term a in Eq. (1) is the time rate of change of waste solute mass per unit volume of the aquifer water; term b, the combined effect of hydraulic dispersion and molecular diffusion; term c, the effects of advective transport; term d, the contribution of waste source ; term e, the effects of first order chemical and biological degradation; term f, the effects of radioactive decay; and term g, the effects of reversible ion exchange or sorption.

The initial condition of Eq. (1) is assumed to be known:

$$C = C_i (x, y, z, 0) \text{ at } t = 0 \text{ in } R , \quad (2)$$

where C_i is a given function of spatial coordinates, x , y , and z ; R is a region bounded by the curve, $S(x,y,z) = 0$, as shown in Fig. 1. This C_i may also be obtained by simulating the steady state version of Eq. (1) with steady boundary conditions and groundwater flow field. Three types of boundary conditions may be specified depending on the physical constraints. The first type is the Dirichlet boundary condition, according to which the concentration is prescribed:

$$C = C_1(x,y,z,t) \text{ on } S_1 , \quad (3)$$

where S_1 is a portion of S and C_1 is a given function of time and the location on S_1 . The second type is the Neumann boundary condition, according to which the normal gradient of the concentration is prescribed:

$$- n_e \bar{D} \cdot \nabla C \cdot \vec{n} = q_2(x,y,z,t) \text{ on } S_2 , \quad (4)$$

where \vec{n} is the unit vector normal to the S_2 portion of the surface S , $q_2(x,y,z,t)$ is the given function of time t , and space (x,y,z) on S_2 .

A third type or mixed type (Cauchy) boundary condition, which is applied to the flow-through boundaries with flows into the region, can be written as

$$- (n_e \bar{D} \cdot \nabla C - \vec{q}C) \cdot \vec{n} = q_3(x,y,z,t) \text{ on } S_3 , \quad (5)$$

where q_3 is a given function of time and the point (x,y,z) , on the S_3 portion of S . If the pollutant to be modelled is heat, another type of boundary condition, referred to as radiation condition, may be specified as

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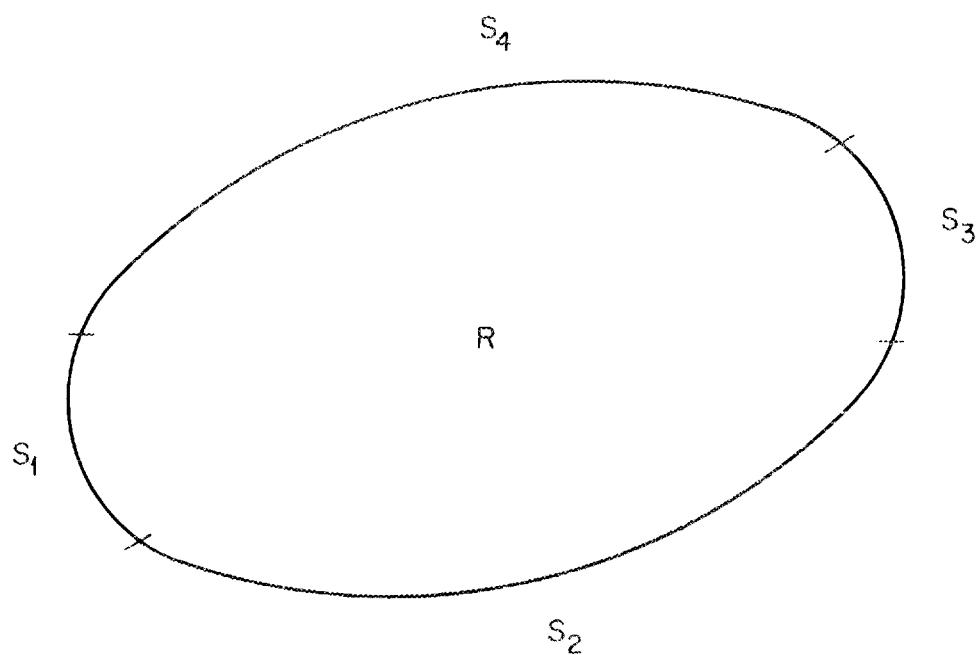


Fig. 1. Spatial boundary of the region of interest.

$$n_e \vec{D} \cdot \nabla C \cdot n + n_e K_e^* C = 0 \text{ on } S_4 , \quad (6)$$

where K_e^* is the modified heat exchange coefficient (Yeh 1980), and S_4 is the air-soil interface. The boundaries, S_1 , S_2 , S_3 , and S_4 , constitute the whole boundary $S(x,y,z) = 0$ as shown in Fig. 1.

III. ANALYTICAL SIMULATION

The solution of Eq. (1) for a complex groundwater system is extremely difficult. It is the general practice to simplify Eq. (1) before it is adopted. Depending on the physical problems, various simplifications can be made.

Several two-dimensional groundwater mass transport models have been developed (Bredhoft and Pinder 1973, Robertson 1974, Duguid and Reeves 1976, Yeh and Ward 1981, Yeh and Strand 1981) for predicting the movement of containment in a non-homogeneous aquifer system. The groundwater characteristics such as seepage velocity, porosity, permeability, dispersivities, etc., are in general not uniform in space. Numerical simulations of groundwater dynamics and mass transport are therefore necessary. However, for the "first pass" estimates and the design of a monitoring system, transport phenomena on the local scale would be sufficient. Under such circumstances, the assumptions of fairly uniform groundwater characteristics are justifiable. A further assumption is made that the sorption is in a state of instantaneous linear isothermal equilibrium. In other words, it is assumed that the adsorption of the constituent by the solid soil matrix is to occur at a rapid rate such that the dissolved material is in equilibrium with the material absorbed by the solids under isothermal conditions. With these simplifications, Eq. (1) is then reduced to (Robertson 1974):

$$\frac{\partial C}{\partial t} = \nabla \cdot (\bar{K} \nabla C) - \nabla \cdot \bar{U}C - \left(\frac{K}{R_d} + \lambda \right) C + \frac{\dot{M}}{n_e R_d} , \quad (7)$$

where

$$R_d = \text{Retardation Factor} = 1 + \rho_b K_d / n_e$$

$$\bar{\bar{K}} = \text{Retarded Dispersion Tensor} = \bar{\bar{D}} / R_d$$

$$\vec{U} = \text{Retarded Seepage Velocity} = (\vec{q} / n_e) / R_d$$

$$K_d = \text{Distribution coefficient}$$

The solution of Eq. 7, subject to initial and boundary conditions of Eqs. (2) through (5), is

$$\begin{aligned} C(x, y, z, t) &= \int_0^t \int_R \frac{\dot{M}}{n_e R_d} G dR_0 d\tau + \int_R (G C_i)_{\tau=0} dR_0 \\ &- \int_0^t \int_{S_1} \bar{\bar{K}} \cdot \nabla G \cdot \vec{n} C_1 dS_0 d\tau - \int_0^t \int_{S_2} \frac{G q_2}{n_e R_d} dS_0 d\tau \\ &- \int_0^t \int_{S_3} \frac{G q_3}{n_e R_d} dS_0 d\tau \end{aligned} \quad (8)$$

if $G(x, y, z, t; \xi, \eta, \zeta, \tau)$ satisfies the following conditions:

$$\lim_{t \rightarrow \tau} G = \delta(x - \xi) \delta(y - \eta) \delta(z - \zeta) \quad (9a)$$

$$t > \tau$$

$$G = 0 \quad \text{for } t < \tau \quad (9b)$$

$$G = 0 \quad \text{on } S_1 \quad (10)$$

$$(n_e \bar{\bar{D}} \cdot \nabla_0 G + \vec{q} G) \cdot \vec{n} = 0 \quad \text{on } S_2 \quad (11)$$

$$n_e \bar{\bar{D}} \cdot \nabla_0 G \cdot \vec{n} = 0 \quad \text{on } S_3 \quad (12)$$

$$-\bar{\bar{D}} \cdot \nabla G \cdot \vec{n} + K_e^* G = D \quad \text{on } S_4 \quad (13)$$

and

$$-\frac{\partial G}{\partial \tau} = V_0 \cdot (\bar{K} \cdot \nabla_0 G) + U \cdot \nabla G - \left(\frac{K}{R_d} + \lambda \right) G \quad \text{for } t > \tau , \quad (14)$$

where δ is the Dirac Delta function. The subscript, "0", in Eqs. (8) through (14) refers to the operation with respect to ξ , η , ζ rather than x , y , z . Eq. (8) expresses the spatio-temporal distribution of the contaminant in terms of the source/sink, M , the initial condition, C_0 , the boundary conditions, C_1 , q_2 , and q_3 , and Green's function, G . If G is known, the problem is solved. Thus, we have effectively reduced the initial-boundary value problem of Eqs. (2) through (6) to a homogeneous problem of Eqs. (9a) through (14).

It can be shown that for simple geometry such as separable coordinate system, Green's function, G , can be expressed as:

$$G(x,y,z,t;\xi,\eta,\zeta,\tau) = G_1(x,t;\xi,\tau) G_2(y,t;\eta,\tau) G_3(z,t;\zeta,\tau) \quad (15)$$

The derivation of G_1 , G_2 , and G_3 can be found elsewhere (Yeh and Tsai 1976). If we further assume that no waste can flow across the impervious boundaries and the flows through open boundaries are located at infinity, then we obtain $C_1 = 0$, $q_2 = 0$, and $q_3 = 0$. Under this circumstance, Eq. (8) is reduced to:

for continuous source or finite duration release and $t < T$

$$C(x,y,z,t) = \int_0^t \frac{M}{n_e R_d} F_{ijk}(x,y,z,t;\tau) d\tau \quad (16a)$$

for finite duration source and $t > T$

$$= \int_0^T \frac{M}{n_e R_d} F_{ijk}(x,y,z,t;\tau) d\tau \quad (16b)$$

for instantaneous source

$$= \frac{M}{n_e R_d} F_{ijk}(x, y, z, t; \tau) , \quad (16c)$$

where F_{ijk} is the integral of Green's function, G , over the source space; M is the instantaneous release of total mass; and T is the duration of waste release. F_{ijk} is given by:

$$F_{ijk} = X_i Y_j Z_k , \quad (17)$$

where $i = 1$ or 2 , $j = 1, 2, 3$, or 4 , and $k = 1, 2, 3$, or 4 . Functions X_i , Y_j , and Z_k are given by Eqs. (18) through (27) for three-dimensional cases as follows:

for point source in the x -direction:

$$X_1 = \frac{1}{\sqrt{4\pi K_{xx}(t-\tau)}} \exp \left[- \frac{(x-x_s) - U(t-\tau)}{4K_{xx}(t-\tau)} - \left(\frac{K}{R_d} + \lambda \right)(t-\tau) \right] \quad (18)$$

for line source in the x -direction:

$$X_2 = \frac{1}{2} \left\{ \operatorname{erf} \left(\frac{x-L_1 - U(t-\tau)}{\sqrt{4K_{xx}(t-\tau)}} \right) - \operatorname{erf} \left(\frac{x-L_2 - U(t-\tau)}{\sqrt{4K_{xx}(t-\tau)}} \right) \right\} \cdot \exp \left[- \left(\frac{K}{R_d} + \lambda \right)(t-\tau) \right] \quad (19)$$

for finite width and point source in the y -direction:

$$Y_1 = \frac{1}{B} + \frac{2}{B} \sum_{i=1}^{\infty} \cos \left(\frac{i\pi y}{B} \right) \cdot \cos \left(\frac{i\pi y_s}{B} \right) \cdot \exp \left[- \left(\frac{i\pi}{B} \right)^2 K_{yy}(t-\tau) \right] \quad (20)$$

for finite width and line source in the y -direction:

$$Y_2 = \frac{B_2 - B_1}{B} + \frac{2}{B} \sum_{i=1}^{\infty} \cos \left(\frac{i\pi y}{B} \right) \cdot \frac{B}{i\pi} \left\{ \sin \left(\frac{i\pi B_2}{B} \right) - \sin \left(\frac{i\pi B_1}{B} \right) \right\} \\ \exp \left[- \left(\frac{i\pi}{B} \right)^2 K_{yy}(t-\tau) \right] \quad (21)$$

for infinite width and point source in the y-direction:

$$\gamma_3 = \frac{1}{\sqrt{4\pi K_{yy}(t-\tau)}} \exp \left[-\frac{(y-y_s)}{4K_{yy}(t-\tau)} \right] \quad (22)$$

for infinite width and line source in the y-direction:

$$\gamma_4 = \frac{1}{2} \left\{ \operatorname{erf} \left(\frac{y-B_1}{\sqrt{4K_{yy}(t-\tau)}} \right) - \operatorname{erf} \left(\frac{y-B_2}{\sqrt{4K_{yy}(t-\tau)}} \right) \right\} \quad (23)$$

for finite depth and point source in the z-direction:

$$z_1 = \sum_{i=1}^{\infty} \psi_i(z) \psi_i(z_s) \cdot \exp \left[-\kappa_i^2 K_{zz}(t-\tau) \right] \quad (24)$$

for finite depth and line source in the z-direction:

$$z_2 = \sum_{i=1}^{\infty} \psi_i(z) \left(\frac{a_i}{\kappa_i} \right) \left\{ \sin(\kappa_i H_2) - \sin(\kappa_i H_1) - \frac{K_e^*}{K_{zz} \kappa_i} [\cos(\kappa_i H_2) - \cos(\kappa_i H_1)] \right\} \cdot \exp \left[-\kappa_i^2 K_{zz}(t-\tau) \right] \quad (25)$$

for infinite depth and point source in the z-direction:

$$z_3 = \frac{1}{\sqrt{4\pi K_{zz}(t-\tau)}} \left\{ \exp \left[-\frac{(z-z_s)^2}{4K_{zz}(t-\tau)} \right] + \exp \left[-\frac{(z+z_s)^2}{4K_{zz}(t-\tau)} \right] \right\} \\ - \frac{K_e^*}{K_{zz}} \exp [K_{zz} (\frac{K_e^*}{K_{zz}})^2 (t-\tau) + (\frac{K_e^*}{K_{zz}}) (z+z_s)] \cdot \\ \operatorname{erfc} \left[\frac{z+z_s}{\sqrt{4K_{zz}(t-\tau)}} + \frac{K_e^*}{K_{zz}} \sqrt{K_{zz}(t-\tau)} \right] \quad (26)$$

for infinite depth and line source in the z-direction:

$$\begin{aligned}
 Z_4 = & \frac{1}{2} \left\{ \operatorname{erf} \left[\frac{z+H_2}{\sqrt{4K_{zz}(t-\tau)}} \right] - \operatorname{erf} \left[\frac{z+H_1}{\sqrt{4K_{zz}(t-\tau)}} \right] + \operatorname{erf} \left[\frac{z-H_2}{\sqrt{4K_{zz}(t-\tau)}} \right] \right. \\
 & \left. + \operatorname{erf} \left[\frac{z-H_1}{\sqrt{4K_{zz}(t-\tau)}} \right] \right\} + \exp \left[K_{zz} \left(\frac{K_e^*}{K_{zz}} \right)^2 (t-\tau) \right] \cdot \\
 & \left\{ \exp \left[\left(\frac{K_e^*}{K_{zz}} \right) (z+H_2) \right] \cdot \operatorname{erfc} \left[\frac{z+H_2}{\sqrt{4K_{zz}(t-\tau)}} + \left(\frac{K_e^*}{K_{zz}} \right) \sqrt{K_{zz}(t-\tau)} \right] \right. \quad (27) \\
 & \left. - \exp \left[\left(\frac{K_e^*}{K_{zz}} \right) (z+H_1) \right] \cdot \operatorname{erfc} \left[\frac{z+H_1}{\sqrt{4K_{zz}(t-\tau)}} + \left(\frac{K_e^*}{K_{zz}} \right) \sqrt{K_{zz}(t-\tau)} \right] \right\} \\
 & - \left\{ \operatorname{erf} \left[\frac{z+H_2}{\sqrt{4K_{zz}(t-\tau)}} \right] - \operatorname{erf} \left[\frac{z+H_1}{\sqrt{4K_{zz}(t-\tau)}} \right] \right\}
 \end{aligned}$$

where B and H are the width and depth of the aquifer; L_1 , B_1 , H_1 and L_2 , B_2 , H_2 are the beginning x, y, z and the ending x, y, z coordinates of the source; x_s , y_s , and z_s are the x, y, and z coordinates of the point source. In Eqs. (24) and (25), $\psi_i(z)$ denotes the function:

$$\psi_i(z) = a_i \left\{ \cos(\kappa_i z) + \frac{K_e^*}{K_{zz} \kappa_i} \sin(\kappa_i z) \right\}, \quad (28)$$

where κ_i and a_i are given by the following equations:

$$\tan(\kappa_i H) = \frac{K_e^*}{K_{zz} \kappa_i} \quad (29)$$

and

$$a_i^2 = \frac{2}{H \{ 1 + (K_e^*/K_{zz}) \kappa_i \}^2 + (K_e^*/K_{zz}) \chi_i} \quad . \quad (30)$$

To apply the above equations to two-dimensional cases in the x-y plane, one has to set $Z_k = 1$ ($k = 1, 2, \dots, 4$). Similarly for the two-dimensional cases in the x-z plane, one has to set $Y_j = 1$ ($j = 1, 2, \dots, 4$) and for the one dimensional cases, say x-direction, one simply sets both Y_j and Z_k equal to 1.

