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## AEC RESEARCH AND DEVELOPMENT REPORT

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## CURIUM DATA SHEETS

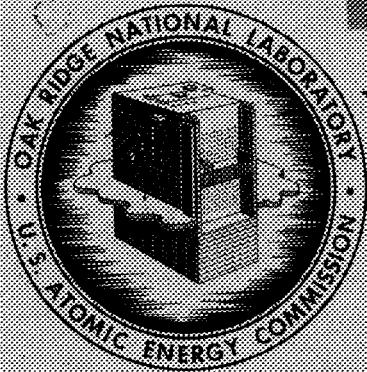
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ORNL-4044

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ISOTOPES DEVELOPMENT CENTER

CURIUM DATA SHEETS

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ISOTOPES DIVISION

NOVEMBER 1966

OAK RIDGE NATIONAL LABORATORY  
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CURIUM DATA SHEETSI. CURIUM-244REFERENCE COLUMNA. CURIUM-244 METAL

HALF-LIFE: 18.1 y

1

1. Compositiona. Radionuclidic abundance

3

<u>Element</u>	<u>Minimum, %</u>	<u>Maximum, %</u>
Cm	99.5	99.8
Am	0.5	0.2

An average  $^{244}\text{Cm}$  product will have the following analysis:

<u>Isotope</u>	<u>% Abundance</u>
$^{244}\text{Cm}$	95.5
$^{245}\text{Cm}$	1.6
$^{246}\text{Cm}$	2.7
$^{243}\text{Am}$	0.2

b. Radiochemical purity

Because of their long half-lives, the  $^{245}\text{Cm}$  ( $T_{1/2} = 8000$  y),  $^{246}\text{Cm}$  ( $T_{1/2} = 6600$  y), and  $^{243}\text{Am}$  ( $T_{1/2} = 8000$  y) impurities act as inert diluents and contribute <0.1% of the total source power.

The radiations from these impurities are weak gammas or alpha particles and can be neglected because they are readily shielded. The prompt gammas and neutrons from the spontaneous fission will be only a few percent of that obtained from spontaneous fission of  $^{244}\text{Cm}$ .

Since the  $^{244}\text{Cm}$  decays to  $^{240}\text{Pu}$ , the plutonium content in the sample will slowly build up after the final purification step as shown in the following table.

<u>Time, months</u>	<u><math>^{240}\text{Pu, %}</math></u>
0	0
7.2	2.7
18	6.4
36	12.3
90	27.8

REFERENCE COLUMN2. Specific Power

- a. 2.67 watts/g of metal (95.5%  $^{244}\text{Cm}$  content) 2, 3, 4

It is assumed that there are 81 curies/g of  $^{244}\text{Cm}$  and that there are 34.3 watts/kilocurie of  $^{244}\text{Cm}$ .

- b. 77.4 curies of  $^{244}\text{Cm}$  per gram of metal 2, 3, 4

3. Radiation

- a. Alpha particles 2, 5

Nuclide	Max E, Mev	Avg E, Mev	Abundance, %	w/kilocurie	Particles w <sup>-1</sup> sec <sup>-1</sup>
$^{244}\text{Cm}$	5.801	5.801	76.7	34.3	$0.825 \times 10^{12}$
	5.759	5.759	23.3	—	$0.252 \times 10^{12}$
Total alpha power				34.3	

The volume of helium from alpha decay as a function of decay time is given in the following table.

Volume of Helium as a Function of Decay Time

cm <sup>3</sup> of He per g of $^{244}\text{Cm}$ (standard conditions)	Time Years	Time Half-lives
6.15	1.8	0.1
11.8	3.6	0.2
17.3	5.4	0.3
22.1	7.2	0.4
26.9	9.1	0.5
31.2	10.9	0.6
35.3	12.7	0.7
39.1	14.5	0.8
42.6	16.3	0.9
45.9	18.1	1.0
59.3	27.1	1.5
68.9	36.2	2.0
80.3	54.3	3.0
86.1	72.4	4.0
88.9	90.5	5.0
91.7	181.0	10.0

REFERENCE COLUMN

- b. Beta particles - none
- c. Gamma

The gammas come from three sources. First there are the gammas associated with the alpha decay of  $^{244}\text{Cm}$ . Secondly, there are the prompt gammas from spontaneous fission. The fission-product gammas constitute the third gamma source. The gamma-emission rates are given in the following table.

2, 3, 5

Gamma-emission rate, photons sec <sup>-1</sup> w <sup>-1</sup> of $^{244}\text{Cm}$	Photon energy, Mev
<u><math>^{244}\text{Cm}</math> gammas</u>	
0.252 x 10 <sup>12</sup>	0.042
5.80 x 10 <sup>7</sup>	0.10
1.40 x 10 <sup>7</sup>	0.15
<u>Prompt gammas from spontaneous fission</u>	
4.34 x 10 <sup>6</sup>	1.0
1.084 x 10 <sup>6</sup>	1.5
1.15 x 10 <sup>6</sup>	2.3
2.03 x 10 <sup>5</sup>	3.0
2.71 x 10 <sup>5</sup>	5.0
<u>Fission-product gammas</u>	
3.84 x 10 <sup>6</sup>	0.63
1.42 x 10 <sup>6</sup>	1.1
1.66 x 10 <sup>6</sup>	1.55
3.20 x 10 <sup>5</sup>	2.38
4.73 x 10 <sup>5</sup>	2.75

- d. Bremsstrahlung - none
- e. Neutrons

$4.19 \times 10^6$  neutrons sec<sup>-1</sup> w<sup>-1</sup> of  $^{244}\text{Cm}$   
from spontaneous fission  
(Half-life for spontaneous fission is  
 $1.4 \times 10^7$  y)

5, 6, 7

$1.51 \times 10^5$  neutrons sec<sup>-1</sup> w<sup>-1</sup> of  $^{244}\text{Cm}$   
from ( $\alpha, n$ ) reaction on oxygen  
in  $\text{Cm}_2\text{O}_3$

5

REFERENCE COLUMN

The energy distribution of spontaneous fission neutrons from  $^{244}\text{Cm}$  is given in the following table.

3

Spontaneous Fission Neutrons From Curium-244

Energy, MeV	Abundance, neutrons sec <sup>-1</sup> w <sup>-1</sup> of $^{244}\text{Cm}$
0.3-0.4	1.51 x 10 <sup>5</sup>
0.4-0.6	3.13 x 10 <sup>5</sup>
0.6-0.8	3.20 x 10 <sup>5</sup>
0.8-1.0	2.77 x 10 <sup>5</sup>
1.0-1.2	2.84 x 10 <sup>5</sup>
1.2-1.4	2.80 x 10 <sup>5</sup>
1.4-1.6	2.44 x 10 <sup>5</sup>
1.6-1.8	2.19 x 10 <sup>5</sup>
1.8-2.0	1.98 x 10 <sup>5</sup>
2.0-2.2	1.80 x 10 <sup>5</sup>
2.2-2.4	1.65 x 10 <sup>5</sup>
2.4-2.6	1.58 x 10 <sup>5</sup>
2.6-2.8	1.30 x 10 <sup>5</sup>
2.8-3.0	1.08 x 10 <sup>5</sup>
3.0-3.2	1.01 x 10 <sup>5</sup>
3.2-3.4	0.97 x 10 <sup>5</sup>
3.4-3.6	0.93 x 10 <sup>5</sup>
3.6-3.8	0.75 x 10 <sup>5</sup>
3.8-4.0	0.79 x 10 <sup>5</sup>
4.0-4.4	1.04 x 10 <sup>5</sup>
4.4-4.8	0.86 x 10 <sup>5</sup>
4.8-5.2	0.65 x 10 <sup>5</sup>
5.2-5.6	0.50 x 10 <sup>5</sup>
5.6-6.0	0.40 x 10 <sup>5</sup>
6.0-6.4	2.95 x 10 <sup>4</sup>
6.4-6.8	2.12 x 10 <sup>4</sup>
6.8-7.2	1.47 x 10 <sup>4</sup>
7.2-7.6	1.12 x 10 <sup>4</sup>
7.6-8.0	0.90 x 10 <sup>4</sup>
8.0-8.8	1.01 x 10 <sup>4</sup>
8.8-9.6	2.95 x 10 <sup>3</sup>
9.6-10.4	3.1 x 10 <sup>3</sup>
10.4-11.2	2.05 x 10 <sup>3</sup>
11.2-12.8	1.40 x 10 <sup>3</sup>

REFERENCE COLUMN

The energy distribution of neutrons occurring as a result of the collision of fast alpha particles from  $^{244}\text{Cm}$  decay with oxygen atoms in  $\text{Cm}_2\text{O}_3$  is given in the following table. 3