In practical computation, Eqs. (20) and (21) often converge very slowly when $K_{yy}(t-\tau)/B^2$ is small. Under such circumstances, the following equations, which are obtained by the method of image, are used:

$$Y_1 = \frac{1}{\sqrt{4 K_y(t-\tau)}} \left\{ \sum_{n=0}^{\infty} \exp \left[- \frac{(y - y_s - 2nB)^2}{4K_{yy}(t-\tau)} \right] + \sum_{n=0}^{\infty} \exp \left[- \frac{(y - y_s - 2(n-1)B)^2}{4K_{yy}(t-\tau)} \right] \right. \\ \left. + \sum_{n=0}^{\infty} \exp \left[- \frac{(y + y_s - 2(n+1)B)^2}{4K_{yy}(t-\tau)} \right] + \sum_{n=0}^{\infty} \exp \left[- \frac{(y + y_s - 2nB)^2}{4K_{yy}(t-\tau)} \right] \right\} \quad (31)$$

$$\begin{aligned}
 Y_2 = & \frac{1}{2} \sum_{n=0}^{\infty} \left\{ \operatorname{erf} \left[\frac{(y-B_1)-2nB}{\sqrt{4K_{yy}(t-\tau)}} \right] - \operatorname{erf} \left[\frac{(y-B_2)-2nB}{\sqrt{4K_{yy}(t-\tau)}} \right] \right. \\
 & + \operatorname{erf} \left[\frac{y-B_1-2(n-1)B}{\sqrt{4K_{yy}(t-\tau)}} \right] - \operatorname{erf} \left[\frac{y-B_2-2(n-1)B}{\sqrt{4K_{yy}(t-\tau)}} \right] \\
 & + \operatorname{erf} \left[\frac{y+B_2-2(n+1)B}{\sqrt{4K_{yy}(t-\tau)}} \right] - \operatorname{erf} \left[\frac{y+B_1-2(n+1)B}{\sqrt{4K_{yy}(t-\tau)}} \right] \\
 & \left. + \operatorname{erf} \left[\frac{y+B_2-2nB}{\sqrt{4K_{yy}(t-\tau)}} \right] - \operatorname{erf} \left[\frac{y+B_1-2nB}{\sqrt{4K_{yy}(t-\tau)}} \right] \right\}
 \end{aligned} \tag{32}$$

It is seen that 32 equations may be obtained for the spatial integral of Green's function, F_{ijk} . These are F_{111} , F_{112} , ... and F_{244} . Substitution of each of those 32 equations into Eqs. (16a), (16b), and (16c) would yield 96 equations. Since each equation is applicable to any of three wastes, there would be 288 options when all three spatial dimensions are considered. Careful adoption of source distribution and media size would yield 72 two-dimensional options each in the x-y plane and x-z plane, respectively, and 18 options for the one-dimensional along the longitudinal direction. AT123D computer code is developed to perform the integration of Eqs. (16a), (16b) and (16c).

IV. PARAMETER SPECIFICATIONS

The applications of AT123D to practical problems require: (a) the geometry of the region of interest; (b) the dispersion coefficient tensor, \hat{K} , characterized by its components, K_{xx} , K_{yy} , K_{zz} ; (c) the soil properties, n_e , ρ_b , and the hydraulic conductivity, K_h ; (d) the source/sink strength and configuration, M , and x_s , y_s , z_s , or L_1 , L_2 , B_1 , B_2 , H_1 , and H_2 ; (e) the parameter representing the waste-soil interaction, K_d ; and (f) the pressure field of the flow and the decay constant, λ . Among these inputs, K_{xx} , K_{yy} , and K_{zz} are perhaps the most difficult ones to determine. No effective way is currently practical to measure these coefficients in the field because of the aquifer inhomogeneities (Bredehoft and Pinder 1973, Robertson 1974). Tensor analysis indicates that they would be a linear function of the groundwater velocity (Bear 1972). For our case, we may write:

$$K_{xx} = \alpha_L U; K_{yy} = \alpha_T U; K_{zz} = \alpha_V U , \quad (18)$$

where α_L , α_T and α_V are the longitudinal, transverse, and vertical dispersivities, respectively. The distribution coefficient, K_d , should be determined by batch test or column test. The decay constant, λ , is a function of radwastes. The pressure field, which may be obtained either by numerical simulation of flow equation or by field mapping of well data, and hydraulic conductivity are used to compute the velocity.

Typical values of the effective porosity, hydraulic conductivity, and the dispersivities for sand, silt, and clay are listed in Table 1 (Eagleson 1970, Bredehoeft and Pinder 1973, Robertson 1974). These values are intended to provide guidelines for these parameters. For actual application, soil measurements should be made to determine the effective porosity and hydraulic conductivity. Dispersivities should be obtained by calibration against field data (Robertson 1974) or they may be extrapolated from values that have been calibrated from similar aquifer system. Based on the field experimental results, the dispersivity varies with aquifer materials, the more permeable an aquifer, the higher the dispersivity. Thus, the values of α_L , α_T , and α_V may be modified by the permeability factor from the calibrated values.

Table 1. Typical values of effective porosity, hydraulic conductivity, dispersivity, and bulk density

	Sand	Silt	Clay
Effective porosity, n_e	0.1 ~ 0.3	0.05 ~ 0.1	0.03 ~ 0.05
Hydraulic conductivity K_h (cm/sec)	$10 \sim 10^{-2}$	$10^{-3} \sim 10^{-4}$	$10^{-5} \sim 10^{-6}$
Longitudinal dispersivity a_L (m)	$10 \sim 100$	$1 \sim 10$	$0.1 \sim 1.0$
Transverse dispersivity a_T (m)	$1 \sim 10$	$0.1 \sim 1.0$	$0.01 \sim 0.1$
Vertical dispersivity a_V (m)	$1 \sim 10$	$0.1 \sim 1.0$	$0.01 \sim 0.1$
Bulk density, ρ_b gram/cm ³	$1.18 \sim 1.58$	$1.29 \sim 1.8$	$1.4 \sim 2.2$

V. SAMPLE PROBLEM

To illustrate the application of AT123D code, radwaste will be assumed to be released into an aquifer system continuously. For simplicity, the release rate will be assumed constant, although the code takes care of the time-dependent rate. Thirty-two (32) sample problems are performed for the three-dimensional application. In addition, 8 sample problems each for the two-dimensional cases in the x-y and x-z planes, respectively, and two sample problems for the one-dimensional case in the longitudinal direction are illustrated. These fifty cases are listed in Table 2. Inputs of these sample problems are given in Appendix B. Output of four sample cases are also included in Appendix B. Output of all fifty cases are given in the microfiche which is attached in the inside page of the back cover. Preparation of input data is given in Appendix A and a listing of FORTRAN source program is given in Appendix C.

For the sample problems, porosity, n_e , of the aquifer is assumed to be 0.2. The hydraulic conductivity, K_h , is assumed to be 0.5 m hr^{-1} . A hydraulic gradient of 0.05 is assumed along the longitudinal direction which results in a velocity of 0.025 m hr^{-1} . Typical values of longitudinal, transverse, and vertical dispersivities, α_L , α_T , and α_y , are assumed to be 30.0, 5.0, and 5.0 meters, respectively for silty sand. A distribution coefficient, K_d , of $10 \text{ cm}^3/\text{gram}$ is used to represent the absorption of strontium in the silty sand. Bulk density, ρ_b of the soil is assumed to be 1.4 gram/cm^3 . Decay constant, λ , of $2.83 \times 10^{-6} \text{ hr}^{-1}$ is used. This decay constant is equivalent to a half life of 28 years. The source location is at $(x_s, y_s, z_s) = (0, 10, 1)$ in the example of point source.

Table 2. List of sample problems

Sample problem case	Aquifer geometry				Source configuration					
	FW	IW	FD	ID	PS	LS	PS	LS	PS	LS
1	X		X		X		X		X	
2	X		X			X	X		X	
3	X		X		X			X	X	
4	X		X		X		X			X
5	X		X		X			X		X
6	X		X			X	X			X
7	X		X			X		X	X	
8	X		X			X		X		X
9	X			X	X		X		X	
10	X			X		X	X		X	
11	X			X	X			X	X	
12	X			X	X		X			X
13	X			X	X			X		X
14	X			X		X	X			X
15	X			X		X		X	X	
16	X			X		X		X		X
17		X	X		X		X		X	
18	X	X				X	X		X	
19	X	X			X			X	X	
20	X	X			X		X			X
21	X	X			X			X		X
22	X	X				X	X			X
23	X	X				X		X	X	
24	X	X				X		X		X
25	X			X	X		X		X	
26	X			X		X	X		X	
27	X			X	X			X	X	
28	X			X	X		X			X
29	X			X	X			X		X
30	X			X		X	X			X
31	X			X		X		X	X	
32	X			X		X		X		X
33	X		X		X		X			X
34	X		X			X	X			X
35	X		X		X			X		X
36	X		X			X		X		X
37		X	X		X		X			X
38	X	X				X	X			X
39	X	X			X			X		X
40	X	X				X		X		X
41	X	X			X			X	X	
42	X	X				X		X	X	
43	X	X			X			X		X
44	X	X				X		X		X
45	X			X	X			X	X	
46	X			X		X		X	X	
47	X			X	X			X		X
48	X			X		X		X		X
49	X		X		X			X		X
50	X		X			X		X		X

FW = finite width, IW = infinite width, FD = finite depth, ID = infinite depth,
 PS = point source, LS = line source.

In the example of volume source, the following source dimensions are used: $L_1 = 0.0$ meter, $L_2 = 5.0$ meter, $B_1 = 0.0$ meter, $B_2 = 20.0$ meters, $H_1 = 0.0$ meters and $H_2 = 2.0$ meters. When the finite width is used, a width of $B = 200$ meters is assumed. If the finite depth option is used, a depth of $H = 10$ meters is assumed. These source dimensions are shown in Fig. 2.

It should be noted that if the code is applied for a two-dimensional problem in the x-y plane (sample cases 33-40), one has to input $H_1 = 0$ and $H_2 = H$. Similarly, if the model is employed for a two-dimensional problem in the x-z plane (sample cases 41-48), one just uses input $B_1 = 0$ and $B_2 = B$. For the reduction to one-dimensional problem in the longitudinal direction (sample cases 49 and 50), one has to input $B_1 = 0$ and $B_2 = B$ as well as $H_1 = 0$ and $H_2 = H$.

The following sample cases are intended to illustrate the effect of source configurations and sizes of the media on the distribution of the radionuclides. Sample case no. 1 in Appendix B presents the concentration distribution as a result of the continuous release of radwaste with a rate of 1.0 Ci/hr and lasting for 240 hours. A point source configuration is assumed and it is discharged into a three-dimensional media with finite depth and finite width. Initially, the media is clean and the concentration at time = 0 hour is zero everywhere. At the end of 1224 hours, the concentration at the point $(x,y,z) = (10,10,2)$ is 33300 pCi/liter. At the point $(x,y,z) = (60,10,2)$, the concentration has decreased to 0.0269 pCi/liter. Had

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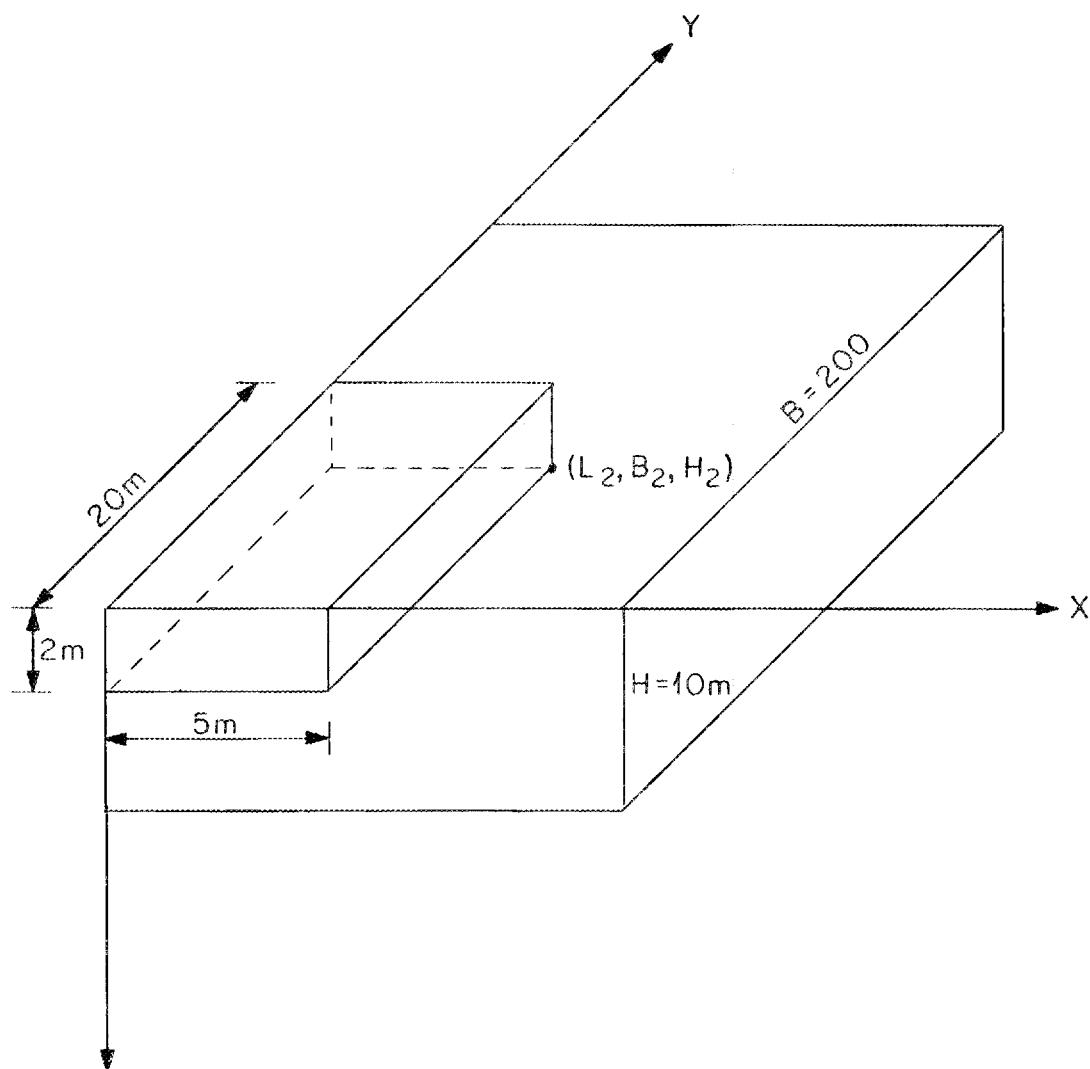


Fig. 2. Schematization of source dimensions and the medium.

the dispersion not been included, the concentration at both points would have been zero since the retarded velocity is 0.176×10^{-2} m/hr, thus the mean front of the waste has traveled only to $x = 2.16$ m at the end of 1224 hours. It should be pointed out that at the end of 1224 hours, the decay mechanism would not significantly attenuate the concentration because the half life of 28 years is relatively much longer than the simulation time.

Sample case no. 39 shows the concentration distribution of 240 hour continuous release with a rate of 1.0 Ci/hr. A line source configuration parallel to y-direction is assumed and it is discharged into the two-dimensional media in the x-y plane. At the end of 1224 hours, the concentration at points, $(x,y,z) = (10,10,2)$ and $(x,y,z) = (60,10,2)$, are 2310 pCi/liter and 0.0023 pCi/liter, respectively. These values are smaller than those in the above sample case because complete mixing is assumed in the vertical direction. It is noted that the concentration distribution in the vertical direction is uniform as expected. For example, the x-y distribution of the concentration on $z = 2$ m is identical to that on $z = 4$ m.

Sample case no. 48 illustrates the distribution as a result of continuous release into the two-dimensional media in the x-z plane. The release configuration is assumed to be an area source. At the end of 1224 hours, the concentration at points, $(x,y,z) = (10,10,2)$ and $(x,y,z) = (60,10,2)$, are 657.0 pCi/liter and 0.00218 pCi/liter, respectively. Finally, sample case no. 50 shows the concentration distribution resulting from a volume release into a one-dimensional media in the x-direction. As expected, the concentration in the y- and z-directions are uniform.

VI. NOTATION

a_i	A coefficient defined by Eq. (30)
B	Width of the aquifer
B_1	Beginning coordinate of the source in the y -direction
B_2	Ending coordinate of the source in the y -direction
C	Concentration
C_i	Initial concentration
C_1	Concentration on the boundary S_1
C_s	Absorbed concentration in the solid grain
D	Dispersion tension
FD	Finite depth
F_{ijk}	A function defined by Eq. (17)
FW	Finite width
g	gravity
G	Green's function
G_1	Subgreen's function
G_2	Subgreen's function
G_3	Subgreen's function
H	Depth of the aquifer
H_1	Beginning coordinate of the source in the z -direction
H_2	Ending coordinate of the source in the z -direction
ID	Infinity deep
IW	Infinity wide
K	Chemical degeneration rate
K_e^*	Modified heat exchange coefficient

K_d	Distribution coefficient
\bar{K}	Retarded dispersion tensor
K_{xx}	x-component of the retarded dispersion tensor
K_{yy}	y-component of the retarded dispersion tensor
K_{zz}	z-component of the retarded dispersion tensor
L_1	Beginning coordinate of the source in the x-direction
L_2	Ending coordinate of the source in the x-direction
LS	Line source
M	Source rate
M	Total source
n_e	Porosity
\hat{n}	An outward unit vector normal to a surface
PS	Point source
\vec{q}	Darcy's velocity vector
q_2	Flux through boundary S_2
q_3	Flux through boundary S_3
R	A region with respect to x, y, z
R_d	Retardation factor
R_o	A region with respect to ξ, η, ζ
S	The boundary of R
S_1	Part of S
S_2	Part of S
S_3	Part of S
S_4	Part of S
t	Time

\hat{U}	Retarded velocity vector
U	The magnitude of \hat{U}
x	Longitudinal coordinate
x_s	x -coordinate of a point source
X_j	Either function X_1 or X_2
X_1	A function defined by Eq. (18)
X_2	A function defined by Eq. (19)
y	Transfer coordinate
y_s	y -coordinate of a point source
Y_j	Either function Y_1 , Y_2 , Y_3 , Y_4
Y_1	A function defined by Eq. (20)
Y_2	A function defined by Eq. (21)
Y_3	A function defined by Eq. (22)
Y_4	A function defined by Eq. (23)
z	Vertical coordinate
z_s	z -coordinate of a point source
Z_k	k -th Z -function
Z_1	A function defined by Eq. (24)
Z_2	A function defined by Eq. (25)
Z_3	A function defined by Eq. (26)
Z_4	A function defined by Eq. (27)
α_L	Longitudinal dispersivity
α_T	Transverse dispersivity
α_V	Vertical dispersivity
∇	Del operator with respect to x , y , z
∇_0	Del operator with respect to ξ , v , ζ

λ	Decay constant
ρ_b	Bulk density
τ	Time
ξ	Longitudinal coordinate
η	Transverse coordinate
ζ	Vertical coordinate
κ_i	i-th eigenvalue defined by Eq. (29)
ψ_i	i-th eigenfunction defined by Eq. (28)

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APPENDIX A
DATA INPUT GUIDE

1. TITLE: Format (20A4) one card per problem

TITLE								
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TITLE = Array for the title of the problem. It may contain up to 80 characters.

2. Basic Integer Parameters: Format (16I5) one card

NX	NY	NZ	NROOT	NBGTI	NEDTI	NPRINT	INSTAN
5	10	15	20	25	30	35	40

NSOUS	INTER	ICASE	IDEP	IWID	IBUG		
45	50	55	60	65	70	75	80

- NX = Number of points in the x-direction where the solution is desired.
 NY = Number of points in the y-direction where the solution is desired.
 NZ = Number of points in the z-direction where the solution is desired.
 NROOT = Number of eigenvalues required for series evaluation.
 NBGTI = Number of beginning time in terms of DT when the solution is desired.
 NEDTI = Number of ending time in terms of DT when the solution is desired.
 NPRINT = An integer parameter indicating that for every NPRINT time steps the solution is desired
 INSTAN = An integer parameter indicating if the release is an instantaneous release or not; = 0 instantaneous release, = 1 continuous release.
 NSOUS = An integer parameter indicating if the source is constant or changing with time: = 0 constant source, ≠ 0 NSOUS data points as function of time are required.
 INTER = An integer parameter indicating if intermittent solutions between NBGTI and NEDTI are to be line-printed: = 0 No, = 1 yes

ICASE = An integer parameter indicating what type of waste is being simulated: = 1 for heat, = 2 for chemical, = 3 for radwaste.
 IWID = An integer parameter indicating if the media is infinity or not in the y-direction; = 0 yes, = 1 no.
 IDEP = An integer parameter indicating if the aquifer is infinitely deep: = 0 yes, = 1 no.
 IBUG = An integer parameter indicating if the diagnostic check is desired or not: = 0 no, = 1 yes. For debugging, IBUG is normally set to 1. For production, IBUG is normally set to zero.

3. Aquifer Size and Source Size: Format (8F10.0)

DEPTH	WIDTH	RL1	RL2	RB1	RB2	RH1	RH2
10	20	30	40	50	60	70	80

DEPTH = Aquifer depth, (L)
 WIDTH = Aquifer width, (L)
 RL1 = Beginning coordinate of the source in the x-direction, (L)
 RL2 = Ending coordinate of the source in the x-direction, (L)
 RB1 = Beginning coordinate of the source in the y-direction, (L)
 RB2 = Ending coordinate of the source in the y-direction, (L)
 RH1 = Beginning coordinate of the source in the z-direction, (L)
 RH2 = Ending coordinate of the source in the z-direction, (L)

4. Soil and Waste Properties: Format (8F10.0)

POR	HCOND	HGRAD	AELONG	ATRANV	AVERTI	AKD	AKE
10	20	30	40	50	60	70	80

POR = Porosity of the soil

HCOND = Hydraulic conductivity, (LT^{-1})

HGRAD = Hydraulic gradient
 AELONG = Longitudinal dispersivity, (L)
 ATRANV = Transverse dispersivity, (L)
 AVERTI = Vertical dispersivity, (L)
 AKD = Distribution coefficient, ($L^3 M^{-1}$)
 AKE = Modified heat exchange coefficient, ($L T^{-1}$)

5. More soil and waste properties and some real number parameters:
FORMAT (8F10.0)

AMTAU	RAMADA	RHOB	RHOW	ACCU	DT	TDISP	Q
10	20	30	40	50	60	70	80

AMTAU = Molecular diffusion coefficient, ($L^2 T^{-1}$)
 RAMADA = Decay constant (T^{-1})
 RHOB = Bulk density of the soil, ($M L^{-3}$)
 RHOW = Density of water, ($M L^{-3}$)
 ACCU = Error tolerance if steady-state solution is desired
 DT = Time step size for which the solution is desired, (T)
 TDISP = Time duration of waste release, (T)
 Q = Constant waste release rate or total instantaneous release, ($M T^{-1}$)

6. X-SPACE Coordinate: Format (8F10.0)

Number of cards depend on NX: READ (XDIM(I), I = 1, NX).

XDIM(1)	XDIM(2)	---	---	---	---	---	---
10	20	30	40	50	60	70	80

XDIM(I) = x-coordinate of I-th point in the x-direction, where the solution is desired, (L)

7. Y-Space Coordinate: FORMAT (8F10.0)

Number of cards depend on NY: READ (YDIM(I), I = 1, NY).

YDIM(1)	YDIM(2)	---	---	---	---	---	---	---
10	20	30	40	50	60	70	80	

YDIM(I) = y-coordinate of I-th point in the y-direction where the solution is desired, (L)

8. Z-Space Coordinate: FORMAT (8F10.0)

Number of cards depends on NZ: READ (ZDIM(I), I = 1, NZ).

ZDIM(1)	ZDIM(2)	---	---	---	---	---	---	---
10	20	30	40	50	60	70	80	

ZDIM(I) = z-coordinate of the I-th point in the z-direction where the solution is desired, (L)

9. Variably Source Release Rate: FORMAT (8F10.0)

The number of cards depends on NSORS. This group of cards is required only if NSORS > 0. READ (QS(I), I = 1, NSORS).

QS(1)	QS(2)	---	---	---	---	---	---	---
10	20	30	40	50	60	70	80	

QS(1) = waste release rate at time = (I-1)*DT, (MT⁻¹)

APPENDIX B
INPUT AND OUTPUT OF SAMPLE CASES

APPENDIX B

INPUT AND OUTPUT OF SAMPLE CASES

B.1 INPUT DATA OF ALL FIFTY CASES

RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 1											
6	2	1000	101	103	1	1	0	1	3	1	1
10.0		200.0	0.0	0.0		10.0		10.0		1.0	1.0
0.2		0.5	0.05	30.0		5.0		5.0		0.01	0.0
0.0		0.00000283	1400.0	1000.0		0.001		12.0		240.0	1.0
10.0		20.0	30.0	40.0		50.0		60.0		70.0	80.0
0.0		5.0	10.0	15.0		20.0		25.0			
2.0		4.0									
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 2											
6	2	1000	101	103	1	1	0	1	3	1	1
10.0		200.0	0.0	0.0	5.0	10.0		10.0		1.0	1.0
0.2		0.5	0.05	30.0		5.0		5.0		0.01	0.0
0.0		0.00000283	1400.0	1000.0		0.001		12.0		240.0	1.0
10.0		20.0	30.0	40.0		50.0		60.0		70.0	80.0
0.0		5.0	10.0	15.0		20.0		25.0			
2.0		4.0									
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 3											
6	2	1000	101	103	1	1	0	1	3	1	1
10.0		200.0	0.0	0.0	0.0	0.0		20.0		1.0	1.0
0.2		0.5	0.05	30.0		5.0		5.0		0.01	0.0
0.0		0.00000283	1400.0	1000.0		0.001		12.0		240.0	1.0
10.0		20.0	30.0	40.0		50.0		60.0		70.0	80.0
0.0		5.0	10.0	15.0		20.0		25.0			
2.0		4.0									
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 4											
6	2	1000	101	103	1	1	0	1	3	1	1
10.0		200.0	0.0	0.0	0.0	10.0		10.0		0.0	2.0
0.2		0.5	0.05	30.0		5.0		5.0		0.01	0.0
0.0		0.00000283	1400.0	1000.0		0.001		12.0		240.0	1.0
10.0		20.0	30.0	40.0		50.0		60.0		70.0	80.0
0.0		5.0	10.0	15.0		20.0		25.0			
2.0		4.0									
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 5											
6	2	1000	101	103	1	1	0	1	3	1	1
10.0		200.0	0.0	0.0	0.0	0.0		20.0		0.0	2.0
0.2		0.5	0.05	30.0		5.0		5.0		0.01	0.0
0.0		0.00000283	1400.0	1000.0		0.001		12.0		240.0	1.0
10.0		20.0	30.0	40.0		50.0		60.0		70.0	80.0
0.0		5.0	10.0	15.0		20.0		25.0			
2.0		4.0									
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 6											
6	2	1000	101	103	1	1	0	1	3	1	1
10.0		200.0	0.0	0.0	5.0	10.0		10.0		0.0	2.0
0.2		0.5	0.05	30.0		5.0		5.0		0.01	0.0
0.0		0.00000283	1400.0	1000.0		0.001		12.0		240.0	1.0
10.0		20.0	30.0	40.0		50.0		60.0		70.0	80.0
0.0		5.0	10.0	15.0		20.0		25.0			
2.0		4.0									
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 7											
6	2	1000	101	103	1	1	0	1	3	1	1

B.1 INPUT DATA OF ALL FIFTY CASES (continued)

10.0	200.0	0.0	5.0	0.0	20.0	1.0	1.0	CARD 051
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 052
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 053
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 054
0.0	5.0	10.0	15.0	20.0	25.0			CARD 055
2.0	4.0							CARD 056
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 8								
6	2 1000	101 103	1 1 0	1 3 1 1				CARD 057
10.0	200.0	0.0	5.0	0.0	20.0	0.0	2.0	CARD 058
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 059
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 060
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 061
0.0	5.0	10.0	15.0	20.0	25.0			CARD 062
2.0	4.0							CARD 063
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 9								
6	2 1000	101 103	1 1 0	1 3 1 0				CARD 064
10.0	200.0	0.0	5.0	10.0	10.0	1.0	1.0	CARD 065
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 066
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 067
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 068
0.0	5.0	10.0	15.0	20.0	25.0			CARD 069
2.0	4.0							CARD 070
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 10								
6	2 1000	101 103	1 1 0	1 3 1 0				CARD 071
10.0	200.0	0.0	5.0	10.0	10.0	1.0	1.0	CARD 072
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 073
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 074
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 075
0.0	5.0	10.0	15.0	20.0	25.0			CARD 076
2.0	4.0							CARD 077
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 11								
6	2 1000	101 103	1 1 0	1 3 1 0				CARD 078
10.0	200.0	0.0	5.0	0.0	20.0	1.0	1.0	CARD 079
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 080
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 081
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 082
0.0	5.0	10.0	15.0	20.0	25.0			CARD 083
2.0	4.0							CARD 084
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 12								
6	2 1000	101 103	1 1 0	1 3 1 0				CARD 085
10.0	200.0	0.0	5.0	10.0	10.0	0.0	2.0	CARD 086
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 087
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 088
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 089
0.0	5.0	10.0	15.0	20.0	25.0			CARD 090
2.0	4.0							CARD 091
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 13								
6	2 1000	101 103	1 1 0	1 3 1 0				CARD 092
10.0	200.0	0.0	5.0	0.0	20.0	0.0	2.0	CARD 093
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 094
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 095
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 096
0.0	5.0	10.0	15.0	20.0	25.0			CARD 097
2.0	4.0							CARD 098
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 14								
6	2 1000	101 103	1 1 0	1 3 1 0				CARD 099
10.0	200.0	0.0	5.0	0.0	20.0	0.0	2.0	CARD 100
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	

B.1 INPUT DATA OF ALL FIFTY CASES (continued)

0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 101
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 102
0.0	5.0	10.0	15.0	20.0	25.0			CARD 103
2.0	4.0							CARD 104
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 14								CARD 105
6	2 1000 101 103 1 1 0 1 3 1 0							CARD 106
10.0	200.0	0.0	5.0	10.0	10.0	0.0	2.0	CARD 107
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 108
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 109
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 110
0.0	5.0	10.0	15.0	20.0	25.0			CARD 111
2.0	4.0							CARD 112
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 15								CARD 113
6	2 1000 101 103 1 1 0 1 3 1 0							CARD 114
10.0	200.0	0.0	5.0	0.0	20.0	1.0	1.0	CARD 115
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 116
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 117
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 118
0.0	5.0	10.0	15.0	20.0	25.0			CARD 119
2.0	4.0							CARD 120
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 16								CARD 121
6	2 1000 101 103 1 1 0 1 3 1 0							CARD 122
10.0	200.0	0.0	5.0	0.0	20.0	0.0	2.0	CARD 123
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 124
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 125
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 126
0.0	5.0	10.0	15.0	20.0	25.0			CARD 127
2.0	4.0							CARD 128
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 17								CARD 129
6	2 1000 101 103 1 1 0 1 3 0 1							CARD 130
10.0	200.0	0.0	0.0	10.0	10.0	1.0	1.0	CARD 131
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 132
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 133
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 134
0.0	5.0	10.0	15.0	20.0	25.0			CARD 135
2.0	4.0							CARD 136
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 18								CARD 137
6	2 1000 101 103 1 1 0 1 3 0 1							CARD 138
10.0	200.0	0.0	5.0	10.0	10.0	1.0	1.0	CARD 139
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 140
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 141
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 142
0.0	5.0	10.0	15.0	20.0	25.0			CARD 143
2.0	4.0							CARD 144
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 19								CARD 145
6	2 1000 101 103 1 1 0 1 3 0 1							CARD 146
10.0	200.0	0.0	0.0	0.0	20.0	1.0	1.0	CARD 147
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 148
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 149
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 150

B.1 INPUT DATA OF ALL FIFTY CASES (continued)

0.0	5.0	10.0	15.0	20.0	25.0		CARD 151
2.0	4.0						CARD 152
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 20							CARD 153
10.0	5	2 1000 101 103	1	1 0	1 3	0 1	CARD 154
10.0	200.0	0.0	0.0	10.0	10.0	3.0	CARD 155
0.2	0.5	0.05	30.0	5.0	5.0	0.01	CARD 156
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	CARD 157
10.0	20.0	30.0	40.0	50.0	60.0	70.0	CARD 158
0.0	5.0	10.0	15.0	20.0	25.0		CARD 159
2.0	4.0						CARD 160
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 21							CARD 161
10.0	6	2 1000 101 103	1	1 0	1 3	0 1	CARD 162
10.0	200.0	0.0	0.0	20.0	3.0	2.0	CARD 163
0.2	0.5	0.05	30.0	5.0	5.0	0.01	CARD 164
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	CARD 165
10.0	20.0	30.0	40.0	50.0	60.0	70.0	CARD 166
0.0	5.0	10.0	15.0	20.0	25.0		CARD 167
2.0	4.0						CARD 168
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 22							CARD 169
10.0	6	2 1000 101 103	1	1 0	1 3	0 1	CARD 170
10.0	200.0	0.0	5.0	10.0	10.0	0.0	CARD 171
0.2	0.5	0.05	30.0	5.0	5.0	0.01	CARD 172
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	CARD 173
10.0	20.0	30.0	40.0	50.0	60.0	70.0	CARD 174
0.0	5.0	10.0	15.0	20.0	25.0		CARD 175
2.0	4.0						CARD 176
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 23							CARD 177
10.0	6	2 1000 101 103	1	1 0	1 3	0 1	CARD 178
10.0	200.0	0.0	5.0	0.0	20.0	1.0	CARD 179
0.2	0.5	0.05	30.0	5.0	5.0	0.01	CARD 180
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	CARD 181
10.0	20.0	30.0	40.0	50.0	60.0	70.0	CARD 182
0.0	5.0	10.0	15.0	20.0	25.0		CARD 183
2.0	4.0						CARD 184
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 24							CARD 185
10.0	6	2 1000 101 103	1	1 0	1 3	0 1	CARD 186
10.0	200.0	0.0	5.0	0.0	20.0	0.0	CARD 187
0.2	0.5	0.05	30.0	5.0	5.0	0.01	CARD 188
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	CARD 189
10.0	20.0	30.0	40.0	50.0	60.0	70.0	CARD 190
0.0	5.0	10.0	15.0	20.0	25.0		CARD 191
2.0	4.0						CARD 192
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 25							CARD 193
10.0	6	2 1000 101 103	1	1 0	1 3	0 0	CARD 194
10.0	200.0	0.0	0.0	10.0	10.0	1.0	CARD 195
0.2	0.5	0.05	30.0	5.0	5.0	0.01	CARD 196
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	CARD 197
10.0	20.0	30.0	40.0	50.0	60.0	70.0	CARD 198
0.0	5.0	10.0	15.0	20.0	25.0		CARD 199
2.0	4.0						CARD 200

B.1 INPUT DATA OF ALL FIFTY CASES (continued)

	RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 26											
6	2	1000	101	103	1	1	0	1	3	0	0	CARD 201
10.0	200.0	0.0	5.0	10.0	10.0	1.0	1.0					CARD 202
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0					CARD 203
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0					CARD 204
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0					CARD 205
0.0	5.0	10.0	15.0	20.0	25.0							CARD 206
2.0	4.0											CARD 207
	RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 27											
6	2	1000	101	103	1	1	0	1	3	0	0	CARD 208
10.0	200.0	0.0	0.0	0.0	20.0	1.0	1.0					CARD 209
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0					CARD 210
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0					CARD 211
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0					CARD 212
0.0	5.0	10.0	15.0	20.0	25.0							CARD 213
2.0	4.0											CARD 214
	RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 28											
6	2	1000	101	103	1	1	0	1	3	0	0	CARD 215
10.0	200.0	0.0	0.0	10.0	10.0	0.0	2.0					CARD 216
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0					CARD 217
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0					CARD 218
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0					CARD 219
0.0	5.0	10.0	15.0	20.0	25.0							CARD 220
2.0	4.0											CARD 221
	RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 29											
6	2	1000	101	103	1	1	0	1	3	0	0	CARD 222
10.0	200.0	0.0	0.0	0.0	20.0	0.0	2.0					CARD 223
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0					CARD 224
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0					CARD 225
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0					CARD 226
0.0	5.0	10.0	15.0	20.0	25.0							CARD 227
2.0	4.0											CARD 228
	RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 30											
6	2	1000	101	103	1	1	0	1	3	0	0	CARD 229
10.0	200.0	0.0	5.0	10.0	10.0	0.0	2.0					CARD 230
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0					CARD 231
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0					CARD 232
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0					CARD 233
0.0	5.0	10.0	15.0	20.0	25.0							CARD 234
2.0	4.0											CARD 235
	RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 31											
6	2	1000	101	103	1	1	0	1	3	0	0	CARD 236
10.0	200.0	0.0	5.0	0.0	20.0	1.0	1.0					CARD 237
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0					CARD 238
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0					CARD 239
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0					CARD 240
0.0	5.0	10.0	15.0	20.0	25.0							CARD 241
2.0	4.0											CARD 242
	RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 32											
6	2	1000	101	103	1	1	0	1	3	0	0	CARD 243
10.0	200.0	0.0	5.0	0.0	20.0	1.0	1.0					CARD 244
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0					CARD 245
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0					CARD 246
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0					CARD 247
0.0	5.0	10.0	15.0	20.0	25.0							CARD 248
2.0	4.0											CARD 249
											CARD 250	