Neutrons From ( $\alpha$ ,n) Reactions With Oxygen

Energy, Mev	Abundance, neutrons sec <sup>-1</sup> w <sup>-1</sup> of $^{244}\text{Cm}$
0.2	$1.62 \times 10^2$
0.4	$0.68 \times 10^3$
0.6	$0.83 \times 10^3$
0.8	$1.69 \times 10^3$
1.0	$2.70 \times 10^3$
1.2	$0.43 \times 10^4$
1.4	$0.61 \times 10^4$
1.6	$0.83 \times 10^4$
1.8	$1.01 \times 10^4$
2.0	$1.19 \times 10^4$
2.2	$1.33 \times 10^4$
2.4	$1.40 \times 10^4$
2.6	$1.40 \times 10^4$
2.8	$1.37 \times 10^4$
3.0	$1.22 \times 10^4$
3.2	$1.01 \times 10^4$
3.4	$0.79 \times 10^4$
3.6	$0.50 \times 10^4$
3.8	$3.02 \times 10^3$
4.0	$2.01 \times 10^3$
4.2	$1.37 \times 10^3$
4.4	$0.86 \times 10^3$
4.6	$0.72 \times 10^2$

4. Critical Mass

The critical mass of unreflected and reflected spheres of  $^{244}\text{Cm}$  and  $^{244}\text{Cm}_2\text{O}_3$  have been calculated by C. W. Craven, Jr., at ORNL using the cross-section data available as of November 1965. The results, shown in the following table, agree within 10% of the results obtained in the replacement experiment at Los Alamos. 8

REFERENCE COLUMNCalculated Critical Mass of  $^{244}\text{Cm}$  and  $^{244}\text{Cm}_2\text{O}_3$ 

Core Mixture	Density, g/cm <sup>3</sup>	Reflector		Critical mass, kg	Critical radius, cm
		Mixture	Thickness, cm		
Cm <sup>a</sup>	14.0	Bare	--	12.5	5.97
Cm <sub>2</sub> O <sub>3</sub> <sup>a</sup>	10.60	Bare	--	21.1	7.8031
Cm <sub>2</sub> O <sub>3</sub>	9.01	Bare	--	29.2	9.1803
Cm <sub>2</sub> O <sub>3</sub>	10.60	Au-H <sub>2</sub> O	4.0-15.0	11.9	6.4540
Cm <sub>2</sub> O <sub>3</sub>	10.60	Au-H <sub>2</sub> O	2.0-7.5	13.5	6.7188
Cm <sub>2</sub> O <sub>3</sub>	10.60	Au-H <sub>2</sub> O	0.5-2.0	16.5	7.1966

Critical Mass Equations

$$\text{Cm: } M_C = 2450/\rho^2 \text{ (kg)} \quad \text{Cm}_2\text{O}_3: M_C = 2370/\rho^2 \text{ (kg)}$$

<sup>a</sup>Assumed composition: 98.07 wt %  $^{244}\text{Cm}$  and 1.93 wt %  $^{241}\text{Pu}$ .

5. Compatibility With Materials of Containment6. Thermophysical Properties

## a. Density

13.51 g/cm<sup>3</sup> of metal

9

## b. Coefficient of thermal expansion

$$\alpha_a = 7.5 \times 10^{-6}/^\circ\text{C}$$

10 (Am)

$$\alpha_c = 6.2 \times 10^{-6}/^\circ\text{C}$$

## c. Specific heat and enthalpy

## (1) Specific heat

$$0.0270 \text{ cal g}^{-1} \text{ }^\circ\text{C}^{-1}$$

11 (Nd)

## (2) Enthalpy in calories

$$H_t - H_0 = 6.48 + 3.53 \times 10^{-3} t^2 + 1.49 \times 10^{-6} t^3$$

12 (Nd)

(Nd temperature is 0-400°C and  
t is in °C)

## d. Temperatures of phase transformations

(1) Melting point = 1340°C

9

(2) Boiling point = 3100°C

13

(Average of terbium and gadolinium  
boiling points)

REFERENCE COLUMN

e.	Latent heats of phase transformations $\Delta H$ fusion 37.5 kcal/mole (Richard's rule)	11
	$\Delta H$ vaporization 77.0 kcal/mole (Trouton's rule)	11
f.	Vapor pressure $\log_{10} P = 8.4 - 18,400/T$ (T is in °K and P is in torr)	14
	This is an average of neodymium, gadolinium, and terbium.	
g.	Thermal conductivity 0.021 cal $\text{cm}^{-1}$ $\text{sec}^{-1}$ $^{\circ}\text{C}^{-1}$ at 26°C	15 (Gd)
h.	Thermal diffusivity 0.575 $\text{cm}^2/\text{sec}$ at 26°C This value was calculated by dividing the product of the specific heat and density into the thermal conductivity.	
i.	Viscosity 2.5 centipoises at 1340°C	16
j.	Surface tension 500 dyn/cm	17
k.	Total hemispherical emittance 0.37 at 89°C	18 (Pu)
l.	Spectral emissivity 0.55 A higher value of 0.9 can be assumed if the metal surface is oxidized or if impurities are present.	19 (Er)
m.	Crystallography double hexagonal close packed $a = 3.496 \pm 0.003 \text{ \AA}$ $c = 11.331 \pm 0.005 \text{ \AA}$	9
n.	Solubilities Reacts strongly with water	20
o.	Diffusion rates	

REFERENCE COLUMN7. Mechanical Properties

## a. Hardness

Vicker's - 97.7 13 (Dy)

## b. Crush strength

7741 kg/cm<sup>2</sup> 13 (Tm)8. Chemical Properties

## a. Heat and free energy of formation, entropy

## (1) Heat of formation

Zero - by definition of standard state

## (2) Free energy of formation

Zero - by definition of standard state

## (3) Entropy (temperature)

S<sub>298</sub><sup>o</sup> = 15 cal °C<sup>-1</sup> mole<sup>-1</sup> 22 (Am)

## b. Chemical reactions and reaction rates

(oxygen, nitrogen, water, steam, hydrogen, liquid metals, other)

(1) Oxygen at room temperature - slow 9

(2) Oxygen at elevated temperature - fast 9

(3) Nitrogen at room temperature - very slow 23

(4) Nitrogen at elevated temperature - slow 23

(5) Water at room temperature - fast 20

(6) Hydrogen at room temperature - slow 20

(7) Hydrogen at elevated temperature - fast 20

9. Biological TolerancesMaximum permissible body burdens and maximum permissible concentrations of <sup>244</sup>Cm in air and water are shown in the table on the following page. 2410. Shielding Data

Gamma dose rates with water, iron, lead, and uranium shielding are given in Figs. 1-5 for <sup>244</sup>Cm power sources of 100, 200, 500, 1000, 2000, 5000, 10,000, and 20,000 watts. Neutron dose rates with water shielding are given in Fig. 6. Neutron dose rates on shielding with Be, CH, CH<sub>2</sub>, or LiH can be estimated by using Fig. 6 in conjunction with Fig. 7.

Maximum Permissible Body Burdens and Maximum Permissible Concentrations  
for Radionuclides in Air and in Water for Occupational Exposure<sup>24</sup>

Radionuclide and type of decay	Organ of reference (critical organ underscored)	Max. permissible burden in total body, g(uc)	Maximum permissible concentrations, $\mu\text{c}/\text{cm}^3$			
			For 40-hr week		For 168-hr week	
			Water	Air	Water	Air
$^{96}\text{Cm}^{244}$  $(\alpha, \gamma)$	Bone	0.1	$2 \times 10^{-4}$	$9 \times 10^{-12}$	$7 \times 10^{-5}$	$3 \times 10^{-12}$
	Liver	0.2	$3 \times 10^{-4}$	$10^{-11}$	$9 \times 10^{-5}$	$4 \times 10^{-12}$
	(Sol) Kidney	0.2	$4 \times 10^{-4}$	$2 \times 10^{-11}$	$10^{-4}$	$6 \times 10^{-12}$
		0.3	$6 \times 10^{-4}$	$3 \times 10^{-11}$	$2 \times 10^{-4}$	$9 \times 10^{-12}$
	Total Body	0.3	$8 \times 10^{-4}$	$2 \times 10^{-7}$	$3 \times 10^{-4}$	$6 \times 10^{-8}$
	GI (LLI)*					
(Insol)	Lung			$10^{-10}$		$3 \times 10^{-11}$
	GI (LLI)*		$8 \times 10^{-4}$	$10^{-7}$	$3 \times 10^{-4}$	$5 \times 10^{-8}$

\*The abbreviations GI and LLI refer to the gastrointestinal tract and lower large intestine, respectively.

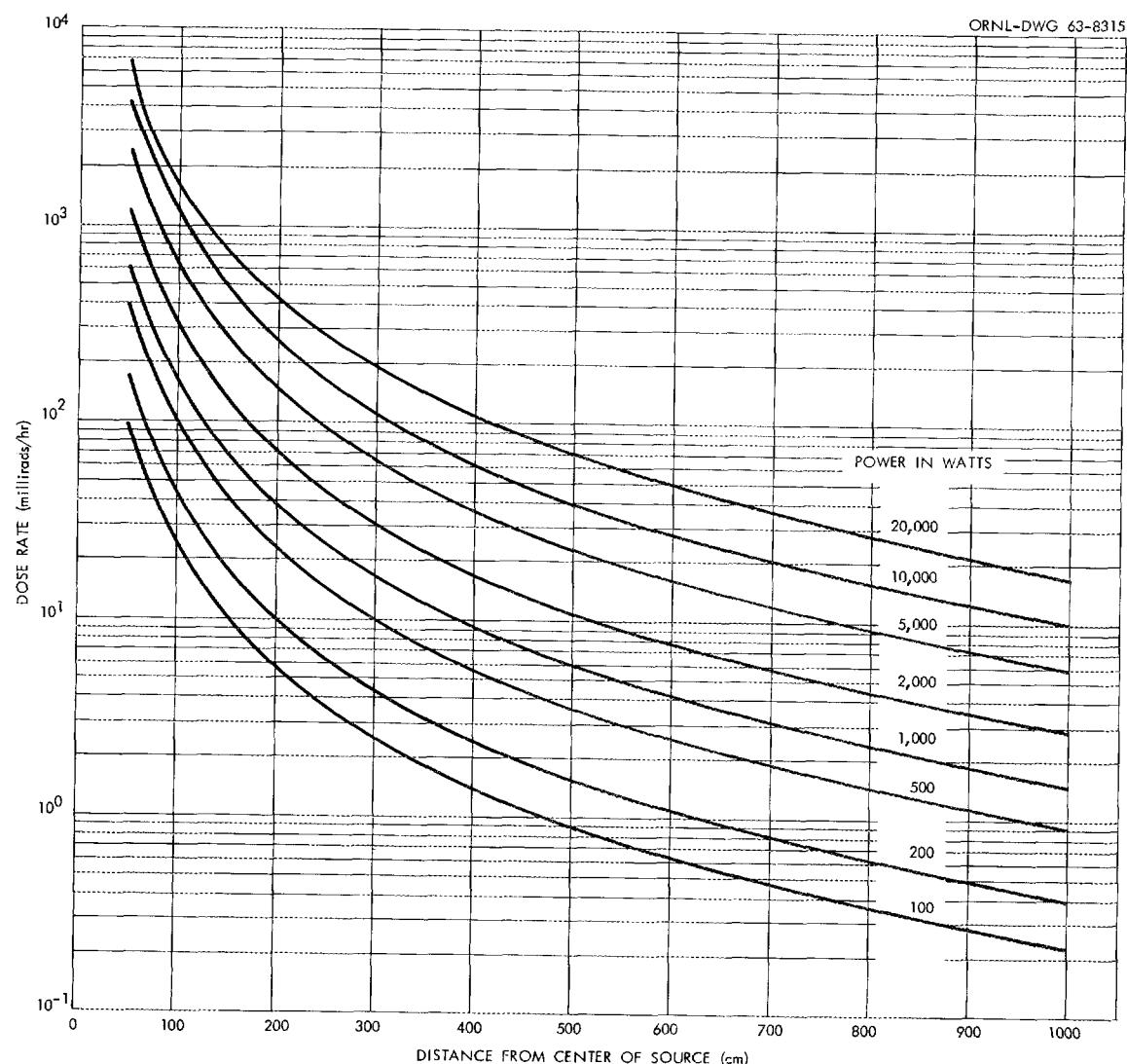


Fig. 1. Gamma Dose Rates From Unshielded Isotopic Power Sources of Curium-244 as a Function of Distance From Center of Source.

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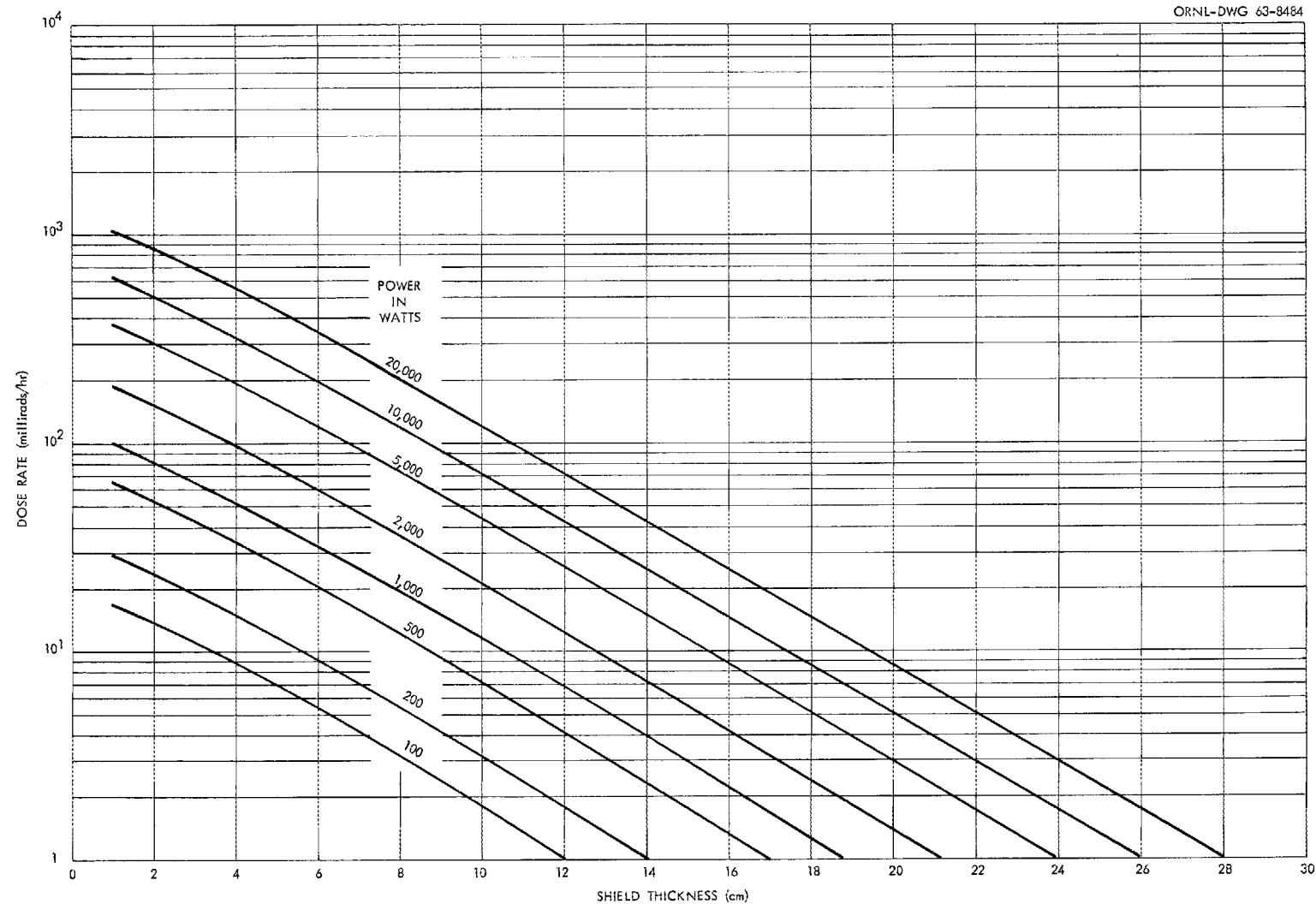
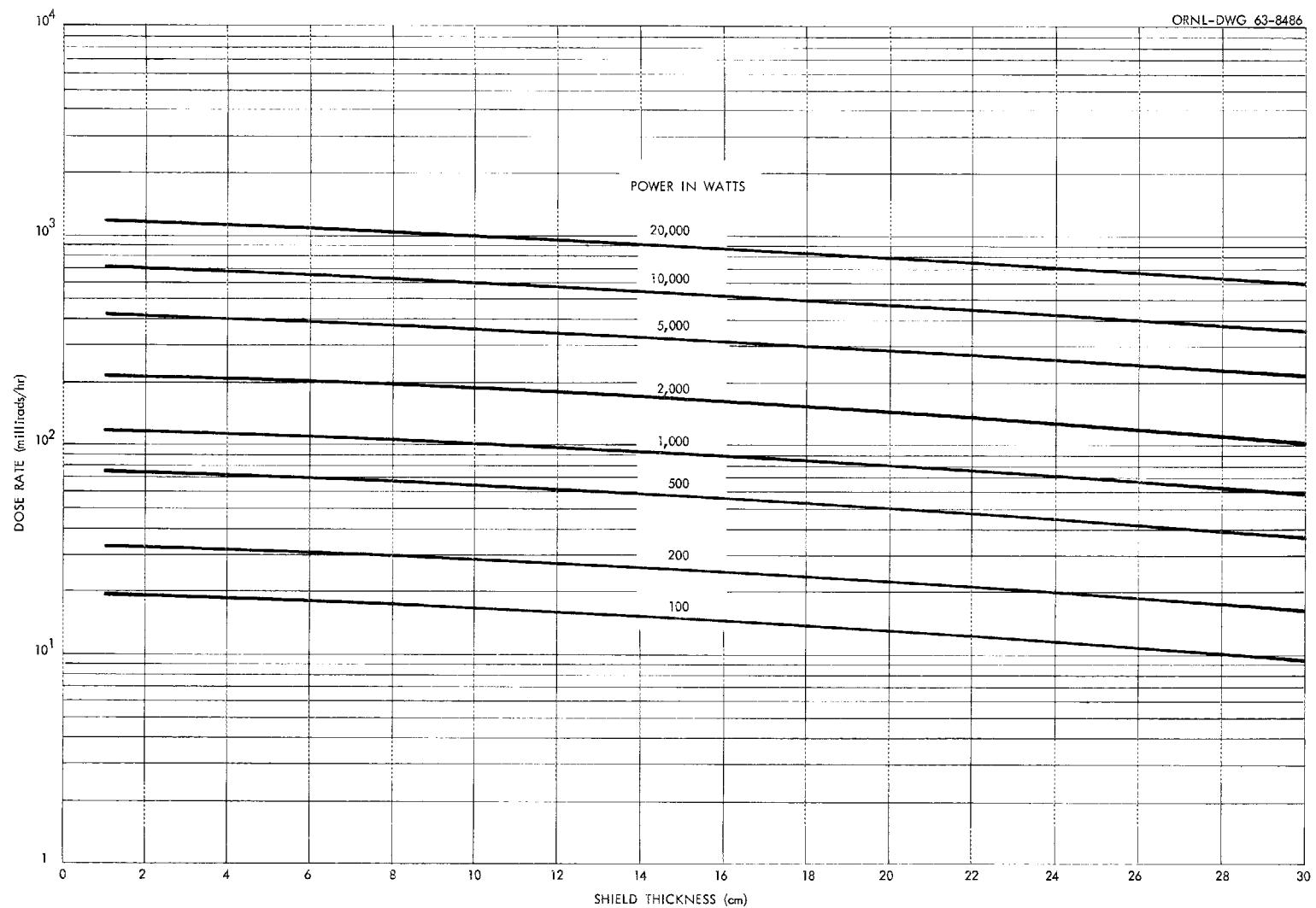