B.1 INPUT DATA OF ALL FIFTY CASES (continued)

10.0	200.0	0.0	5.0	0.0	20.0	0.0	2.0	CARD 251
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 252
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 253
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 254
0.0	5.0	10.0	15.0	20.0	25.0			CARD 255
2.0	4.0							CARD 256
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 33								CARD 257
6	2	1000	101	103	1	1	1	CARD 258
10.0	200.0	0.0	0.0	10.0	10.0	0.0	10.0	CARD 259
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 260
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 261
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 262
0.0	5.0	10.0	15.0	20.0	25.0			CARD 263
2.0	4.0							CARD 264
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 34								CARD 265
6	2	1000	101	103	1	1	1	CARD 266
10.0	200.0	0.0	5.0	10.0	10.0	0.0	10.0	CARD 267
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 268
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 269
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 270
0.0	5.0	10.0	15.0	20.0	25.0			CARD 271
2.0	4.0							CARD 272
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 35								CARD 273
6	2	1000	101	103	1	1	1	CARD 274
10.0	200.0	0.0	0.0	0.0	20.0	0.0	10.0	CARD 275
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 276
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 277
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 278
0.0	5.0	10.0	15.0	20.0	25.0			CARD 279
2.0	4.0							CARD 280
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 36								CARD 281
6	2	1000	101	103	1	1	1	CARD 282
10.0	200.0	0.0	5.0	0.0	20.0	0.0	10.0	CARD 283
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 284
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 285
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 286
0.0	5.0	10.0	15.0	20.0	25.0			CARD 287
2.0	4.0							CARD 288
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 37								CARD 289
6	2	1000	101	103	1	1	1	CARD 290
10.0	200.0	0.0	0.0	10.0	10.0	0.0	10.0	CARD 291
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 292
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 293
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 294
0.0	5.0	10.0	15.0	20.0	25.0			CARD 295
2.0	4.0							CARD 296
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 38								CARD 297
6	2	1000	101	103	1	1	1	CARD 298
10.0	200.0	0.0	5.0	10.0	10.0	0.0	10.0	CARD 299
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 300

B.1 INPUT DATA OF ALL FIFTY CASES (continued)

0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 301
10.0	200.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 302
0.0	5.0	10.0	15.0	20.0	25.0			CARD 303
2.0	4.0							CARD 304
	RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 39							CARD 305
6	5	2 1000	101 103	1 1 0	1 3 0	1	1	CARD 306
10.0	200.0	0.0	9.0	0.0	20.0	0.0	10.0	CARD 307
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 308
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 309
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 310
0.0	5.0	10.0	15.0	20.0	25.0			CARD 311
2.0	4.0							CARD 312
	RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 40							CARD 313
6	6	2 1000	101 103	1 1 0	1 3 0	1	1	CARD 314
10.0	200.0	0.0	5.0	0.0	20.0	0.0	10.0	CARD 315
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 316
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 317
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 318
0.0	5.0	10.0	15.0	20.0	25.0			CARD 319
2.0	4.0							CARD 320
	RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 41							CARD 321
6	6	2 1000	101 103	1 1 0	1 3 1	1	1	CARD 322
10.0	200.0	0.0	0.0	0.0	200.0	1.0	1.0	CARD 323
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 324
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 325
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 326
0.0	5.0	10.0	15.0	20.0	25.0			CARD 327
2.0	4.0							CARD 328
	RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 42							CARD 329
6	6	2 1000	101 103	1 1 0	1 3 1	1	1	CARD 330
10.0	200.0	0.0	5.0	0.0	200.0	1.0	1.0	CARD 331
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 332
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 333
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 334
0.0	5.0	10.0	15.0	20.0	25.0			CARD 335
2.0	4.0							CARD 336
	RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 43							CARD 337
6	6	2 1000	101 103	1 1 0	1 3 1	1	1	CARD 338
10.0	200.0	0.0	0.0	0.0	200.0	0.0	2.0	CARD 339
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 340
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 341
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 342
0.0	5.0	10.0	15.0	20.0	25.0			CARD 343
2.0	4.0							CARD 344
	RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 44							CARD 345
6	6	2 1000	101 103	1 1 0	1 3 1	1	1	CARD 346
10.0	200.0	0.0	5.0	0.0	200.0	0.0	2.0	CARD 347
0.2	0.5	0.05	30.0	5.0	5.0	0.01	0.0	CARD 348
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	1.0	CARD 349
10.0	20.0	30.0	40.0	50.0	60.0	70.0	80.0	CARD 350

8.1 INPUT DATA OF ALL FIFTY CASES (continued)

0.0	5.0	10.0	15.0	20.0	25.0		CARD 351
2.0	4.0						CARD 352
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 45							CARD 353
6	2 1000 101 103	1 1 0	1 3	1 0			CARD 354
10.0	200.0	0.0	0.0	200.0	1.0	1.0	CARD 355
0.2	0.5	0.05	30.0	5.0	5.0	0.01	CARD 356
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	CARD 357
10.0	20.0	30.0	40.0	50.0	60.0	70.0	CARD 358
0.0	5.0	10.0	15.0	20.0	25.0		CARD 359
2.0	4.0						CARD 360
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 46							CARD 361
6	2 1000 101 103	1 1 0	1 3	1 0			CARD 362
10.0	200.0	0.0	5.0	200.0	1.0	1.0	CARD 363
0.2	0.5	0.05	30.0	5.0	5.0	0.01	CARD 364
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	CARD 365
10.0	20.0	30.0	40.0	50.0	60.0	70.0	CARD 366
0.0	5.0	10.0	15.0	20.0	25.0		CARD 367
2.0	4.0						CARD 368
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 47							CARD 369
6	2 1000 101 103	1 1 0	1 3	1 0			CARD 370
10.0	200.0	0.0	0.0	200.0	0.0	2.0	CARD 371
0.2	0.5	0.05	30.0	5.0	5.0	0.01	CARD 372
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	CARD 373
10.0	20.0	30.0	40.0	50.0	60.0	70.0	CARD 374
0.0	5.0	10.0	15.0	20.0	25.0		CARD 375
2.0	4.0						CARD 376
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 48							CARD 377
6	2 1000 101 103	1 1 0	1 3	1 0			CARD 378
10.0	200.0	0.0	5.0	200.0	0.0	2.0	CARD 379
0.2	0.5	0.05	30.0	5.0	5.0	0.01	CARD 380
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	CARD 381
10.0	20.0	30.0	40.0	50.0	60.0	70.0	CARD 382
0.0	5.0	10.0	15.0	20.0	25.0		CARD 383
2.0	4.0						CARD 384
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 49							CARD 385
6	2 1000 101 103	1 1 0	1 3	1 1			CARD 386
10.0	200.0	0.0	0.0	200.0	0.0	10.0	CARD 387
0.2	0.5	0.05	30.0	5.0	5.0	0.01	CARD 388
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	CARD 389
10.0	20.0	30.0	40.0	50.0	60.0	70.0	CARD 390
0.0	5.0	10.0	15.0	20.0	25.0		CARD 391
2.0	4.0						CARD 392
RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 50							CARD 393
6	2 1000 101 103	1 1 0	1 3	1 1			CARD 394
10.0	200.0	0.0	5.0	200.0	0.0	10.0	CARD 395
0.2	0.5	0.05	30.0	5.0	5.0	0.01	CARD 396
0.0	0.00000283	1400.0	1000.0	0.001	12.0	240.0	CARD 397
10.0	20.0	30.0	40.0	50.0	60.0	70.0	CARD 398
0.0	5.0	10.0	15.0	20.0	25.0		CARD 399
2.0	4.0						CARD 400

IHC002I STOP 0

B.2 OUTPUT OF SAMPLE CASE NO. 1

RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 1

NO. OF POINTS IN X-DIRECTION	6
NO. OF POINTS IN Y-DIRECTION	6
NO. OF POINTS IN Z-DIRECTION	2
NO. OF ROOTS: NO. OF SERIES TERMS	1000
NO. OF BEGINNING TIME STEPS	100
NO. OF ENDING TIME STEP	103
NO. OF TIME INTERVALS FOR PRINTED OUT SOLUTION	1
INSTANTANEOUS SOURCE CONTROL = 0 FOR INSTANT SOURCE	1
SOURCE CONDITION CONTROL = 0 FOR STEADY SOURCE	0
INTERMITTENT OUTPUT CONTROL = 0 NO SUCH OUTPUT	1
CASE CONTROL = 1 THERMAL, = 2 FOR CHEMICAL, = 3 RAD	3
 AQUIFER DEPTH, = 0.0 FOR INFINITE DEEP (METERS)	0.1000E 02
AQUIFER WIDTH, = 0.0 FOR INFINITE WIDE (METERS)	0.2000E 03
BEGIN POINT OF X-SOURCE LOCATION (METERS)	0.0
END POINT OF X-SOURCE LOCATION (METERS)	0.0
BEGIN POINT OF Y-SOURCE LOCATION (METERS)	0.1000E 02
END POINT OF Y-SOURCE LOCATION (METERS)	0.1000E 02
BEGIN POINT OF Z-SOURCE LOCATION (METERS)	0.1000E 01
END POINT OF Z-SOURCE LOCATION (METERS)	0.1000E 01
 POROSITY	0.2000E 00
HYDRAULIC CONDUCTIVITY (METER/HOUR)	0.5000E 00
HYDRAULIC GRADIENT	0.5000E-01
LONGITUDINAL DISPERSIVITY (METER)	0.3000E 02
LATERAL DISPERSIVITY (METER)	0.5000E 01
VERTICAL DISPERSIVITY (METER)	0.5000E 01
DISTRIBUTION COEFFICIENT, KD (M**3/KG)	0.1000E-01
HEAT EXCHANGE COEFFICIENT (KCAL/HR-M**2-DEGREE C)	0.0
 MOLECULAR DIFFUSION MULTIPLY BY POROSITY (M**2/HR)	0.0
DECAY CONSTANT (PER HOUR)	0.2830E-05
BULK DENSITY OF THE SOIL (GRAM/CM**3)	0.1400E-04
ACCURACY TOLERANCE FOR REACHING STEADY STATE	0.1000E-02
DENSITY OF WATER (KG/M**3)	0.1000E 04
TIME INTERVAL SIZE FOR THE DESIRED SOLUTION (HR)	0.1200E 02
DISCHARGE TIME (HR), (KG/HR), OR (CI/HR)	0.2400E 03
WASTE RELEASE RATE (KCAL/HR); (KG/HR); OR (CI/HR)	0.1000E 01
 RETARDATION FACTOR	0.7300E 02
RETARDED Darcy VELOCITY (M/HR)	0.1761E-02
RETARDED LONGITUDINAL DISPERSION COEF. (M**2/HR)	0.5282E-01
RETARDED LATERAL DISPERSION COEFFICIENT (M**2/HR)	0.8803E-02
RETARDED VERTICAL DISPERSION COFFICIENT (M**2/HR)	0.8803E-02

B.2 OUTPUT OF SAMPLE CASE NO. 1 (continued)

DISTRIBUTION OF RAD WASTE IN PCI AT 0.0 HRS

	Z = 2.00					
Y	10.	20.	30.	40.	X 50.	60.
0.	0.0	0.0	0.0	0.0	0.0	0.0
5.	0.0	0.0	0.0	0.0	0.0	0.0
10.	0.0	0.0	0.0	0.0	0.0	0.0
15.	0.0	0.0	0.0	0.0	0.0	0.0
20.	0.0	0.0	0.0	0.0	0.0	0.0
25.	0.0	0.0	0.0	0.0	0.0	0.0

Z = 4.00

Y	10.	20.	30.	40.	X 50.	60.
0.	0.0	0.0	0.0	0.0	0.0	0.0
5.	0.0	0.0	0.0	0.0	0.0	0.0
10.	0.0	0.0	0.0	0.0	0.0	0.0
15.	0.0	0.0	0.0	0.0	0.0	0.0
20.	0.0	0.0	0.0	0.0	0.0	0.0
25.	0.0	0.0	0.0	0.0	0.0	0.0

DISTRIBUTION OF RAD WASTE IN PCI AT 0.1200E-04 HRS

	Z = 2.00					
Y	10.	20.	30.	40.	X 50.	60.
0.	3.167E-00	3.522E-01	0.586E-02	0.387E-03	0.971E-05	0.112E-06
5.	0.274E-03	0.950E-02	0.146E-02	0.991E-03	0.301E-01	0.410E-03
10.	0.334E-05	0.104E-05	0.134E-04	0.743E-02	0.180E-01	0.198E-01
15.	0.274E-03	0.950E-02	0.146E-02	0.991E-03	0.301E-01	0.410E-03
20.	0.234E-00	0.733E-01	0.963E-02	0.543E-03	0.136E-04	0.158E-06
25.	0.505E-01	0.156E-01	0.200E-02	0.108E-03	0.250E-05	0.256E-07

Z = 4.00

Y	10.	20.	30.	40.	X 50.	60.
0.	0.199E-01	0.573E-02	0.995E-03	0.651E-04	0.191E-05	0.255E-07
5.	0.719E-02	0.251E-02	0.388E-01	0.268E-03	0.826E-02	0.114E-03
10.	3.373E-04	0.125E-04	0.181E-03	0.115E-02	0.324E-03	0.409E-02
15.	0.719E-02	0.251E-02	0.388E-01	0.268E-03	0.826E-02	0.114E-03
20.	0.268E-01	0.907E-02	0.135E-02	0.895E-04	0.267E-05	0.363E-07
25.	0.536E-02	0.176E-02	0.247E-03	0.149E-04	0.392E-06	0.454E-08

8.2 OUTPUT OF SAMPLE CASE NO. 1 (continued)

DISTRIBUTION OF RAD WASTE IN PCI AT 0.1212E 04 HRS

Z = 2.00

Y	10.	20.	30.	40.	X 50.	60.
0.	0.167E 00	0.529E-01	0.712E-02	0.415E-03	0.108E-04	0.130E-06
5.	0.274E 03	0.960E 02	0.150E 02	0.105E 01	0.332E-01	0.473E-03
10.	0.333E 05	0.105E 05	0.140E 04	0.797E 02	0.201E 01	0.231E-01
15.	0.274E 03	0.960E 02	0.150E 02	0.105E 01	0.332E-01	0.473E-03
20.	0.234E 00	0.744E-01	0.100E-01	0.582E-03	0.152E-04	0.184E-06
25.	0.504E-01	0.158E-01	0.208E-02	0.116E-03	0.280E-05	0.361E-07

Z = 4.00

Y	10.	20.	30.	40.	X 50.	60.
0.	0.199E-01	0.681E-02	0.103E-02	0.693E-04	0.211E-05	0.294E-07
5.	0.718E 02	0.253E 02	0.401E 01	0.285E 00	0.910E-02	0.132E-02
10.	0.372E 04	0.126E 04	0.187E 03	0.123E 02	0.359E 00	0.474E-02
15.	0.718E 02	0.253E 02	0.401E 01	0.285E 00	0.910E-02	0.132E-02
20.	0.267E-01	0.918E-02	0.140E-02	0.953E-04	0.295E-05	0.419E-07
25.	0.535E-02	0.178E-02	0.255E-03	0.159E-04	0.436E-06	0.529E-08

STEADY STATE SOLUTION HAS NOT BEEN REACHED BEFORE FINAL SIMULATING TIME

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DISTRIBUTION OF RAD WASTE IN PCI AT 0.1224E 04 HRS

Z = 2.00

Y	10.	20.	30.	40.	X 50.	60.
0.	0.166E 00	0.537E-01	0.739E-02	0.444E-03	0.120E-04	0.152E-06
5.	0.273E 03	0.971E 02	0.155E 02	0.112E 01	0.368E-01	0.544E-03
10.	0.333E 05	0.107E 05	0.145E 04	0.854E 02	0.224E 01	0.269E-01
15.	0.273E 03	0.971E 02	0.155E 02	0.112E 01	0.366E-01	0.544E-03
20.	0.234E 00	0.754E-01	0.104E-01	0.623E-03	0.169E-04	0.214E-06
25.	0.504E-01	0.160E-01	0.216E-02	0.124E-03	0.313E-05	0.352E-07

Z = 4.00

Y	10.	20.	30.	40.	X 50.	60.
0.	0.199E-01	0.689E-02	0.105E-02	0.737E-04	0.233E-05	0.339E-07
5.	0.717E 02	0.256E 02	0.413E 01	0.302E 00	0.100E-01	0.151E-03
10.	0.372E 04	0.128E 04	0.194E 03	0.131E 02	0.397E 00	0.548E-02
15.	0.717E 02	0.256E 02	0.413E 01	0.302E 00	0.100E-01	0.151E-03
20.	0.267E-01	0.929E-02	0.144E-02	0.101E-03	0.325E-05	0.482E-07
25.	0.535E-02	0.180E-02	0.264E-03	0.170E-04	0.483E-06	0.615E-08

B.3 OUTPUT OF SAMPLE CASE NO. 2

RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 39

NO. OF POINTS IN X-DIRECTION	6
NO. OF POINTS IN Y-DIRECTION	6
NO. OF POINTS IN Z-DIRECTION	2
NO. OF ROOTS; NO. OF SERIES TERMS	1000
NO. OF BEGINNING TIME STEPS	101
NO. OF ENDING TIME STEP	103
NO. OF TIME INTERVALS FOR PRINTED OUT SOLUTION	1
INSTANTANEOUS SOURCE CONTROL = 0 FOR INSTANT SOURCE	1
SOURCE CONDITION CONTROL = 0 FOR STEADY SOURCE	0
INTERMITTENT OUTPUT CONTROL = 0 NO SUCH OUTPUT	1
CASE CONTROL = 1 THERMAL, = 2 FOR CHEMICAL, = 3 RAD	3