Fig. 2. Gamma Dose Rates From Iron-Shielded Isotopic Power Sources of Curium-244. Center of source to dose point separation distance = 100 cm.

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Fig. 3. Gamma Dose Rates From Water-Shielded Isotopic Power Sources of Curium-244. Center of source to dose point separation distance = 100 cm.

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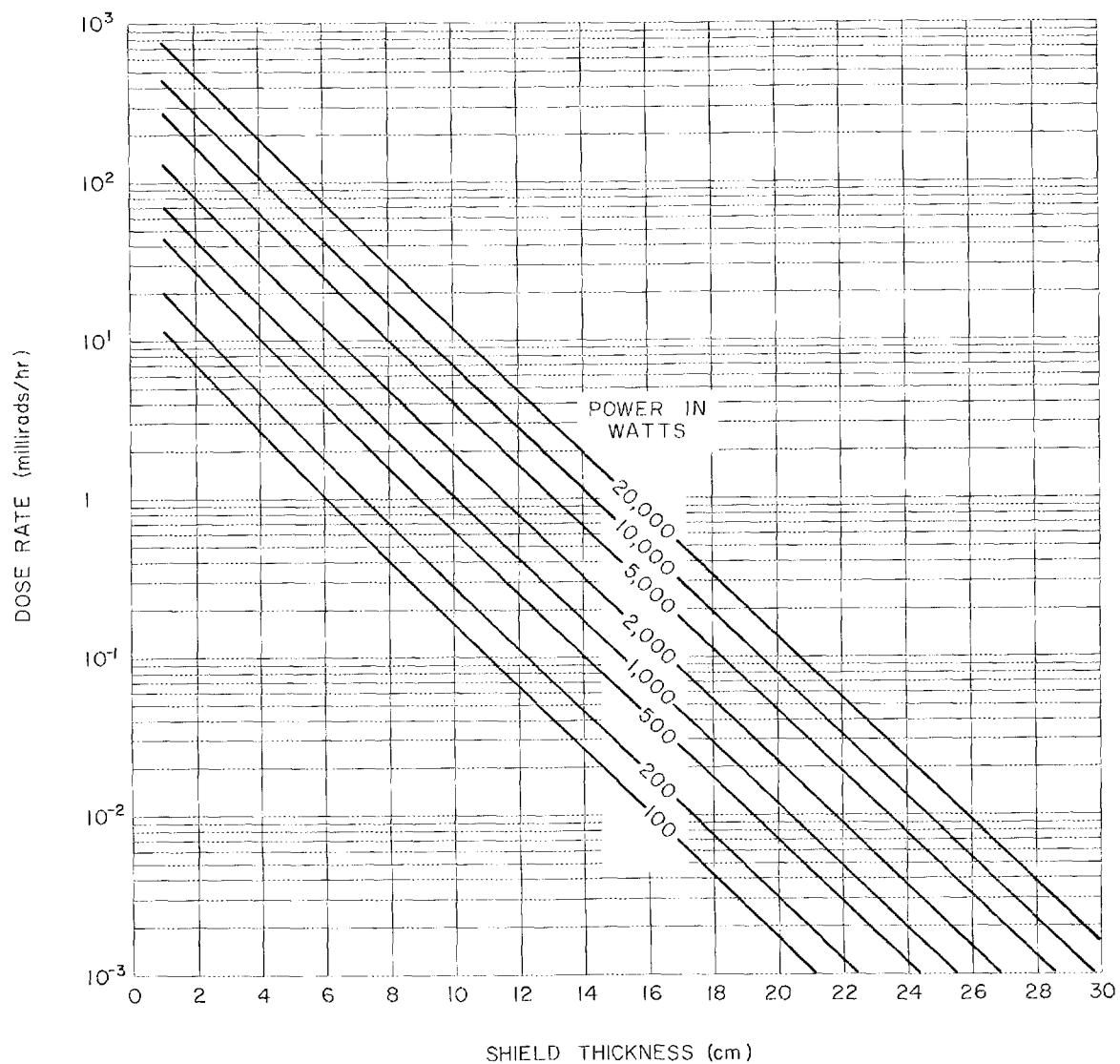


Fig. 4. Gamma Dose Rates From Lead-Shielded Isotopic Power Source of Curium-244. Center of source to dose point separation distance = 100 cm.

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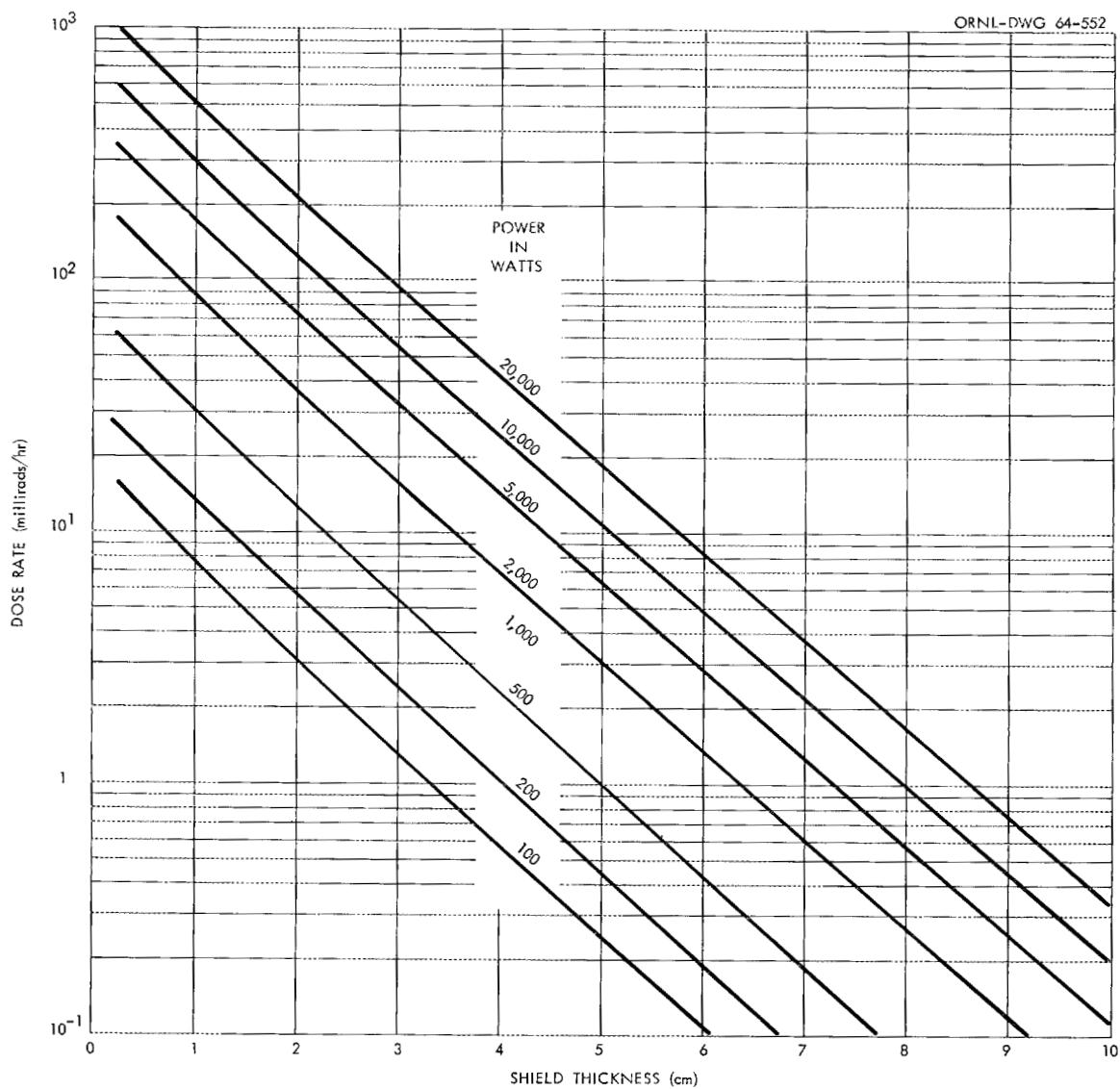


Fig. 5. Gamma Dose Rates From Uranium-Shielded Isotopic Power Sources of Curium-244. Center of source to dose point separation distance = 100 cm.

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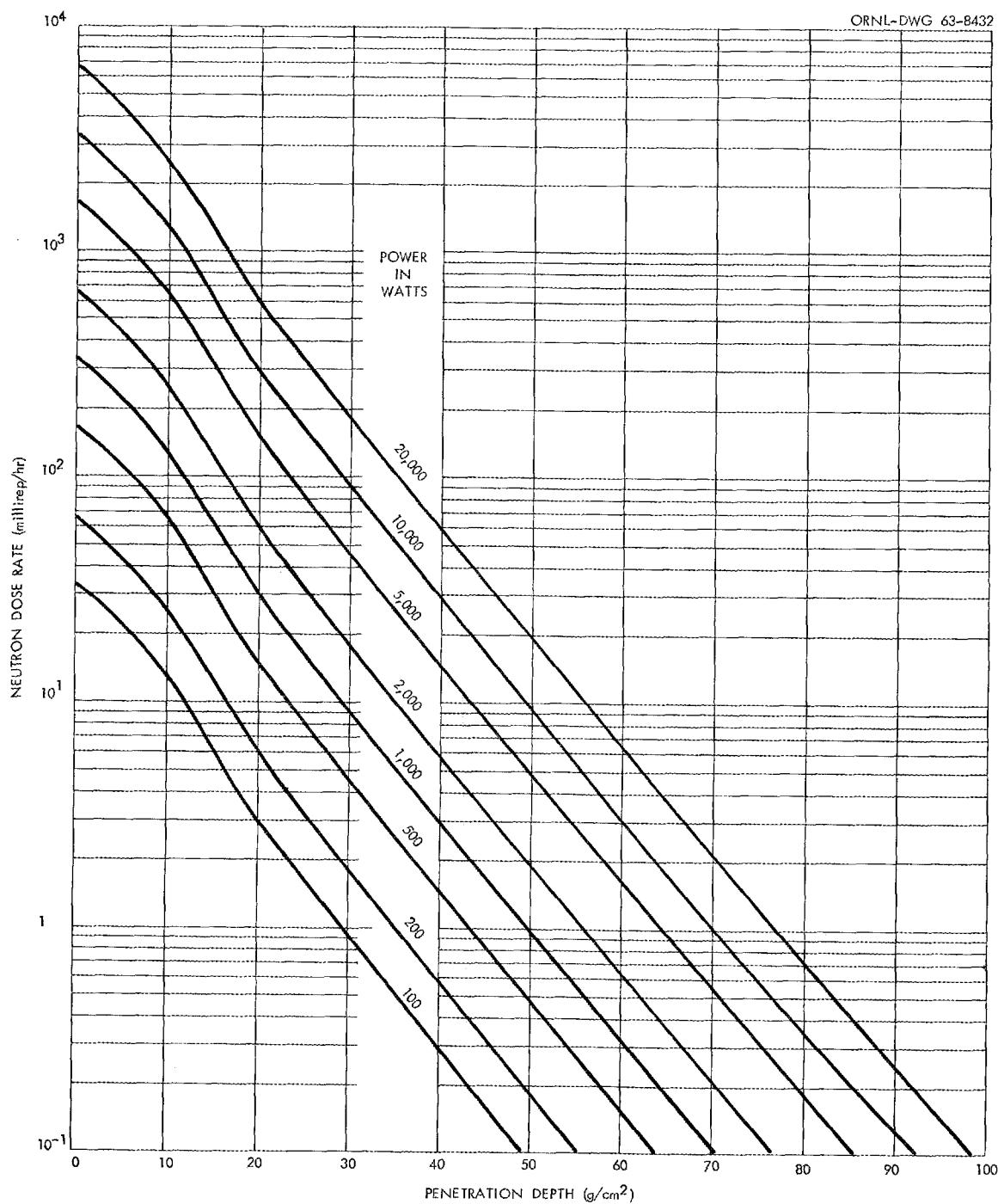


Fig. 6. Neutron Dose Rates From Water-Shielded Isotopic Power Sources of Curium-244 as a Function of Penetration Depth of Shielding Material. Center of source to dose point separation distance = 100 cm.