AQUIFER DEPTH, = 0.0 FOR INFINITE DEEP (METERS)	0.1000E 02
AQUIFER WIDTH, = 0.0 FOR INFINITE WIDE (METERS)	0.0
BEGIN POINT OF X-SOURCE LOCATION (METERS)	0.0
END POINT OF X-SOURCE LOCATION (METERS)	0.0
BEGIN POINT OF Y-SOURCE LOCATION (METERS)	0.0
END POINT OF Y-SOURCE LOCATION (METERS)	0.2000E 02
BEGIN POINT OF Z-SOURCE LOCATION (METERS)	0.0
END POINT OF Z-SOURCE LOCATION (METERS)	0.1000E 02

POROSITY	0.2000E 00
HYDRAULIC CONDUCTIVITY (METER/HOUR)	0.5000E 00
HYDRAULIC GRADIENT	0.5000E-01
LONGITUDINAL DISPERSIVITY (METER)	0.3000E 02
LATERAL DISPERSIVITY (METER)	0.5000E-01
VERTICAL DISPERSIVITY (METER)	0.5000E-01
DISTRIBUTION COEFFICIENT, K0 (M**3/KG)	0.1000E-01
HEAT EXCHANGE COEFFICIENT (KCAL/HR-M**2-DEGREE C)	0.0

MOLECULAR DIFFUSION MULTIPLY BY POROSITY (MM**2/HR)	0.0
DECAY CONSTANT (PER HOUR)	0.2830E-05
BULK DENSITY OF THE SOIL (GRAM/CM**3)	0.1400E-04
ACCURACY TOLERANCE FOR REACHING STEADY STATE	0.1000E-02
DENSITY OF WATER (KG/M**3)	0.1000E-04
TIME INTERVAL SIZE FOR THE DESIRED SOLUTION (HR)	0.1200E 02
DISCHARGE TIME (HR)	0.2400E 03
WASTE RELEASE RATE (KCAL/HR), (KG/HR), OR (CI/HR)	0.1000E 01

RETARDATION FACTOR	0.7100E 02
RETARDED DARCY VELOCITY (M/HR)	0.1761E-02
RETARDED LONGITUDINAL DISPERSION COEF., (M**2/HR)	0.5262E-01
RETARDED LATERAL DISPERSION COEFFICIENT (M**2/HR)	0.8803E-02
RETARDED VERTICAL DISPERSION COEFFICIENT (M**2/HR)	0.8803E-02

B.3 OUTPUT OF SAMPLE CASE NO. 2 (continued)

DISTRIBUTION OF RAD WASTE IN PCI AT 0.0 HRS

Z = 2.00

Y	10.	20.	30.	40.	X 50.	60.
0.	0.0	0.0	0.0	0.0	0.0	0.0
5.	0.0	0.0	0.0	0.0	0.0	0.0
10.	0.0	0.0	0.0	0.0	0.0	0.0
15.	0.0	0.0	0.0	0.0	0.0	0.0
20.	0.0	0.0	0.0	0.0	0.0	0.0
25.	0.0	0.0	0.0	0.0	0.0	0.0

Z = 4.00

Y	10.	20.	30.	40.	X 50.	60.
0.	0.0	0.0	0.0	0.0	0.0	0.0
5.	0.0	0.0	0.0	0.0	0.0	0.0
10.	0.0	0.0	0.0	0.0	0.0	0.0
15.	0.0	0.0	0.0	0.0	0.0	0.0
20.	0.0	0.0	0.0	0.0	0.0	0.0
25.	0.0	0.0	0.0	0.0	0.0	0.0

DISTRIBUTION OF RAD WASTE IN PCI AT 0.1200E 04 HRS

Z = 2.00

Y	10.	20.	30.	40.	X 50.	60.
0.	0.116E 04	0.368E 03	0.493E 02	0.286E 01	0.732E-01	0.850E-03
5.	0.232E 04	0.735E 03	0.985E 02	0.570E 01	0.146E 00	0.169E-02
10.	0.232E 04	0.736E 03	0.987E 02	0.571E 01	0.146E 00	0.170E-02
15.	0.232E 04	0.735E 03	0.985E 02	0.570E 01	0.146E 00	0.169E-02
20.	0.116E 04	0.368E 03	0.493E 02	0.286E 01	0.732E-01	0.850E-03
25.	0.352E 01	0.122E 01	0.189E 00	0.130E-01	0.402E-03	0.555E-05

Z = 4.00

Y	10.	20.	30.	40.	X 50.	60.
0.	0.116E 04	0.368E 03	0.493E 02	0.286E 01	0.732E-01	0.850E-03
5.	0.232E 04	0.735E 03	0.985E 02	0.570E 01	0.146E 00	0.169E-02
10.	0.232E 04	0.736E 03	0.987E 02	0.571E 01	0.146E 00	0.170E-02
15.	0.232E 04	0.735E 03	0.985E 02	0.570E 01	0.146E 00	0.169E-02
20.	0.116E 04	0.368E 03	0.493E 02	0.286E 01	0.732E-01	0.850E-03
25.	0.352E 01	0.122E 01	0.189E 00	0.130E-01	0.402E-03	0.555E-05

B.3 OUTPUT OF SAMPLE CASE NO. 2 (continued)

DISTRIBUTION OF RAD WASTE IN PCI AT 0.1212E 04 HRS

	Z = 2.00					
Y	10.	20.	30.	40.	X 50.	60.
0.	0.116E 04	0.373E 03	0.512E 02	0.306E 01	0.815E-01	0.990E-03
5.	0.231E 04	0.745E 03	0.102E 03	0.610E 01	0.162E 00	0.197E-02
10.	0.232E 04	0.746E 03	0.102E 03	0.612E 01	0.163E 00	0.198E-02
15.	0.231E 04	0.745E 03	0.102E 03	0.610E 01	0.162E 00	0.197E-02
20.	0.116E 04	0.373E 03	0.512E 02	0.306E 01	0.815E-01	0.990E-03
25.	0.351E 01	0.124E 01	0.196E 00	0.139E-01	0.443E-03	0.639E-05

	Z = 4.00					
Y	10.	20.	30.	40.	X 50.	60.
0.	0.116E 04	0.373E 03	0.512E 02	0.306E 01	0.815E-01	0.990E-03
5.	0.231E 04	0.745E 03	0.102E 03	0.610E 01	0.162E 00	0.197E-02
10.	0.232E 04	0.746E 03	0.102E 03	0.612E 01	0.163E 00	0.198E-02
15.	0.231E 04	0.745E 03	0.102E 03	0.610E 01	0.162E 00	0.197E-02
20.	0.116E 04	0.373E 03	0.512E 02	0.306E 01	0.815E-01	0.990E-03
25.	0.351E 01	0.124E 01	0.196E 00	0.139E-01	0.443E-03	0.639E-05

STEADY STATE SOLUTION HAS NOT BEEN REACHED BEFORE FINAL SIMULATING TIME

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DISTRIBUTION OF RAD WASTE IN PCI AT 0.1224E 04 HRS

	Z = 2.00					
Y	10.	20.	30.	40.	X 50.	60.
0.	0.116E 04	0.378E 03	0.531E 02	0.327E 01	0.905E-01	0.115E-02
5.	0.231E 04	0.755E 03	0.106E 03	0.652E 01	0.180E 00	0.229E-02
10.	0.231E 04	0.756E 03	0.106E 03	0.654E 01	0.181E 00	0.230E-02
15.	0.231E 04	0.755E 03	0.106E 03	0.652E 01	0.180E 00	0.229E-02
20.	0.116E 04	0.378E 03	0.531E 02	0.327E 01	0.905E-01	0.115E-02
25.	0.351E 01	0.125E 01	0.202E 00	0.147E-01	0.487E-03	0.735E-05

	Z = 4.00					
Y	10.	20.	30.	40.	X 50.	60.
0.	0.116E 04	0.378E 03	0.531E 02	0.327E 01	0.905E-01	0.115E-02
5.	0.231E 04	0.755E 03	0.106E 03	0.652E 01	0.180E 00	0.229E-02
10.	0.231E 04	0.756E 03	0.106E 03	0.654E 01	0.181E 00	0.230E-02
15.	0.231E 04	0.755E 03	0.106E 03	0.652E 01	0.180E 00	0.229E-02
20.	0.116E 04	0.378E 03	0.531E 02	0.327E 01	0.905E-01	0.115E-02
25.	0.351E 01	0.125E 01	0.202E 00	0.147E-01	0.487E-03	0.735E-05

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B.4 OUTPUT OF SAMPLE CASE NO. 3

RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 48

NO. OF POINTS IN X-DIRECTION	6
NO. OF POINTS IN Y-DIRECTION	6
NO. OF POINTS IN Z-DIRECTION	2
NO. OF ROOTS: NO. OF SERIES TFRMS	1000
NO. OF BEGINNING TIME STEPS	100
NO. OF ENDING TIME STEP	103
NO. OF TIME INTERVALS FOR PRINTED OUT SOLUTION	3
INSTANTANEOUS SOURCE CONTROL = 0 FOR INSTANT SOURCE	1
SOURCE CONDITION CONTROL = 0 FOR STEADY SOURCE	0
INTERMITTENT OUTPUT CONTROL = 0 NO SUCH OUTPUT	0
CASE CONTROL #1 THERMAL, = 2 FOR CHEMICAL, = 3 RAD	3
 AQUIFER DEPTH, = 0.0 FOR INFINITE DEEP (METERS)	0.0
AQUIFER WIDTH, = 0.0 FOR INFINITE WIDE (METERS)	0.2000E 03
BEGIN POINT OF X-SOURCE LOCATION (METERS)	0.0
END POINT OF X-SOURCE LOCATION (METERS)	0.5000E 01
BEGIN POINT OF Y-SOURCE LOCATION (METERS)	0.0
END POINT OF Y-SOURCE LOCATION (METERS)	0.2000E 02
BEGIN POINT OF Z-SOURCE LOCATION (METERS)	0.0
END POINT OF Z-SOURCE LOCATION (METERS)	0.2000E 01
 POROSITY	0.2000E 00
HYDRAULIC CONDUCTIVITY (METER/HOUR)	0.5000E 00
HYDRAULIC GRADIENT	0.5000E-01
LONGITUDINAL DISPERSIVITY (METER)	0.3000E 02
LATERAL DISPERSIVITY (METER)	0.5000E 01
VERTICAL DISPERSIVITY (METER)	0.5000E 01
DISTRIBUTION COEFFICIENT, Kd (M**3/KG)	0.1000E-01
HEAT EXCHANGE COEFFICIENT (KCAL/HR-M**2-DEGREE C)	0.0
 MOLECULAR DIFFUSION MULTIPLY BY TURBOSITY (M**2/HR)	0.0
DECAY CONSTANT (PER HOUR)	0.2830E-05
BULK DENSITY OF THE SOIL (GRAM/CM**3)	0.1430E 04
ACCURACY TOLERANCE FOR REACHING STEADY STATE	0.1000E-02
DENSITY OF WATER (KG/M**3)	0.1000E 04
TIME INTERVAL SIZE FOR THE DESIRED SOLUTION (HR)	0.1200E 02
DISCHARGE TIME (HR)	0.2400E 03
WASTE RELEASE RATE (KCAL/HR), (KG/HR), OR (CL/HR)	0.1000 E 01
 RETARDATION FACTOR	0.7100E 02
RETARDED DARCY VELOCITY (M/HR)	0.1761E-02
RETARDED LONGITUDINAL DISPERSION COEF. (M**2/HR)	0.5282E-01
RETARDED LATERAL DISPERSION COEFFICIENT (M**2/HR)	0.8803E-02
RETARDED VERTICAL DISPERSION COEFFICIENT (M**2/HR)	0.8803E-02

B.4 OUTPUT OF SAMPLE CASE NO. 3 (continued)

DISTRIBUTION OF RAD WASTE IN PCI AT 0.0 HRS

Z = 2.00						
Y	10.	20.	30.	40.	X	60.
0.	0.0	0.0	0.0	0.0	0.0	0.0
5.	0.0	0.0	0.0	0.0	0.0	0.0
10.	0.0	0.0	0.0	0.0	0.0	0.0
15.	0.0	0.0	0.0	0.0	0.0	0.0
20.	0.0	0.0	0.0	0.0	0.0	0.0
25.	0.0	0.0	0.0	0.0	0.0	0.0
Z = 4.00						
Y	10.	20.	30.	40.	X	60.
0.	0.0	0.0	0.0	0.0	0.0	0.0
5.	0.0	0.0	0.0	0.0	0.0	0.0
10.	0.0	0.0	0.0	0.0	0.0	0.0
15.	0.0	0.0	0.0	0.0	0.0	0.0
20.	0.0	0.0	0.0	0.0	0.0	0.0
25.	0.0	0.0	0.0	0.0	0.0	0.0

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DISTRIBUTION OF RAD WASTE IN PCI AT 0.1200E-04 HRS

Z = 2.00						
Y	10.	20.	30.	40.	X	60.
0.	0.661E-03	0.265E-03	0.453E-02	0.337E-01	0.111E-00	0.166E+02
5.	0.661E-03	0.265E-03	0.453E-02	0.337E-01	0.111E-00	0.166E+02
10.	0.661E-03	0.265E-03	0.453E-02	0.337E-01	0.111E-00	0.166E+02
15.	0.661E-03	0.265E-03	0.453E-02	0.337E-01	0.111E-00	0.166E+02
20.	0.661E-03	0.265E-03	0.453E-02	0.337E-01	0.111E-00	0.166E+02
25.	0.661E-03	0.265E-03	0.453E-02	0.337E-01	0.111E-00	0.166E+02
Z = 4.00						
Y	10.	20.	30.	40.	X	60.
0.	0.107E-03	0.450E-02	0.830E-01	0.678E-00	0.248E-01	0.412E-03
5.	0.107E-03	0.450E-02	0.830E-01	0.678E-00	0.248E-01	0.412E-03
10.	0.107E-03	0.450E-02	0.830E-01	0.678E-00	0.248E-01	0.412E-03
15.	0.107E-03	0.450E-02	0.830E-01	0.678E-00	0.248E-01	0.412E-03
20.	0.107E-03	0.450E-02	0.830E-01	0.678E-00	0.248E-01	0.412E-03
25.	0.107E-03	0.450E-02	0.830E-01	0.678E-00	0.248E-01	0.412E-03

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B.4 OUTPUT OF SAMPLE CASE NO. 3 (continued)

DISTRIBUTION OF RAD WASTE IN PCI AT 0.1212E 04 HRS

	Z = 2.00					
Y	10.	20.	30.	40.	X 50.	60.
0.	0.659E 03	0.267E 03	0.466E 02	0.357E 01	0.122E 00	0.192E-02
5.	0.659E 03	0.267E 03	0.466E 02	0.357E 01	0.122E 00	0.192E-02
10.	0.659E 03	0.267E 03	0.466E 02	0.357E 01	0.122E 00	0.192E-02
15.	0.659E 03	0.267E 03	0.466E 02	0.357E 01	0.122E 00	0.192E-02
20.	0.659E 03	0.267E 03	0.466E 02	0.357E 01	0.122E 00	0.192E-02
25.	0.659E 03	0.267E 03	0.466E 02	0.357E 01	0.122E 00	0.192E-02
	Z = 4.00					
Y	10.	20.	30.	40.	X 50.	60.
0.	0.107E 03	0.453E 02	0.852E 01	0.715E 00	0.271E-01	0.471E-03
5.	0.107E 03	0.453E 02	0.852E 01	0.715E 00	0.271E-01	0.471E-03
10.	0.107E 03	0.453E 02	0.852E 01	0.715E 00	0.271E-01	0.471E-03
15.	0.107E 03	0.453E 02	0.852E 01	0.715E 00	0.271E-01	0.471E-03
20.	0.107E 03	0.453E 02	0.852E 01	0.715E 00	0.271E-01	0.471E-03
25.	0.107E 03	0.453E 02	0.852E 01	0.715E 00	0.271E-01	0.471E-03

STEADY STATE SOLUTION HAS NOT BEEN REACHED BEFORE FINAL SIMULATING TIME

DISTRIBUTION OF RAD WASTE IN PCI AT 0.1224E 04 HRS

	Z = 2.00					
Y	10.	20.	30.	40.	X 50.	60.
0.	0.657E 03	0.269E 03	0.480E 02	0.377E 01	0.134E 00	0.218E-02
5.	0.657E 03	0.269E 03	0.480E 02	0.377E 01	0.134E 00	0.218E-02
10.	0.657E 03	0.269E 03	0.480E 02	0.377E 01	0.134E 00	0.218E-02
15.	0.657E 03	0.269E 03	0.480E 02	0.377E 01	0.134E 00	0.218E-02
20.	0.657E 03	0.269E 03	0.480E 02	0.377E 01	0.134E 00	0.218E-02
25.	0.657E 03	0.269E 03	0.480E 02	0.377E 01	0.134E 00	0.218E-02
	Z = 4.00					
Y	10.	20.	30.	40.	X 50.	60.
0.	0.107E 03	0.457E 02	0.875E 01	0.754E 00	0.296E-01	0.532E-03
5.	0.107E 03	0.457E 02	0.875E 01	0.754E 00	0.296E-01	0.532E-03
10.	0.107E 03	0.457E 02	0.875E 01	0.754E 00	0.296E-01	0.532E-03
15.	0.107E 03	0.457E 02	0.875E 01	0.754E 00	0.296E-01	0.532E-03
20.	0.107E 03	0.457E 02	0.875E 01	0.754E 00	0.296E-01	0.532E-03
25.	0.107E 03	0.457E 02	0.875E 01	0.754E 00	0.296E-01	0.532E-03

B.5 OUTPUT OF SAMPLE CASE NO. 4

RAD WASTE DISTRIBUTION IN GROUND WATER: SAMPLE PROBLEM CASE 50

NO. OF POINTS IN X-DIRECTION	6
NO. OF POINTS IN Y-DIRECTION	6
NO. OF POINTS IN Z-DIRECTION	2
NO. OF ROOTS; NO. OF SERIES TERMS	1000
NO. OF BEGINNING TIME STEPS	101
NO. OF ENDING TIME STEP	102
NO. OF TIME INTERVALS FOR PRINTED OUT SOLUTION	1
INSTANTANEOUS SOURCE CONTROL = 0 FOR INSTANT SOURCE	1
SOURCE CONDITION CONTROL = 0 FOR STEADY SOURCE	0
INTERMITTENT OUTPUT CONTROL = 0 NO SUCH OUTPUT	1
CASE CONTROL = 1 THERMAL, = 2 FOR CHEMICAL, = 3 RAD	3
 AQUIFER DEPTH, = 0.0 FOR INFINITE DEEP (METERS) ...	0.1000E 02
AQUIFER WIDTH, = 0.0 FOR INFINITE WIDE (METERS) ...	0.2000E 03
BEGIN POINT OF X-SOURCE LOCATION (METERS)	0.0
END POINT OF X-SOURCE LOCATION (METERS)	0.5000E 01
BEGIN POINT OF Y-SOURCE LOCATION (METERS)	0.0
END POINT OF Y-SOURCE LOCATION (METERS)	0.2000E 03
BEGIN POINT OF Z-SOURCE LOCATION (METERS)	0.0
END POINT OF Z-SOURCE LOCATION (METERS)	0.1000E 02
 POROSITY	0.2000E 00
HYDRAULIC CONDUCTIVITY (METER/HOUR)	0.5000E 00
HYDRAULIC GRADIENT	0.5000E-01
LONGITUDINAL DISPERSIVITY (METER)	0.3000E 02
LATERAL DISPERSIVITY (METER)	0.5000E 01
VERTICAL DISPERSIVITY (METER)	0.5000E 01
DISTRIBUTION COEFFICIENT, KD (MM ³ /KG)	0.1000E-01
HEAT EXCHANGE COEFFICIENT (KCAL/HR-M ² -DEGREE C),	0.0
 MOLECULAR DIFFUSION MULTIPLY BY TOROSITY (MM ² /HR)	0.0
DECAY CONSTANT (PER HOUR)	0.2830E-05
BULK DENSITY OF THE SOIL (GRAM/CM ³)	0.1400E 04
ACCURACY TOLERANCE FOR REACHING STEADY STATE	0.1000E-02
DENSITY OF WATER (KG/M ³)	0.1000E 04
TIME INTERVAL SIZE FOR THE DESIRED SOLUTION (HR)	0.1200E 02
DISCHARGE TIME (HR), (KG/HR), OR (CI/HP)	0.2400E 03
WASTE RELEASE RATE (KCAL/HR), (KG/HR), OR (CI/HP)	0.1000 E 01
 RETARDATION FACTOR	0.7100E 02
RETARDED Darcy VELOCITY (M/HR)	0.1761E-02
RETARDED LONGITUDINAL DISPERSION COEF., (MM ² /HR)	0.5282E-01
RETARDED LATERAL DISPERSION COEFFICIENT (MM ² /HR)	0.8803E-02
RETARDED VERTICAL DISPERSION COEFFICIENT (MM ² /HR)	0.8803E-02

B.5 OUTPUT OF SAMPLE CASE NO. 4 (continued)

DISTRIBUTION OF RAD WASTE IN PCI AT 0.0 HPS

Z = 2.00

Y	10.	20.	30.	40.	X 50.	60.
0.	0.0	0.0	0.0	0.0	0.0	0.0
5.	0.0	0.0	0.0	0.0	0.0	0.0
10.	0.0	0.0	0.0	0.0	0.0	0.0
15.	0.0	0.0	0.0	0.0	0.0	0.0
20.	0.0	0.0	0.0	0.0	0.0	0.0
25.	0.0	0.0	0.0	0.0	0.0	0.0

Z = 4.00

Y	10.	20.	30.	40.	X 50.	60.
0.	0.0	0.0	0.0	0.0	0.0	0.0
5.	0.0	0.0	0.0	0.0	0.0	0.0
10.	0.0	0.0	0.0	0.0	0.0	0.0
15.	0.0	0.0	0.0	0.0	0.0	0.0
20.	0.0	0.0	0.0	0.0	0.0	0.0
25.	0.0	0.0	0.0	0.0	0.0	0.0

DISTRIBUTION OF RAD WASTE IN PCI AT 0.1200E 04 HRS

Z = 2.00

Y	10.	20.	30.	40.	X 50.	60.
0.	0.268E 03	0.107E 03	0.184E 02	0.137E 01	0.454E-01	0.683E-03
5.	0.268E 03	0.107E 03	0.184E 02	0.137E 01	0.454E-01	0.683E-03
10.	0.268E 03	0.107E 03	0.184E 02	0.137E 01	0.454E-01	0.683E-03
15.	0.268E 03	0.107E 03	0.184E 02	0.137E 01	0.454E-01	0.683E-03
20.	0.268E 03	0.107E 03	0.184E 02	0.137E 01	0.454E-01	0.683E-03
25.	0.268E 03	0.107E 03	0.184E 02	0.137E 01	0.454E-01	0.683E-03

Z = 4.00

Y	10.	20.	30.	40.	X 50.	60.
0.	0.268E 03	0.107E 03	0.184E 02	0.137E 01	0.454E-01	0.683E-03
5.	0.268E 03	0.107E 03	0.184E 02	0.137E 01	0.454E-01	0.683E-03
10.	0.268E 03	0.107E 03	0.184E 02	0.137E 01	0.454E-01	0.683E-03
15.	0.268E 03	0.107E 03	0.184E 02	0.137E 01	0.454E-01	0.683E-03
20.	0.268E 03	0.107E 03	0.184E 02	0.137E 01	0.454E-01	0.683E-03
25.	0.268E 03	0.107E 03	0.184E 02	0.137E 01	0.454E-01	0.683E-03

B.5 OUTPUT OF SAMPLE CASE NO. 4 (continued)

DISTRIBUTION OF RAD WASTE IN PCI AT 0.1212E 04 HPS

	Z = 2.00					
Y	10.	20.	30.	40.	X 50.	60.
0.	0.267E 03	0.108E 03	0.190E 02	0.145E 01	0.499E-01	0.788E-03
5.	0.267E 03	0.108E 03	0.190E 02	0.145E 01	0.499E-01	0.788E-03
10.	0.267E 03	0.108E 03	0.190E 02	0.145E 01	0.499E-01	0.788E-03
15.	0.267E 03	0.108E 03	0.190E 02	0.145E 01	0.499E-01	0.788E-03
20.	0.267E 03	0.108E 03	0.190E 02	0.145E 01	0.499E-01	0.788E-03
25.	0.267E 03	0.108E 03	0.190E 02	0.145E 01	0.499E-01	0.788E-03
	Z = 4.00					
Y	10.	20.	30.	40.	X 50.	60.
0.	0.267E 03	0.108E 03	0.190E 02	0.145E 01	0.499E-01	0.788E-03
5.	0.267E 03	0.108E 03	0.190E 02	0.145E 01	0.499E-01	0.788E-03
10.	0.267E 03	0.108E 03	0.190E 02	0.145E 01	0.499E-01	0.788E-03
15.	0.267E 03	0.108E 03	0.190E 02	0.145E 01	0.499E-01	0.788E-03
20.	0.267E 03	0.108E 03	0.190E 02	0.145E 01	0.499E-01	0.788E-03
25.	0.267E 03	0.108E 03	0.190E 02	0.145E 01	0.499E-01	0.788E-03

STEADY STATE SOLUTION HAS NOT BEEN REACHED BEFORE FINAL SIMULATING TIME

DISTRIBUTION OF RAD WASTE IN PCI AT 0.12224E 04 HPS

	Z = 2.00					
Y	10.	20.	30.	40.	X 50.	60.
0.	0.266E 03	0.109E 03	0.195E 02	0.154E 01	0.547E-01	0.895E-03
5.	0.266E 03	0.109E 03	0.195E 02	0.154E 01	0.547E-01	0.895E-03
10.	0.266E 03	0.109E 03	0.195E 02	0.154E 01	0.547E-01	0.895E-03
15.	0.266E 03	0.109E 03	0.195E 02	0.154E 01	0.547E-01	0.895E-03
20.	0.266E 03	0.109E 03	0.195E 02	0.154E 01	0.547E-01	0.895E-03
25.	0.266E 03	0.109E 03	0.195E 02	0.154E 01	0.547E-01	0.895E-03
	Z = 4.00					
Y	10.	20.	30.	40.	X 50.	60.
0.	0.266E 03	0.109E 03	0.195E 02	0.154E 01	0.547E-01	0.895E-03
5.	0.266E 03	0.109E 03	0.195E 02	0.154E 01	0.547E-01	0.895E-03
10.	0.266E 03	0.109E 03	0.195E 02	0.154E 01	0.547E-01	0.895E-03
15.	0.266E 03	0.109E 03	0.195E 02	0.154E 01	0.547E-01	0.895E-03
20.	0.266E 03	0.109E 03	0.195E 02	0.154E 01	0.547E-01	0.895E-03
25.	0.266E 03	0.109E 03	0.195E 02	0.154E 01	0.547E-01	0.895E-03

APPENDIX C
LISTING OF FORTRAN SOURCE PROGRAM

APPENDIX C (continued)

```
C 300  QS(I)=1.0          MAIN 255
      DO 400 I=1,MAXRUT   MAIN 260
          RTY(I)=0.0        MAIN 265
          AIY(I)=0.0        MAIN 270
          RTZ(I)=0.0        MAIN 275
          AIZ(I)=0.0        MAIN 280
 400
C     ----- PASS THE PROGRAM TO AT123D
      CALL AT123D(TEMP,TEMPO,XDIM,YDIM,ZDIM,RTY,AIY,PSIS,FCTY,
> RTZ,AIZ,PHIS,FCTZ,QS,TITLE,MAXNX,MAXNY,MAXNZ,MAXNTI,MAXRUT)
C     STOP
      END
      MAIN 290
      MAIN 295
      MAIN 300
      MAIN 305
      MAIN 310
      MAIN 315
      MAIN 320
      MAIN 325
      MAIN 330
```

APPENDIX C (continued)

```

      SUBROUTINE AT123D(TEMP, TEMPO, XDIM, YDIM, ZDIM, RTY, AIV, PSIS, FCTY,
> RTZ, ATZ, PHIS, FCTZ, QS, TITLE, MAXNX, MAXNY, MAXNZ, MAXNTI, MAXRUT)
C
C      DIMENSION TITLE(20), XDIM(MAXNX), YDIM(MAXNY), ZDIM(MAXNZ)
C      DIMENSION TEMP(MAXNX,MAXNY,MAXNZ), TEMPO(MAXNX,MAXNY,MAXNZ)
C      DIMENSION RTY(MAXRUT), AIV(MAXRUT), PSIS(MAXRUT), FCTY(MAXNY,MAXNTI)
C      DIMENSION RTZ(MAXRUT), AIZ(MAXRUT), PHIS(MAXRUT), FCTZ(MAXNZ,MAXNTI)
C      DIMENSION QS(MAXNTI)

C      DATA CP,PAI/1.0,3.141593/

C      ----- READ IN TITLE, SYSTEM PARAMETERS, AND CONTROL INPUTS

999 READ(5,10,END=999) TITLE
      READ(5,20) NX,NY,NZ,NROOT,NBGT,I,NEDTI,NPRINT,INSTAN,NSOURS,INTER,
1 ICASE,IWID,IDEP,IBUG
      READ(5,30) DEPTH,WIDTH,RL1,RL2,RB1,RB2,RH1,RH2
      READ(5,30) POR,HCOND,HGRAD,AELONG,ATRANV,AVERTI,AKD,AKE
      READ(5,30) AMTAU,RAMADA,RHOB,RHOW,ACCU,DT,TDISP,Q
      READ(5,30) (XDIM(I),I=1,NX)
      READ(5,30) (YDIM(I),I=1,NY)
      READ(5,30) (ZDIM(I),I=1,NZ)
      IF(NSOURS.NE.0) READ(5,30) (QS(I),I=1,NSOURS)
      IF(IWID.EQ.0) WIDTH=0.0
      IF(IDEP.EQ.0) DEPTH=0.0

C      ----- PRINT TITLE, SYSTEM PARAMETERS AND CONTROL INPUTS

      WRITE(6,1000) (TITLE(I),I=1,20)
      WRITE(6,1100) NX,NY,NZ,NROOT,NBGT,I,NEDTI,NPRINT,INSTAN,NSOURS,
> INTER,ICASE
      WRITE(6,1200) DEPTH,WIDTH,RL1,RL2,RB1,RB2,RH1,RH2
      WRITE(6,1300) POR,HCOND,HGRAD,AELONG,ATRANV,AVERTI,AKD,AKE
      WRITE(6,1400) AMTAU,RAMADA,RHOB,ACCU,RHOW,DT,TDISP,Q
      IF(NSOURS.NE.0) WRITE(6,2000) (QS(I),I=1,NSOURS)

C      ----- MAKE SOME PRELIMINARY COMPUTATIONS

      NTDISP=TDISP/DT + 1.0001
      XS=0.0
      YS=0.0
      ZS=0.0
      IF(RL1.EQ.RL2) XS=RL1
      IF(RB1.EQ.RB2) YS=RB1
      IF(RH1.EQ.RH2) ZS=RH1
      QTOTAL=Q
      IF(NSOURS.NE.0) Q=1.0

      AT3D 005
      AT3D 010
      AT3D 015
      AT3D 020
      AT3D 025
      AT3D 030
      AT3D 035
      AT3D 040
      AT3D 045
      AT3D 050
      AT3D 055
      AT3D 060
      AT3D 065
      AT3D 070
      AT3D 075
      AT3D 080
      AT3D 085
      AT3D 090
      AT3D 095
      AT3D 100
      AT3D 105
      AT3D 110
      AT3D 115
      AT3D 120
      AT3D 125
      AT3D 130
      AT3D 135
      AT3D 140
      AT3D 145
      AT3D 150
      AT3D 155
      AT3D 160
      AT3D 165
      AT3D 170
      AT3D 175
      AT3D 180
      AT3D 185
      AT3D 190
      AT3D 195
      AT3D 200
      AT3D 205
      AT3D 210
      AT3D 215
      AT3D 220
      AT3D 225
      AT3D 230
      AT3D 235
      AT3D 240
      AT3D 245
      AT3D 250

```

APPENDIX C (continued)

```

C
      FACTOR=1.0/(CP*RHOW)
      IF(ICASE.EQ.2) FACTOR=1.0E3
      IF(ICASE.EQ.3) FACTOR=1.0E6
      RATIO=1.0
      IF(RL1.NE.RL2) RATIO=RATIO/(RL2-RL1)
      IF(RB1.NE.RB2) RATIO=RATIO/(RB2-RB1)
      IF(RH1.NE.RH2) RATIO=RATIO/(RH2-RH1)

C
C      ----- COMPUTE RETARDED VELOCITY, DISPERSION COEFFICIENTS, AND
C      ----- OTHER PARAMETERS
C
      RETARD=1.0 + RHOB*AKD/POR
      UF=HCOND*HGRAD/(POR*RETARD)
      AKX=AELONG*UF+AMTAU/(POR*RETARD)
      AKY=ATRANV*UF+AMTAU/(POR*RETARD)
      AKZ=AVERTI*UF+AMTAU/(POR*RETARD)
      RKE=(AKE/(PCR*RETARD))/AKZ
      ROTPAR=1.0E50
      IF(IDEF.NE.0) ROTPAR=RKE*DEPTH

C
      WRITE(6,1500) RETARD,UF,AKX,AKY,AKZ

C
C      ----- COMPUTE RTY(I) AND AIY(I) FOR FINITE WIDTH CASE
C
      IF(IWID.EQ.0) GO TO 180
      DO 130 I=1,NROOT
      RTY(I)=I*PAI/WIDTH
  130 AIY(I)=2.0/WIDTH

C
C      ----- WRITE OUT Y-EIGENVALUES AND Z-COEFFICIENTS
C
      IF(IBUG.EQ.0) GO TO 180
      WRITE(6,3100) (RTY(I),I=1,NROOT)
      WRITE(6,3200) (AIY(I),I=1,NROOT)

C
C      ----- COMPUTE RTZ(I) AND AIZ(I) FOR FINITE DEPTH CASE
C
  180 IF(IDEF.EQ.0) GO TO 290
C
C      ----- FOR THE THERMAL CASE, I.E. AKE NOT EQUAL TO 0.0
C
      IF(ICASE.NE.1) GO TO 250
      DO 200 I=1,NROOT
  200 CALL ROOT(RTZ,I,ROTPAR,MAXRUT)
      DO 210 I=1,NROOT
      RTZ(I) = RTZ(I)/DEPTH

      AT3D 255
      AT3D 260
      AT3D 265
      AT3D 270
      AT3D 275
      AT3D 280
      AT3D 285
      AT3D 290
      AT3D 295
      AT3D 300
      AT3D 305
      AT3D 310
      AT3D 315
      AT3D 320
      AT3D 325
      AT3D 330
      AT3D 335
      AT3D 340
      AT3D 345
      AT3D 350
      AT3D 355
      AT3D 360
      AT3D 365
      AT3D 370
      AT3D 375
      AT3D 380
      AT3D 385
      AT3D 390
      AT3D 395
      AT3D 400
      AT3D 405
      AT3D 410
      AT3D 415
      AT3D 420
      AT3D 425
      AT3D 430
      AT3D 435
      AT3D 440
      AT3D 445
      AT3D 450
      AT3D 455
      AT3D 460
      AT3D 465
      AT3D 470
      AT3D 475
      AT3D 480
      AT3D 485
      AT3D 490
      AT3D 495
      AT3D 500