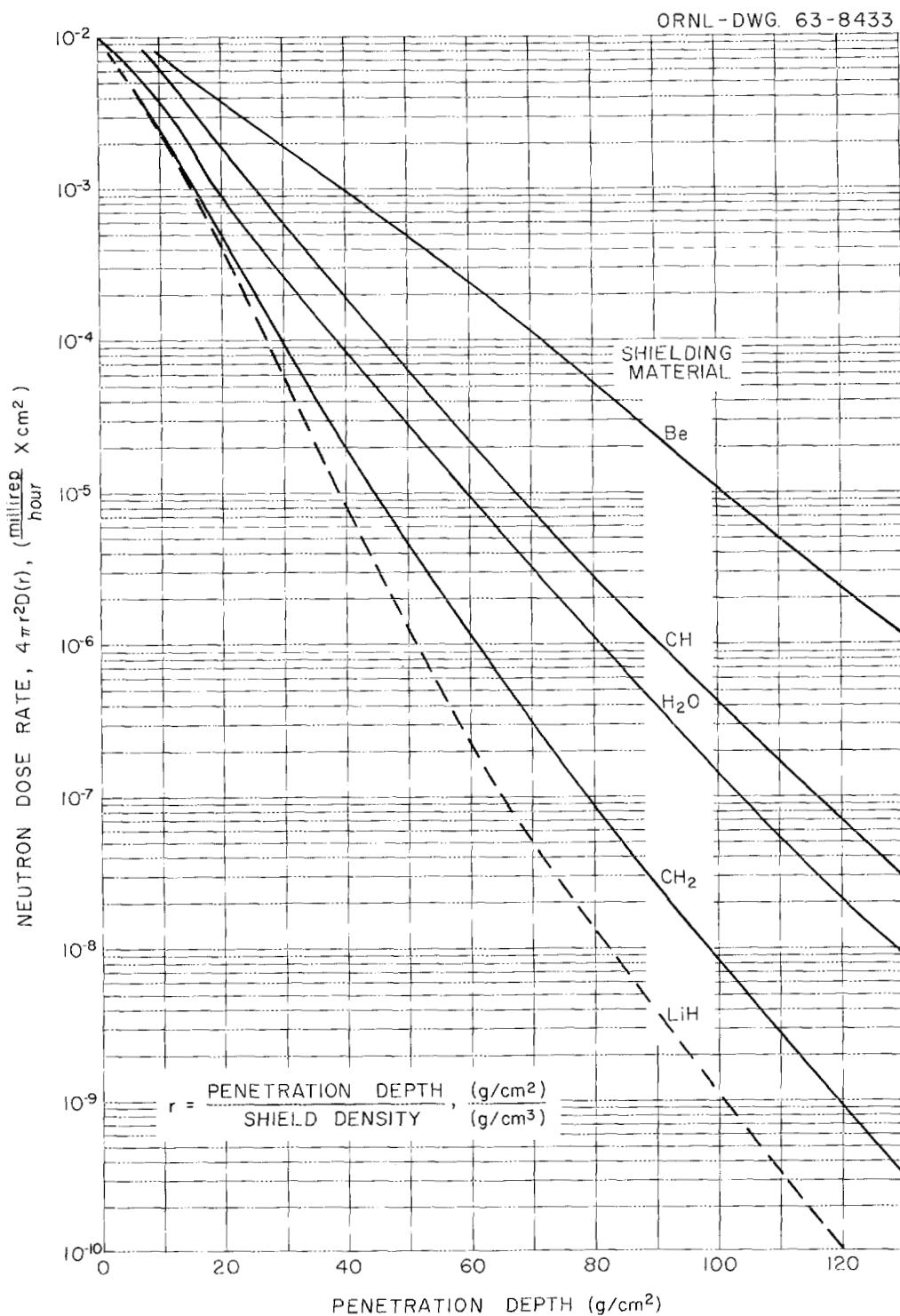


Fig. 7. Fast Neutron Dose Rate (Multiplied by  $4\pi r^2$ ) in Various Materials as a Function of Penetration Depth From a Unit Point Isotropic Fission Source.

REFERENCE COLUMNB. CURIUM SESQUIOXIDE ( $\text{Cm}_2\text{O}_3$ )1. Composition

## a. Radionuclidic abundance

See Section I.A.1.

## b. Radiochemical purity

Section I.A.1.

## c. Phase composition of various curium oxides                    25, 26, 27

$\text{CmO}_2$ .00	$\text{CmO}_1$ .77	$\text{CmO}_1$ .68
$\text{CmO}_1$ .91	$\text{CmO}_1$ .72	$\text{CmO}_1$ .50
$\text{CmO}_1$ .85		

2. Specific Powera. 2.53 watts/g of pure  $\text{Cm}_2\text{O}_3$  (91.0%  $^{244}\text{Cm}$  metal)  
2.42 watts/g of  $\text{Cm}_2\text{O}_3$  (86.9% Cm metal)

It is assumed that there are 81 curies/g  
of  $^{244}\text{Cm}$  metal and 34.3 watts/kilocurie of  
 $^{244}\text{Cm}$ .

b. 73.7 curies of  $^{244}\text{Cm}$  per gram of pure  $\text{Cm}_2\text{O}_3$                     2, 3, 4  
(91.0%  $^{244}\text{Cm}$  metal)  
70.5 curies of  $^{244}\text{Cm}$  per gram of  $\text{Cm}_2\text{O}_3$   
(86.9% Cm metal)3. Radiation

The radiation is given under Section I.A.3.

4. Critical Mass

See Section I.A.4.

5. Compatibility With Materials of Containment

A molybdenum alloy containing 0.5% titanium and 0.1% zirconium (TZM) was contacted with an oxide mixture containing 29 wt %  $^{244}\text{Cm}_2\text{O}_3$ , 57 wt %  $^{241}\text{AmO}_2$ , and 14 wt %  $^{239}\text{PuO}_2$ . Static capsule tests at 1100°C for periods of 250 and 1000 hr and at 2000°C for 25 hr showed no reaction with molybdenum, even though the oxide fuel was molten at 2000°C.

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<u>System</u>	<u>Temp, °C</u>	<u>Time, hr</u>	<u>Atm</u>	<u>Extent of reaction</u>	<u>REFERENCE COLUMN</u>
Cm <sub>2</sub> O <sub>3</sub> powder in W crucible	1800	8	Vacuum	None detected visually	27
Cm <sub>2</sub> O <sub>3</sub> powder on W filament	2150 (melted)	1	4% H <sub>2</sub> - 96% He	No reaction, wetting, or penetration detected by metallography or by fission fragment autoradiography	
Cm <sub>2</sub> O <sub>3</sub> powder on Ir filament	2150 (melted)	1	Helium	Curium penetration and surface reaction	
Cm <sub>2</sub> O <sub>3</sub> powder on Pt-50% Rh filament	1700	10	O <sub>2</sub>	No curium penetration, but possible surface reaction	

## 6. Thermophysical Properties

### a. Density

11.67 ± 0.03 g/cm <sup>3</sup> - monoclinic	29
11.94 ± 0.07 g/cm <sup>3</sup> - hexagonal	25

### b. Coefficient of thermal expansion

<u>°C<sup>-1</sup></u>	<u>Temperature, °C</u>	
8.90 x 10 <sup>-6</sup>	300	30 (Nd <sub>2</sub> O <sub>3</sub> )
10.60 x 10 <sup>-6</sup>	500	
11.35 x 10 <sup>-6</sup>	800	
11.41 x 10 <sup>-6</sup>	1050	

### c. Specific heat and enthalpy

(1) Specific heat in cal g <sup>-1</sup> °C <sup>-1</sup>		
3.7 x 10 <sup>-2</sup> + 2.91 x 10 <sup>-5</sup> T (°K)		31 (Am <sub>2</sub> O <sub>3</sub> )

### (2) Enthalpy in calories

### d. Temperatures of phase transformations

(1) Melting point - 1950°C	32
- 2150°C	27
(2) Boiling point - 3130°C	31 (Am <sub>2</sub> O <sub>3</sub> )
(3) Cm <sub>2</sub> O <sub>3</sub> (monoclinic) to Cm <sub>2</sub> O <sub>3</sub> (orthorhombic) - 1900°C	27

REFERENCE COLUMN

(4) Decomposition temperatures to lower oxides at oxygen pressures as cited:

27

Oxide	Temperature, °C		
	P O <sub>2</sub> = 10 <sup>-5</sup>	3 x 10 <sup>-3</sup>	1 atm
CmO <sub>2.00</sub>	360	391	440
CmO <sub>1.91</sub>	Nonexistent	Nonexistent	520
CmO <sub>1.85</sub>	520	625	>700
CmO <sub>1.77</sub>	725	870	--
CmO <sub>1.73</sub>	870	1065	--
CmO <sub>1.68</sub>	1070	>1120	--
CmO <sub>1.50</sub>	--	--	--

e. Latent heats of phase transformations

ΔH fusion 17 kcal/mole 31 (Am<sub>2</sub>O<sub>3</sub>)

ΔH vaporization 85 kcal/mole 31 (Am<sub>2</sub>O<sub>3</sub>)

f. Vapor pressure

Vaporization rate of Cm<sub>2</sub>O<sub>3</sub> is as follows:

27

Temperature, °C	Rate, g cm <sup>-2</sup> sec <sup>-1</sup>
1914	4.0 x 10 <sup>-6</sup>
1929	9.0 x 10 <sup>-6</sup>
1958	15.9 x 10 <sup>-6</sup>
1986	17.0 x 10 <sup>-6</sup>
2023	59.8 x 10 <sup>-6</sup>
2041	76.5 x 10 <sup>-6</sup>
2109	119 x 10 <sup>-6</sup>
2122	221 x 10 <sup>-6</sup>

g. Thermal conductivity

cal cm <sup>-1</sup> sec <sup>-1</sup> °C <sup>-1</sup>	Temperature, °C
0.0245	100
0.0204	200
0.0143	400
0.0104	600
0.0081	800
0.0073	1000
0.0060	1200
0.0059	1400

REFERENCE COLUMN

## h. Thermal diffusivity

<u>cm<sup>2</sup>/sec</u>	<u>Temperature, °C</u>
0.0478	100
0.0111	800
0.00645	1400

Calculated by dividing the product of the specific heat and room temperature density into the thermal conductivity.