```

APPENDIX C (continued)

```

DENOMT=DEPTH*(1.0+RKE**2/RTZ(I)**2) + RKE/RTZ(I)**2
210 AIZ(I)=2.0/DENOMT
      GO TO 285
C ----- FOR THE NON-THERMAL CASES
C
250 DO 260 I=1,NROOT
      RTZ(I)=I*PAI/DEPTH
260 AIZ(I)=2.0/DEPTH
C ----- WRITE OUT Z-EIGENVALUES AND Z-COEFFICIENTS
C
285 IF(BUG.EQ.0) GO TO 290
      WRITE(6,3300) (RTZ(I),I=1,NROOT)
      WRITE(6,3400) (AIZ(I),I=1,NROOT)
C ----- COMPUTE SOURCE PART OF EACH OF THE SERIES TERMS
C
C ----- COMPUTE SOURCE PART OF EACH OF Y-SERIES
C
290 IF(IWID.EQ.0) GO TO 310
      DO 300 I=1,NROOT
      IF(RB1.EQ.RB2) PSIS(I)=COS(RTY(I)*YS)
      IF(RB1.NE.RB2) PSIS(I)=(WIDTH/(I*PAI))*(SIN(RTY(I)*RB2) -
      > SINK(RTY(I)*RB1))
300 CONTINUE
C ----- COMPUTE SOURCE PART OF EACH OF Z-SERIES
C
310 IF(IDEP.EQ.0) GO TO 330
      DO 320 I=1,NROOT
      IF(RH1.EQ.RH2) PHIS(I)=COS(RTZ(I)*ZS)+RKE/RTZ(I)*SIN(RTZ(I)*ZS)
      IF(RH1.NE.RH2) PHIS(I)=(SIN(RTZ(I)*RH2)-SIN(RTZ(I)*RH1) -
      > RKE/RTZ(I)*(COS(RTZ(I)*RH2)-COS(RTZ(I)*PHI(I)))/RTZ(I))
320 CONTINUE
C ----- WRITE OUT THE YS-SERIES AND ZS-SERIES
C
330 IF(BUG.EQ.0) GO TO 350
      IF(IWID.NE.0) WRITE(6,3500) (PSIS(I),I=1,NROOT)
      IF(IDEP.NE.0) WRITE(6,3600) (PHIS(I),I=1,NROOT)
C ----- COMPUTE THE Y- AND Z-PART OF THE INTEGRAND
C ----- FOR EACH SERIES TERM
C
350 DO 490 IT=1,NEDT
      TIMED=(IT-1)*DT
      AT3D 505
      AT3D 510
      AT3D 515
      AT3D 520
      AT3D 525
      AT3D 530
      AT3D 535
      AT3D 540
      AT3D 545
      AT3D 550
      AT3D 555
      AT3D 560
      AT3D 565
      AT3D 570
      AT3D 575
      AT3D 580
      AT3D 585
      AT3D 590
      AT3D 595
      AT3D 600
      AT3D 605
      AT3D 610
      AT3D 615
      AT3D 620
      AT3D 625
      AT3D 630
      AT3D 635
      AT3D 640
      AT3D 645
      AT3D 650
      AT3D 655
      AT3D 660
      AT3D 665
      AT3D 670
      AT3D 675
      AT3D 680
      AT3D 685
      AT3D 690
      AT3D 695
      AT3D 700
      AT3D 705
      AT3D 710
      AT3D 715
      AT3D 720
      AT3D 725
      AT3D 730
      AT3D 735
      AT3D 740
      AT3D 745
      AT3D 750

```

APPENDIX C (continued)

```

      IF(IT.EQ.1) TIMED=DT          AT3D 755
C
      DO 440 IY=1,NY              AT3D 760
         Y=ZDIM(IY)                AT3D 765
C
C ----- TO EVALUATE THE FUNCTION Y1(Y,T;TAU) OR Y2(Y,T;TAU)    AT3D 770
C
      IF(IWID.EQ.0) GO TO 420      AT3D 775
      IF(IT.NE.1) GO TO 410        AT3D 780
      FCTY(IY,IT)=0.0              AT3D 785
      IF(RB1.EQ.RB2 .AND. Y.EQ.YS) FCTY(IY,IT)=1.0      AT3D 790
      IF((RB1.NE.RB2) .AND. (Y.GE.RB1 .AND. Y.LE.RB2))   AT3D 795
         FCTY(IY,IT)=1.0          AT3D 800
      GO TO 440                    AT3D 805
      CALL SERIEY(SERY,Y,YS,RB1,RB2,WIDTH,TIMED,AKY,RTY,AIY,
      PSIS,MAXRUT,NROOT)          AT3D 810
      IF(RB1.EQ.RB2) FCTY(IY,IT)=1.0/WIDTH+SERY          AT3D 815
      IF(RB1.NE.RB2) FCTY(IY,IT)=(RB2-RB1)/WIDTH+SERY      AT3D 820
      IF(RB1.EQ.0.0 .AND. RB2.EQ.WIDTH) FCTY(IY,IT)=1.0      AT3D 825
      IF(FCTY(IY,IT).LT.0.0) FCTY(IY,IT)=0.0              AT3D 830
      GO TO 440                    AT3D 835
C
C ----- TO EVALUATE THE FUNCTION Y3(Y,T;TAU) OR Y4(Y,T;TAU)    AT3D 840
C
C ----- TO COMPUTE FUNCTION Y3                                AT3D 845
C
      420     IF(RB1.NE.RB2) GO TO 430          AT3D 850
      IF(IT.NE.1) GO TO 425          AT3D 855
      FCTY(IY,IT)=0.0                AT3D 860
      IF(Y.EQ.YS) FCTY(IY,IT)=1.0      AT3D 865
      GO TO 440                    AT3D 870
      Y1=SQRT(4.0*PAI*AKY*TIMED)    AT3D 875
      EARG=(Y-YS)*(Y-YS)/(4.0*AKY*TIMED)          AT3D 880
      IF(ABS(EARG).GT.100.0) EARG=170.0          AT3D 885
      FCTY(IY,IT)=(1.0/Y1)*(EXP(-EARG))          AT3D 890
      GO TO 440                    AT3D 895
C
C ----- TO COMPUTE FUNCTION Y4                                AT3D 900
C
      430     IF(IT.NE.1) GO TO 435          AT3D 905
      FCTY(IY,IT)=0.0                AT3D 910
      IF(Y.GE.RB1 .AND. Y.LE.RB2) FCTY(IY,IT)=1.0      AT3D 915
      GO TO 440                    AT3D 920
      435     SRT=SQRT(4.0*AKY*TIMED)          AT3D 925
      FCTY(IY,IT)=(ERF((Y-RB1)/SRT)-ERF((Y-RB2)/SRT))/2.0  AT3D 930
      440     CONTINUE                      AT3D 935
C
      DO 480 IZ=1,NZ              AT3D 940
         Z=ZDIM(IZ)                AT3D 945

```

APPENDIX C (continued)

```

C ----- TO EVALUATE THE FUNCTION Z1(Z,T;TAU) OR Z2(Z,T;TAU)
C
C IF(IDEF.EQ.0) GO TO 460
C IF(IT.NE.1) GO TO 450
C FCTZ(IZ,IT)=0.0
C IF(RH1.EQ.RH2 .AND. Z.EQ.ZS) FCTZ(IZ,IT)=1.0
C IF((RH1.NE.RH2) .AND. (Z.GE.RH1 .AND. Z.LE.RH2))
C   FCTZ(IZ,IT)=1.0
C   GO TO 480
450  CALL SERIEZ(SERZ,Z,TIMED,AKZ,RKE,RTZ,AIZ,PHIS,MAXRUT,NRCOT)
C   FCTZ(IZ,IT)=SERZ
C   IF(AKE.EQ.0. .AND. RH1.EQ.RH2) FCTZ(IZ,IT)=1.0/DEPTH+SERZ
C   IF(AKE.EQ.0. .AND. RH1.NE.RH2) FCTZ(IZ,IT)=(RH2-RH1)/DEPTH+
C     SERZ
C   IF(RH1.EQ.0.0 .AND. RH2.EQ.DEPTH) FCTZ(IZ,IT)=1.0
C   GO TO 480
C ----- TO EVALUATE THE FUNCTION Z3(Z,T;TAU) OR Z4(Z,T;TAU)
C
C ----- TO COMPUTE FUNCTION Z3
C
460  IF(RH1.NE.RH2) GO TO 470
C   IF(IT.NE.1) GO TO 465
C   FCTZ(IZ,IT)=0.0
C   IF(Z.EQ.ZS) FCTZ(IZ,IT)=1.0
C   GO TO 480
C
465  AKZT=4.0*AKZ*TIMED
C   AKZTP1=AKZT*PAI
C   AKZT4S=AKZT/4.0
C   EARG1=(Z-ZS)*(Z-ZS)/AKZT
C   EARG2=(Z+ZS)*(Z+ZS)/AKZT
C   EARG3=AKZ*RKE*RKE*TIMED+RKE*(Z+ZS)
C   ARG=(Z+ZS)/SQRT(AKZT) + RKE*SQRT(AKZT4S)
C   TERM1=0.0
C   IF(EARG1.LT.100.0) TERM1=EXP(-EARG1)/SQRT(AKZTP1)
C   TERM2=0.0
C   IF(EARG2.LE.100.0) TERM2=EXP(-EARG2)/SQRT(AKZTP1)
C   TERM3=0.0
C   IF(EARG3.LT.100.0) TERM3=-RKE*EXP(EARG3)*(1.0-ERF(ARG))
C   FCTZ(IZ,IT)=TERM1+TERM2+TERM3
C   GO TO 480
C ----- TO COMPUTE FUNCTION Z4
C
470  IF(IT.NE.1) GO TO 475
C   FCTZ(IZ,IT)=0.0
C   IF(Z.GE.RH1 .AND. Z.LE.RH2) FCTZ(IZ,IT)=1.0

```

APPENDIX C (continued)

```

GO TO 480
C   475   AKZT1=SQRT(4.0*AKZ*TIMED)
          AKZT2=AKZT1/2.0
          ARG1=(Z+RH2)/AKZT1
          ARG2=(Z+RH1)/AKZT1
          ARG3=(Z-RH2)/AKZT1
          ARG4=(Z-RH1)/AKZT1
          ARG5=AKZ*RKE*RKE*TIMED + RKE*(Z+RH2)
          ARG6=AKZ*RKE*RKE*TIMED + RKE*(Z+RH1)
          TERMS4=0.5*(ERF(ARG1)-ERF(ARG2)-ERF(ARG3)+ERF(ARG4))
          TERMS=0.0
          IF(ARG5.LT.100.) TERMS=-EXP(ARG5)*(1.0-ERF(ARG1+RKE*AKZT2))
          TERM6=0.0
          IF(ARG6.LT.100.) TERM6=EXP(ARG6)*(1.0-ERF(ARG2+RKE*AKZT2))
          TERM7B=-(ERF(ARG1)-ERF(ARG2))
          FCTZ(IZ,IT)=TERMS4+TERMS+TERM6+TERM7B
C   480   CONTINUE
C   490   CONTINUE
C
C ----- START TRANSIENT LOOP COMPUTATION
C
C       TIME=0.0
C       DO 800 ITT=NBTI,NEDTI,NPRINT
C
C           DO 710 IX=1,NX
C               DO 710 IY=1,NY
C                   DO 710 IZ=1,NZ
C                       TEMPO(IX,IY,IZ)=TEMP(IX,IY,IZ)
C
C           IF(INTER.EQ.0) GO TO 725
C
C           IF(ICASE.EQ.1) WRITE(6,5100) TIME
C           IF(ICASE.EQ.2) WRITE(6,5200) TIME
C           IF(ICASE.EQ.3) WRITE(6,5300) TIME
C
C           DO 720 IZOUT=1,NZ
C               WRITE(6,6000) ZDIM(IZOUT)
C               CALL ALLOUT(TEMP,XDIM,YDIM,ZDIM,IZOUT,NX,NY,NZ,
C                           MAXNX,MAXNY,MAXNZ)
C
C           725   TIME=(ITT-1)*DT
C
C           DO 760 IXX=1,NX
C               X=XDIM(IXX)
C               DO 750 IYY=1,NY
C                   Y=YDIM(IYY)
C                   DO 740 IZZ=1,NZ
C
AT3D1255
AT3D1260
AT3D1265
AT3D1270
AT3D1275
AT3D1280
AT3D1285
AT3D1290
AT3D1295
AT3D1300
AT3D1305
AT3D1310
AT3D1315
AT3D1320
AT3D1325
AT3D1330
AT3D1335
AT3D1340
AT3D1345
AT3D1350
AT3D1355
AT3D1360
AT3D1365
AT3D1370
AT3D1375
AT3D1380
AT3D1385
AT3D1390
AT3D1395
AT3D1400
AT3D1405
AT3D1410
AT3D1415
AT3D1420
AT3D1425
AT3D1430
AT3D1435
AT3D1440
AT3D1445
AT3D1450
AT3D1455
AT3D1460
AT3D1465
AT3D1470
AT3D1475
AT3D1480
AT3D1485
AT3D1490
AT3D1495
AT3D1500

```

APPENDIX C (continued)

```

      Z=ZD1MR(IZZ)
C ----- BRANCH TO INSTANTANEOUS SOURCE OR CONTINUOUS SOURCE
C           IF(INSTAN) 731,732,731
C ----- FOR THE CASE OF CONTINUOUS SOURCE FOR THE DURATION OF NTDESP
C
    731      IF(ITT.LE.NTDESP) CALL TINTEGS,X,XS,RL1,RL2,
              FCTY,FCTZ,TIME,IYY,IZZ,ITT,UF,DT,AKX,RAMADA,QS,
              MAXNY,MAXNZ,MAXNTI,INSTAN)
    >          IF(ITT.GT.NTDESP) CALL TINTEGS,X,XS,RL1,RL2,
              FCTY,FCTZ,TIME,IYY+IZZ,NTDESP,UF,DT,AKX,RAMADA,QS,
              MAXNY,MAXNZ,MAXNTI,INSTAN)
    >          GO TO 733
C ----- FOR THE CASE OF INSTANTANEOUS SOURCE RELEASE
C
    732      CALL TINTEG(S,X,XS,RL1,RL2,FCTY,FCTZ,TIME,IYY,IZZ,ITT,
              UF,DT,AKX,RAMADA,QS,MAXNY,MAXNZ,MAXNTI,INSTAN)
    >          S=S*2.0/DT
    733      TEMP(IXX,IYY,IZZ)=S*X0*RATIO*FACTOR/(PDR*RETARD)
    740      CONTINUE
    750      CONTINUE
    760      CONTINUE
C
      IF(ITT.EQ.NBGT1) GO TO 800
      IF(INSOURS.NE.0) GO TO 800
C ----- CHECK IF STEADY STATE SOLUTION HAS BEEN OBTAINED
C ----- BEFORE THE FINAL SIMULATING TIME
C
      DIFMAX=0.0
      DO 770 IX=1,NX
      DO 770 IY=1,NY
      DO 770 IZ=1,NZ
          IF(TEMP(IX,IY,IZ).EQ.0.0) GO TO 770
          DIF=ABS(TEMP(IX,IY,IZ)/TEMPO(IX,IY,IZ)-1.0)
          IF(DIF.LE.DIFMAX) GO TO 770
          DIFMAX=DIF
    770      CONTINUE
C
      IF(DIFMAX.LE.ACCL) GO TO 910
C
      800 CONTINUE
C
      WRITE(6,7000)
      GO TO 920
  910  WRITE(6,8000)
  920  CONTINUE

```

AT3D1505
AT3D1510
AT3D1515
AT3D1520
AT3D1525
AT3D1530
AT3D1535
AT3D1540
AT3D1545
AT3D1550
AT3D1555
AT3D1560
AT3D1565
AT3D1570
AT3D1575
AT3D1580
AT3D1585
AT3D1590
AT3D1595
AT3D1600
AT3D1605
AT3D1610
AT3D1615
AT3D1620
AT3D1625
AT3D1630
AT3D1635
AT3D1640
AT3D1645
AT3D1650
AT3D1655
AT3D1660
AT3D1665
AT3D1670
AT3D1675
AT3D1680
AT3D1685
AT3D1690
AT3D1695
AT3D1700
AT3D1705
AT3D1710
AT3D1715
AT3D1720
AT3D1725
AT3D1730
AT3D1735
AT3D1740
AT3D1745
AT3D1750

APPENDIX C (continued)

```

IF( ICASE.EQ.1) WRITE(6,5100) TIME          AT3D1755
IF( ICASE.EQ.2) WRITE(6,5200) TIME          AT3D1760
IF( ICASE.EQ.3) WRITE(6,5300) TIME          AT3D1765
DO 930 IZOUT=1,NZ                         AT3D1770
      WRITE(6,6000) ZDIM(IZOUT)
930   CALL ALLOUT(TEMP,XDIM,YDIM,ZDIM,IZOUT,NX,NY,NZ,
      > MAXNX,MAXNY,MAXNZ)
C
      DO 950 IX=1,NX
      DO 950 IY=1,NY
      DO 950 IZ=1,NZ
950   TEMP(IX,IY,IZ)=0.0
      GO TO 999
C
9999 CONTINUE
C
10 FORMAT(20A4)
20 FORMAT(16I5)
30 FORMAT(8F10.0)
1000 FORMAT(1H1,///,5X,20A4,//)
1100 FORMAT(1H ,/5X,
      > *NO. OF POINTS IN X-DIRECTION ..... ,15/5X,
      > *NO. OF POINTS IN Y-DIRECTION ..... ,15/5X,
      > *NO. OF POINTS IN Z-DIRECTION ..... ,15/5X,
      > *NO. OF ROOTS! NO. OF SERIES TERMS ..... ,15/5X,
      > *NO. OF BEGINNING TIME STEPS ..... ,15/5X,
      > *NO. OF ENDING TIME STEP ..... ,15/5X,
      > *NO. OF TIME INTERVALS FOR PRINTED OUT SOLUTION ..... ,15/5X,
      > *INSTANTANEOUS SOURCE CONTROL = 0 FOR INSTANT SOURCE ,15/5X,
      > *SOURCE CONDITION CONTROL = 0 FOR STEADY SOURCE .... ,15/5X,
      > *INTERMITTENT OUTPUT CONTROL = 0 NO SUCH OUTPUT .... ,15/5X,
      > *CASE CONTROL = 1 THERMAL, = 2 FOR CHEMICAL, = 3 RAD ,15/)
1200 FORMAT(1H ,/5X,
      > *AQUIFER DEPTH, = 0.0 FOR INFINITE DEEP (METERS) ... ,E12.4/5X,
      > *AQUIFER WIDTH, = 0.0 FOR INFINITE WIDE (METERS) ... ,E12.4/5X,
      > *BEGIN POINT OF X-SOURCE LOCATION (METERS) ..... ,E12.4/5X,
      > *END POINT OF X-SOURCE LOCATION (METERS) ..... ,E12.4/5X,
      > *BEGIN POINT OF Y-SOURCE LOCATION (METERS) ..... ,E12.4/5X,
      > *END POINT OF Y-SOURCE LOCATION (METERS) ..... ,E12.4/5X,
      > *BEGIN POINT OF Z-SOURCE LOCATION (METERS) ..... ,E12.4/5X,
      > *END POINT OF Z-SOURCE LOCATION (METERS) ..... ,E12.4/5X)
1300 FORMAT(1H ,/5X,
      > *POROSITY ..... ,E12.4/5X,
      > *HYDRAULIC CONDUCTIVITY (METER/HOUR) ..... ,E12.4/5X,
      > *HYDRAULIC GRADIENT ..... ,E12.4/5X,
      > *LONGITIDUNAL DESPERSEIVITY (METER) ..... ,E12.4/5X,
      > *LATERAL DESPERSEIVITY (METER) ..... ,E12.4/5X,
      > *VERTICAL DESPERSEIVITY (METER) ..... ,E12.4/5X,
      > *DISTRIBUTION COEFFICIENT, KD (M**3/KG) ..... ,E12.4/5X,
      > *HEAT EXCHANGE COEFFICIENT (KCAL/HR-M**2-DEGREE C) .. ,E12.4/5X)