## i. Viscosity

## j. Surface tension

## k. Total hemispherical emittance

## l. Spectral emissivity

0.20 to 0.57	19 (ThO <sub>2</sub> )
--------------	------------------------

The precise value is a function of the roughness of the material surface, the presence of impurities, and the effects of radiation.

## m. Crystallography

29

Cm<sub>2</sub>O<sub>3</sub>: Monoclinic, beta-type rare-earth oxide

a = 14.28  
 b = 3.65  
 c = 8.92  
 β = 100°24'

Space group

C<sub>2</sub><sup>3</sup>h

Six units per cell

Cm<sub>2</sub>O<sub>3</sub>: Orthorhombic

a = 7.993  
 b = 6.188  
 c = 3.368

## n. Solubilities

Insoluble in water

20

## o. Diffusion rates

REFERENCE COLUMN7. Mechanical Properties

a. Hardness

b. Crush strength

1900 kg/cm<sup>2</sup>34 (CeO<sub>2</sub>)8. Chemical Properties

a. Heat and free energy of formation, entropy

(1) Heat of formation

 $\Delta H_f^\circ = -440$  kcal/mole

31

(estimated from Am<sub>2</sub>O<sub>3</sub> and Pu<sub>2</sub>O<sub>3</sub>)

(2) Free energy of formation

 $\Delta F_f^\circ = -420$  kcal/mole

31

(estimated from Am<sub>2</sub>O<sub>3</sub> and Pu<sub>2</sub>O<sub>3</sub>)

(3) Entropy (estimated)

35

Cm<sub>2</sub>O<sub>3</sub>: S<sub>298</sub><sup>o</sup> = 38.4 euCmO<sub>2</sub>: S<sub>298</sub><sup>o</sup> = 20.9 eu

b. Chemical reactions and reaction rates

(oxygen, nitrogen, water, steam, hydrogen liquid metals, other)

(1) Oxygen at room temperature - slow

20

(2) Oxygen at elevated temperature - fast

(3) Nitrogen - no reaction

(4) Water - possible hydration reaction

(5) Inorganic acids - soluble in acids

9. Biological TolerancesMaximum permissible body burdens and maximum permissible concentrations of <sup>244</sup>Cm in air and in water are given under Section I.A.9.

24

10. Shielding Data

The dose rates are given under Section I.A.10.

REFERENCE COLUMNC. CURIUM OXYSULFIDE ( $\text{Cm}_2\text{O}_2\text{S}$ )1. Composition

- a. Radionuclidic abundance

See Section I.A.1.

- b. Radiochemical purity

See Section I.A.1.

2. Specific Power

- a. 2.46 watts/g of pure  $\text{Cm}_2\text{O}_2\text{S}$  (88.4%  $^{244}\text{Cm}$  metal)  
2.35 watts/g of  $\text{Cm}_2\text{O}_2\text{S}$  (84.4%  $^{244}\text{Cm}$  metal)

It is assumed that there are 81 curies/g of  $^{244}\text{Cm}$  and 34.3 watts/kilocurie of  $^{244}\text{Cm}$ .

- b. 71.6 curies of  $^{244}\text{Cm}$  per gram of pure  $\text{Cm}_2\text{O}_2\text{S}$   
(88.4%  $^{244}\text{Cm}$  metal)  
68.4 curies of  $^{244}\text{Cm}$  per gram of  $\text{Cm}_2\text{O}_2\text{S}$   
(84.4%  $^{244}\text{Cm}$  metal)

2, 3, 4

3. Radiation

The radiation is given under Section I.A.3.

4. Critical Mass

See Section I.A.4.

5. Compatibility With Materials of Containment6. Thermophysical Properties

- a. Density

9.95 g/cm<sup>3</sup>

36 ( $\text{Pu}_2\text{O}_2\text{S}$ )

- b. Coefficient of thermal expansion

$^{\circ}\text{C}^{-1}$	<u>Temperature, <math>^{\circ}\text{C}</math></u>	
$8.90 \times 10^{-6}$	300	30 ( $\text{Nd}_2\text{O}_3$ )
$10.60 \times 10^{-6}$	500	
$11.35 \times 10^{-6}$	800	
$11.41 \times 10^{-6}$	1050	

REFERENCE COLUMN

- c. Specific heat and enthalpy
  - (1) Specific heat in cal g<sup>-1</sup> °C<sup>-1</sup>  
 $3.62 \times 10^{-2} + 2.83 \times 10^{-5} T$  (°K) 31 (Am<sub>2</sub>O<sub>3</sub>)
  - (2) Enthalpy in calories
- d. Temperatures of phase transformations
  - (1) Melting point = 2000°C 37 (Ce<sub>2</sub>O<sub>2</sub>S)
  - (2) Boiling point = 3130°C 31 (Am<sub>2</sub>O<sub>3</sub>)
- e. Latent heats of phase transformations
  - ΔH fusion 17 kcal/mole 31 (Am<sub>2</sub>O<sub>3</sub>)
  - ΔH vaporization 85 kcal/mole 31 (Am<sub>2</sub>O<sub>3</sub>)
- f. Vapor pressure
- g. Thermal conductivity
 

<u>cal cm<sup>-1</sup> sec<sup>-1</sup> °C<sup>-1</sup></u>	<u>Temperature, °C</u>	
0.0245	100	33 (ThO <sub>2</sub> )
0.0081	800	
0.0059	1400	
- h. Thermal diffusivity
 

<u>cm<sup>2</sup>/sec</u>	<u>Temperature, °C</u>
0.0528	100
0.0116	800
0.00708	1400

Calculated by dividing the product of the specific heat and room temperature density into the thermal conductivity.
- i. Viscosity
- j. Surface tension
- k. Total hemispherical emittance
- l. Spectral emissivity
 

0.20 to 0.57	19 (ThO <sub>2</sub> )
--------------	------------------------

The emissivity value depends on the roughness of the material surface, radiation effects, and the presence of impurities.

	<u>REFERENCE COLUMN</u>
m. Crystallography	
hexagonal	36 ( $\text{Pu}_2\text{O}_2\text{S}$ )
$a = 4.008 \text{ \AA}$	
$c = 6.769 \text{ \AA}$	
The cell constants should be slightly smaller for $\text{Cm}_2\text{O}_2\text{S}$ due to the actinide contraction.	
n. Solubilities	
(1) Soluble in strong acids ( $\text{Ce}_2\text{O}_2\text{S}$ )	38
(2) Insoluble in acetic acid ( $\text{Ce}_2\text{O}_2\text{S}$ )	38
o. Diffusion rates	
7. <u>Mechanical Properties</u>	
a. Hardness	
b. Crush strength	
8. <u>Chemical Properties</u>	
a. Heat and free energy of formation, entropy	
(1) Heat of formation	
$\Delta H^\circ_f = -430 \text{ kcal/mole}$	37
(approximated by $\text{Ce}_2\text{O}_2\text{S}$ )	
(2) Free energy of formation	
$\Delta F^\circ_f = -414 \text{ kcal/mole}$	
(calculated by $\Delta F^\circ_f = \Delta H^\circ_f - T\Delta S^\circ_f$ )	
(3) Entropy	
$S_{298}^\circ = 34.3 \text{ eu}$	39
(calculated by W. Latimer's method)	
b. Chemical reactions and reaction rates	38
(oxygen, nitrogen, water, steam, hydrogen, liquid metals, other)	
(1) Air at room temperature - slow	
(2) Air at elevated temperature - fast	
(3) Water at room temperature - no reaction	
(4) Inorganic acids at room temperature - reacts	

REFERENCE COLUMN9. Biological Tolerances

Maximum permissible body burdens and maximum permissible concentrations of  $^{244}\text{Cm}$  in air and in water are given under the  $^{244}\text{Cm}$  Metal Source Form, Section I.A.9.

 $^{24}$ 10. Shielding Data

The dose rates are given under the  $^{244}\text{Cm}$  Metal Source Form, Section I.A.10.

D. CURIUM FLUORIDE ( $\text{CmF}_3$ )REFERENCE COLUMN1. Composition

- a. Radionuclidic abundance

See Section I.A.1.

- b. Radiochemical purity

See Section I.A.1.