```

APPENDIX C (continued)

```

1400 FORMAT(1H ,/5X,
> "MOLECULAR DIFFUSION MULTIPLY BY TCROSITY (M**2/HR) ",E12.4/5X,
> "DECAY CONSTANT (PER HOUR) ..... ",E12.4/5X,
> "BULK DENSITY OF THE SOIL (GRAM/CM**3) ..... ",E12.4/5X,
> "ACCURACY TOLERANCE FOR REACHING STEADY STATE .....",E12.4/5X,
> "DENSITY OF WATER (KG/M**3) ..... ",E12.4/5X,
> "TIME INTERVAL SIZE FOR THE DESIRED SOLUTION (HR) .....",E12.4/5X,
> "DISCHARGE TIME (HR) ..... ",E12.4/5X,
> "WASTE RELEASE RATE (KCAL/HR), (KG/HR), OR (CL/HR) ",E12.4/)
1500 FORMAT(1H0,/5X,
> "RETARDATION FACTOR ..... ",E12.4/5X,
> "RETARDED DARCY VELOCITY (M/HR) ..... ",E12.4/5X,
> "RETARDED LONGITUDINAL DISPERSION COEF. (M**2/HR) .....",E12.4/5X,
> "RETARDED LATERAL DISPERSION COEFFICIENT (M**2/HR) .....",E12.4/5X,
> "RETARDED VERTICAL DISPERSION COEFFICIENT (M**2/HR) .....",E12.4/)
2000 FORMAT(1H0,4X,"LIST OF TRANSIENT SOURCE RELEASE RATE"/(5X,10E12.3)
> )
3100 FORMAT(1H1,4X,"LIST OF Y-EIGENVALUES"/(5X,10E12.4))
3200 FORMAT(1H0,4X,"LIST OF Y-COEFFICIENT"/(5X,10E12.4))
3300 FORMAT(1H1,4X,"LIST OF Z-EIGENVALUES"/(5X,10E12.4))
3400 FORMAT(1H0,4X,"LIST OF Z-COEFFICIENTS"/(5X,10E12.4))
3500 FORMAT(1H1,4X,"LIST OF YS-SERIES"/(5X,10E12.4))
3600 FORMAT(1H0,4X,"LIST OF ZS-SERIES"/(5X,10E12.4))
5100 FORMAT(1H1,4X,"TEMPERATURE DISTRIBUTION IN DEGREE C AT ",E12.4,
> " HOURS")
5200 FORMAT(1H1,4X,"DISTRIBUTION OF CHEMICALS IN PPS AT ",E12.4," HRS")
5300 FORMAT(1H1,4X,"DISTRIBUTION OF RAD WASTE IN PCT AT ",E12.4," HRS")
6900 FORMAT(1H0,20X,"Z = ",F10.2)
7000 FORMAT(1H0,"STEADY STATE SOLUTION HAS NOT BEEN REACHED BEFORE FINAL
> SIMULATING TIME//")
8000 FORMAT(1H0,"STEADY STATE SOLUTION HAS BEEN OBTAINED BEFORE FINAL
> SIMULATING TIME//")
      RETURN
      END

```

APPENDIX C (continued)

```

C      SUBROUTINE ROOT(RTZ,I,ROTPAR,MAXRUT)
C      DIMENSION RTZ(MAXRUT)

C      ZL=RTZ(I)
C      IF(I.GT.1) ZL=RTZ(I-1)+0.01
100   ZL=ZL+0.01
      FZL=ZL*SIN(ZL)-ROTPAR*COS(ZL)
      ZR=ZL+0.01
      FZR=ZR*SIN(ZR)-ROTPAR*COS(ZR)
      IF(FZL*FZR.LT.0.0) GO TO 200
      GO TO 100
200   FZL=ZL*SIN(ZL)-ROTPAR*COS(ZL)
      DO 300 J=1,6
      ZH=(ZL+ZR)/2.0
      FZH=ZH*SIN(ZH)-ROTPAR*COS(ZH)
      IF(FZH*FZL.LE.0.0) GO TO 400
      ZL=ZH
      FZL=FZH
      GO TO 300
400   ZR=ZH
300   CONTINUE
      RTZ(I)=(ZL+ZR)/2.0
      RETURN
      END

```

	ROOT 005
	ROOT 010
	ROOT 015
	ROOT 020
	ROOT 025
	ROOT 030
	ROOT 035
	ROOT 040
	ROOT 045
	ROOT 050
	ROOT 055
	ROOT 060
	ROOT 065
	ROOT 070
	ROOT 075
	ROOT 080
	ROOT 085
	ROOT 090
	ROOT 095
	ROOT 100
	ROOT 105
	ROOT 110
	ROOT 115
	ROOT 120
	ROOT 125

APPENDIX C (continued)

```

SUBROUTINE SERIEFY(SER,Y,YS,RB1,RB2,B,TIMED,AKY,RTY,AIY,
> PSIS,MAXRUT,NROOT)
C
DIMENSION RTY(MAXRUT),AIY(MAXRUT),PSIS(MAXRUT)
DIMENSION YTEUL(15)

C
EPS=0.0001
IER=1
I=1
M=1
N=1
ASSIGN 100 TO IFC
GO TO 500
100 YTEUL(1)=FCT
SUM=YTEUL(1)*0.5
3 J=0
4 I=I+1
IF(I-NROOT) 5,5,12
5 N=I
ASSIGN 200 TO IFC
GO TO 500
200 AMN=FCT
DO 6 K=1,M
AMP=(AMN+YTEUL(K))*0.5
YTEUL(K)=AMN
6 AMN=AMP
IF(ABS(AMN)-ABS(YTEUL(M))) 7,9,9
7 IF(M-15) 8,9,9
8 M=M+1
YTEUL(M)=AMN
AMN=0.5*AMN
9 SUM=SUM+AMN
IF(ABS(AMN)-EPS*ABS(SUM)) 10,10,3
10 J=J+1
IF(J-5) 4,11,11
11 IER=0
12 SER=SUM
IF(IER.NE.0) WRITE(6,1000) Y,TIMED
RETURN
C
----- TO EVALUATE N-TH TERM OF Y1(Y,T;TAU) OR Y2(Y,T;TAU)
CCC
500 AKYTB=AKY*TIMED/(B*B)
IF(AKYTB.LE.0.0000014) GO TO 510
EARG=RTY(N)*RTY(N)*AKY*TIMED
IF(EARG.GT.100.0) FCT=0.0
IF(EARG.LE.100) FCT=AIY(N)*(COS(RTY(N)*Y))*PSIS(N)*EXP(-EARG)
GO TO 590
510 IF(RB1.NE.RB2) GO TO 520
AKYTP=4.0*3.141593*AKY*TIMED
      SERY 005
      SERY 010
      SERY 015
      SERY 020
      SERY 025
      SERY 030
      SERY 035
      SERY 040
      SERY 045
      SERY 050
      SERY 055
      SERY 060
      SERY 065
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      SERY 080
      SERY 085
      SERY 090
      SERY 095
      SERY 100
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      SERY 110
      SERY 115
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      SERY 125
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      SERY 150
      SERY 155
      SERY 160
      SERY 165
      SERY 170
      SERY 175
      SERY 180
      SERY 185
      SERY 190
      SERY 195
      SERY 200
      SERY 205
      SERY 210
      SERY 215
      SERY 220
      SERY 225
      SERY 230
      SERY 235
      SERY 240
      SERY 245
      SERY 250

```

APPENDIX C (continued)

```

AKYT=4.0*AKY*TIMED          SERY 255
EARG1=((Y-YS)-2.0*N*B)*((Y-YS)-2.0*N*B)/AKYT      SERY 260
EARG2=((Y-YS)-2.0*(N-1)*B)*((Y-YS)-2.0*(N-1)*B)/AKYT  SERY 265
EARG3=((Y+YS)-2.0*(N+1)*B)*((Y+YS)-2.0*(N+1)*B)/AKYT  SERY 270
EARG4=((Y+YS)-2.0*N*B)*((Y+YS)-2.0*N*B)/AKYT        SERY 275
FCT=(EXP(-EARG1)+EXP(-EARG2)+EXP(-EARG3)+EXP(-EARG4))/SQRT(AKYTP1)  SERY 280
GO TO 590                  SERY 285
520 AKY=SQRT(4.0*AKY*TIMED)  SERY 290
ARG1=Y-RB1-2.0*N*B          SERY 295
ARG2=Y-RB2-2.0*N*B          SERY 300
ARG3=Y-RB1-2.0*(N-1)*B      SERY 305
ARG4=Y-RB2-2.0*(N-1)*B      SERY 310
ARG5=Y+RB1-2.0*(N+1)*B      SERY 315
ARG6=Y+RB2-2.0*(N+1)*B      SERY 320
ARG7=Y+RB1-2.0*N*B          SERY 325
ARG8=Y+RB2-2.0*N*B          SERY 330
FCT=0.5*(ERF(ARG1)-ERF(ARG2)+ERF(ARG3)-ERF(ARG4)      SERY 335
> -ERF(ARG5)+ERF(ARG6)-ERF(ARG7)+ERF(ARG8))          SERY 340
590 GO TO IFC, (100,200)     SERY 345
C 1000 FORMAT(1H0,10X,'WARNING: SERIESY AT Y =',F8.2,' TIMED=',F8.2,','
1 NEED'S MORE TERMS')       SERY 350
END                         SERY 355
                                SERY 360
                                SERY 365

```

APPENDIX C (continued)

```

C      SUBROUTINE SERIEZ(SER,Z,TIMED,AKZ,RKE,RTZ,AIZ,PHIS,MAXRUT,NROOT)
C
C      DIMENSION RTZ(MAXRUT),AIZ(MAXRUT),PHIS(MAXRUT)
C      DIMENSION YTEUL(15)
C
C      EPS=0.0001
C      IER=1
C      I=1
C      M=1
C      N=1
C      ASSIGN 100 TO IFC
C      GO TO 500
100  YTEUL(1)=FCT
      SUM=YTEUL(1)*0.5
      3 J=0
      4 I=I+1
      IF(I-NROOT) 5,5,12
      5 N=
      ASSIGN 200 TO IFC
      GO TO 500
200  AMN=FCT
      DO 6 K=1,M
      AMP=(AMN+YTEUL(K))*0.5
      YTEUL(K)=AMN
      6 AMN=AMP
      IF(ABS(AMN)-ABS(YTEUL(M))) 7,9,9
      7 IF(M-15) 8,9,9
      8 M=M+1
      YTEUL(M)=AMN
      AMN=0.5*AMN
      9 SUM=SUM+AMN
      IF(ABS(AMN)-EPS*ABS(SUM)) 10,10,3
      10 J=J+1
      IF(J-5) 4,11,11
      11 IER=0
      12 SER=SUM
      IF(IER.NE.0) WRITE(6,1000) Z,TIMED
      RETURN
C
C      ----- TO EVALUATE THE N-TH TERM OF Z1(Z,T;TAU) OR Z2(Z,T;TAU)
C
500  EARG=RTZ(N)**2*AKZ*TIMED
      IF(EARG.GT.100.0) FCT=0.0
      IF(EARG.LE.100) FCT=AIZ(N)*(COS(RTZ(N)*Z)+RKE/RTZ(N)*
      SIN(RTZ(N)*Z))*PHIS(N)*EXP(-EARG)
      GO TO IFC, (100,200)
C
1000 FORMAT(1H0,10X,'WARNING: SERIESZ AT Z =',F8.2,' TIMED=',F8.2,'
      NEEDS MORE TERMS')
      END

```

APPENDIX C (continued)

```

SUBROUTINE TINTEGR(S,X,XS,RL1,RL2,FCTY,FCTZ,TIME,IYY,IZZ,ITT,
> UF,DT,AKX,RANADA,QS, MAXNY,MAXNZ,MAXNTI,INSTAN)          TINT 005
C
C
DIMENSION FCTY(MAXNY,MAXNTI),FCTZ(MAXNZ,MAXNTI),QS(MAXNTI)      TINT 010
C
PAI=3.1415927
ITTM1=ITT-1
N=ITTM1/2
SUMEND=0.0
SUMMID=0.0
S=0.0
ITAU=1
ASSIGN 100 TO M
GO TO 800
100 FIT1=FIT
C
----- IF N .LT. 1, THEN THERE IS ONLY ONE INTERVAL
CCC
IF(INSTAN.EQ.0) GO TO 700
IF(N.LT.1) GO TO 700
DO 400 K=1,N
ASSIGN 200 TO M
ITAU=K+K-1
GO TO 800
200 SUMEND=SUMEND+FIT
ASSIGN 300 TO M
ITAU=K+K
GO TO 800
300 SUMMID=SUMMID+FIT
400 CONTINUE
C
----- IF N#2 .NE. ITTM1, THEN THERE ARE ODD NUMBERS OF INTERVALS
CCC
IF(N#2 .NE. ITTM1) GO TO 500
S=(2.0*SUMEND+4.0*SUMMID-FIT1)*DT/3.0
GO TO 900
500 ASSIGN 600 TO M
ITAU=ITTM1
GO TO 800
600 S=(2.0*SUMEND+4.0*SUMMID-FIT1+FIT1)*DT/3.0
700 S=S+(FIT1)*DT/2.0
GO TO 900
CCC
----- COMPUTE FUNCTION VALUE OF THE INTEGRAND
----- FUNCTION F(ITAU)
CCC
----- TO EVALUATE THE FUNCTION X1(X,T;TAU) OR X2(X,T;TAU)
C

```

APPENDIX C (continued)

```

500 XPART=0.0
      TIMD=TIME-(ITAU-1)*DT
      IF(ITAU.EQ.ITT) TIMD=0.01*DT
C ----- POINT SOURCE IN THE X-DIRECTION
C
      IF(RL1.NE.RL2) GO TO 820
      IF(ITAU.NE.ITT) GO TO 810
      XPART=0.0
      IF(X.EQ.XS) XPART=1.0
      GO TO 850
810 EARG=((X-XS)-UF*TIMD)**2/(4.0*AKX*TIMD)
      IF(ABS(EARG).GT.150.) GO TO 850
      XPART=(1.0/(SQRT(4.0*PA1*AKX*TIMD)))*EXP(-EARG)
      GO TO 850
C ----- LINE SOURCE IN THE X-DIRECTION
C
820 IF(ITAU.NE.ITT) GO TO 830
      XPART=0.0
      IF(X.GE.RL1 .AND. X.LE.RL2) XPART=0.0
      GO TO 850
830 SRT=SQRT(4.0*AKX*TIMD)
      EAR=-UF*TIMD
      EARG1=(X-RL1+EAR)/SRT
      EARG2=(X-RL2+EAR)/SRT
      XPART=(ERF(EARG1)-ERF(EARG2))/2.0
C ----- TO EVALUATE THE INTEGRAND, F1JK(X,Y,Z,T;TAU), IN EQ. 16
C
850 IT=ITT-ITAU + 1
      FIT=XPART*FCTZ(IZZ,IT)*FCTY(IYY,IT)*QS(ITAU)*EXP(-RAMADAR*TIMD)
      GO TO M,(100,200,300,600)
900 RETURN
      END

```

TINT	255
TINT	260
TINT	265
TINT	270
TINT	275
TINT	280
TINT	285
TINT	290
TINT	295
TINT	300
TINT	305
TINT	310
TINT	315
TINT	320
TINT	325
TINT	330
TINT	335
TINT	340
TINT	345
TINT	350
TINT	355
TINT	360
TINT	365
TINT	370
TINT	375
TINT	380
TINT	385
TINT	390
TINT	395
TINT	400
TINT	405
TINT	410
TINT	415
TINT	420
TINT	425

APPENDIX C (continued)

```

SUBROUTINE ALLOUT(FTV,XDIM,YDIM,ZDIM,IZ,NX,NY,NZ,
> MAXNX,MAXNY,MAXNZ)
C
C      DIMENSION FTV(MAXNX,MAXNY,MAXNZ)
C      DIMENSION XDIM(MAXNX),YDIM(MAXNY),ZDIM(MAXNZ)
C
C      JOUT=(NX-1)/10+1
DO 96 MM=1,JOUT
JAA=10*(MM-1)+1
JZZ=10*MM
IF(MM.EQ.JOUT) JZZ=NX
IF(MM.GT.1) WRITE(6,225)
225 FORMAT(1H0,50X,'CONTINUE')
WRITE(6,222) (XDIM(J),J=JAA,JZZ)
222 FORMAT(1H ,60X,'X'//X,' Y ',10F12.0)
WRITE(6,223)
223 FORMAT(1H , '   ,10(4X,'        '))
DO 97 NN=1,NY
Y=YDIM(NN)
WRITE(6,224) Y, (FTV(J,NN,IZ),J=JAA,JZZ)
224 FORMAT(1H,F5.0,10E12.3)
97 CONTINUE
96 CONTINUE
RETURN
END

IHC002 I STOP      0

```

ALLO	005
ALLO	010
ALLO	015
ALLO	020
ALLO	025
ALLO	030
ALLO	035
ALLO	040
ALLO	045
ALLO	050
ALLO	055
ALLO	060
ALLO	065
ALLO	070
ALLO	075
ALLO	080
ALLO	085
ALLO	090
ALLO	095
ALLO	100
ALLO	105
ALLO	110
ALLO	115
ALLO	120
ALLO	125

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