2. Specific Power

- a. 2.25 watts/g of pure  $\text{CmF}_3$  (81.1%  $^{244}\text{Cm}$  metal)  
 2.15 watts/g of  $\text{CmF}_3$  (77.5%  $^{244}\text{Cm}$  metal)

It is assumed that there are 81 curies/g of  $^{244}\text{Cm}$  and 34.3 watts/kilocurie of  $^{244}\text{Cm}$ .

- b. 65.7 curies of  $^{244}\text{Cm}$  per gram of pure  $\text{CmF}_3$   
 (81.1%  $^{244}\text{Cm}$  metal)  
 62.7 curies of  $^{244}\text{Cm}$  per gram of  $\text{CmF}_3$   
 (77.5%  $^{244}\text{Cm}$  metal)

2, 3, 4

3. Radiation

The radiation is given under Section I.A.3.

4. Critical Mass

See Section I.A.4.

5. Compatibility With Materials of Containment6. Thermophysical Properties

- a. Density

9.80 g/cm<sup>3</sup>

40

- b. Coefficient of thermal expansion

$$a = 19.74 \times 10^{-6} + 2.62 \times 10^{-3} t + 0.15 \times 10^{-10} t^2$$

41 ( $\text{BaF}_2$ )

(t is in °C with a temperature range of 26-296°C)

- c. Specific heat and enthalpy

(1) Specific heat in cal g<sup>-1</sup> °C<sup>-1</sup>

$$7.21 \times 10^{-2} + 2.06 \times 10^{-5} T (\text{°K})$$

31 ( $\text{AmF}_3$ )

REFERENCE COLUMN

## (2) Enthalpy in calories

$$H_f - H_{298} = 21 T + 3.5 \times 10^{-3} T^2$$

(estimated from other actinide data)

31

## d. Temperatures of phase transformations

(1) Melting point - 1406°C

42

(2) Boiling point - 2330°C

12

This value is the average of the boiling points of  $\text{LaF}_3$ ,  $\text{CeF}_3$ , and  $\text{PrF}_3$ .

## e. Latent heats of phase transformations

 $\Delta H$  fusion 9 kcal/mole31 ( $\text{CeF}_3$ ) $\Delta H$  vaporization 62 kcal/mole31 ( $\text{CeF}_3$ )

## f. Vapor pressure

<u>Vapor pressure, torr</u>	<u>Temperature, °C</u>	
$5.07 \times 10^{-7}$	853	
$7.18 \times 10^{-6}$	943	
$1.486 \times 10^{-4}$	1033	
$1.725 \times 10^{-3}$	1141	
$5.820 \times 10^{-3}$	1196	

Vapor pressures are for  $\text{AmF}_3$ .

## g. Thermal conductivity

<u>cal cm<sup>-1</sup> sec<sup>-1</sup> °C<sup>-1</sup></u>	<u>Temperature, °C</u>	
0.0296	0	
0.0251	100	

44 ( $\text{BaF}_2$ )

## h. Thermal diffusivity

<u>cm<sup>2</sup>/sec</u>	<u>Temperature, °C</u>	
0.0399	0	
0.0321	100	

Calculated by dividing the product of the specific heat and the room temperature density into the thermal conductivity.

## i. Viscosity

## j. Surface tension

REFERENCE COLUMN

k. Total hemispherical emittance

A value of 0.9 can be assumed.

l. Spectral emissivity

m. Crystallography

hexagonal, LaF<sub>3</sub>-type, space group P6<sub>3</sub>/mmc

45

a = 4.041 ± 0.001 Å      c = 7.179 ± 0.002 Å

n. Solubilities

o. Diffusion rates

7. Mechanical Properties

a. Hardness

b. Crush strength

8. Chemical Properties

a. Heat and free energy of formation, entropy

(1) Heat of formation

$$\Delta H^\circ_f = -395 \text{ kcal/mole}$$

31

(estimated from other actinide data)

(2) Free energy of formation

$$\Delta F^\circ_f = -375 \text{ kcal/mole}$$

31

(estimated from other actinide data)

(3) Entropy

$$S_{298}^\circ = 29 \text{ eu}$$

31

(estimated from other actinide data)

b. Chemical reactions and reaction rates

(oxygen, nitrogen, water, steam, hydrogen, liquid metals, other)

(1) Air at room temperature - no reaction

(2) Air at elevated temperature - forms oxyfluoride 20

(3) Nitrogen - no reaction

(4) Water - insoluble

(5) Inorganic acids - insoluble in weak inorganic acid

REFERENCE COLUMN9. Biological Tolerances

Maximum permissible body burdens and maximum permissible concentrations of  $^{244}\text{Cm}$  in air and in water are given under Section I.A.9.

24

10. Shielding Data

The dose rates are given under Section I.A.10.

## II. CURIUM-242

REFERENCE COLUMN

A. CURIUM-242 OXIDE CERMET                    HALF-LIFE: 163 d            1, 2, 5, 7

1. Composition

## a. Radionuclidic abundance

The composition of the product will depend on the irradiation history of the  $^{241}\text{Am}$  target as well as the cooling time after removal from the pile. The product is expected to be at least 40%  $^{242}\text{Cm}$ . If it is not this high, an Am-Cm separation is used to lower the americium content of the product.

The analysis for a typical batch of  $^{241}\text{Am}$  with a total integrated neutron dose of  $1.3 \times 10^{21}$  and with a 90-day cooling and processing period (with all the plutonium removed) is as follows:

46

<u>Isotope</u>	<u>% Abundance</u>
$^{241}\text{Am}$	47.5
$^{242}\text{Am}$	1.6
$^{243}\text{Am}$	7.7
$^{242}\text{Cm}$	41.9
$^{243}\text{Cm}$	0.5
$^{244}\text{Cm}$	0.8

The decay of  $^{242}\text{Cm}$  to  $^{238}\text{Pu}$  is illustrated in the following table. A 10-g product with 40%  $^{242}\text{Cm}$  and 60% other actinides is assumed. The decay is shown for 163 days.

<u>Time, days</u>	<u><math>^{242}\text{Cm}, \text{ g}</math></u>	<u><math>^{238}\text{Pu}, \text{ g}</math></u>
0	4.00	0
16	3.73	0.27
32	3.48	0.52
65	3.03	0.97
81.5	2.83	1.17
98	2.46	1.54
163	2.00	2.00

The oxide mixture will be  $\text{AmO}_2$  and  $\text{Cm}_2\text{O}_3$ . This will be suspended in a neutral matrix material to give the prescribed power density:

30 vol % oxide mixture  
70 vol % matrix material

REFERENCE COLUMN

## b. Radiochemical purity

The only important heat contributor to the  $^{242}\text{Cm}$ -source material is  $^{242}\text{Cm}$ . The following table shows the contribution of each isotope to 10 g of the oxide mixture.

46

Heat Contribution of Each Isotope of the  $^{242}\text{Cm}$  Product

Nuclide	Half-life	Specific activity, w/g	% of nuclide	Heat contribution watts	Heat contribution %
$^{241}\text{Am}$	458 y	0.106	47.5	0.50	0.1
$^{242}\text{Am}$	152 y	0.034	1.6	0.05	0.01
$^{243}\text{Am}$	7650 y	0.006	7.7	0.005	0.001
$^{242}\text{Cm}$	163 d	120.0	41.9	502.8	99.8
$^{243}\text{Cm}$	32 y	1.44	0.5	0.07	0.015
$^{244}\text{Cm}$	18.1 y	2.78	0.8	0.22	0.05
$^{238}\text{Pu}$	89 y	0.55			

The  $^{242}\text{Cm}$  product has contained up to 30 curies of  $^{144}\text{Ce}$  per 8.33 g of  $^{242}\text{Cm}$ . Trace amounts of  $^{103}\text{Ru}$ - $^{106}\text{Ru}$  and  $^{95}\text{Zr}$ - $^{95}\text{Nb}$  have been found in the feed but do not contribute materially to the power or radiation of the source.

The above contaminations can be reduced to much lower levels by additional processing.

2. Specific Powera. 42.8 watts/g of  $\text{AmO}_2\text{-Cm}_2\text{O}_3$  (35.7%  $^{242}\text{Cm}$  metal)

It is assumed that there are 3320 curies/g of  $^{242}\text{Cm}$  and 36.1 watts/kilocurie of  $^{242}\text{Cm}$ .

6

b. 1186 curies of  $^{242}\text{Cm}$  per gram of  $\text{AmO}_2\text{-Cm}_2\text{O}_3$  (35.7%  $^{242}\text{Cm}$  metal)

5

3. Radiation

## a. Alpha particles

5

Nuclide	Max E, Mev	Avg E, Mev	Abundance, %	w/kilocurie	Particles $\text{w}^{-1} \text{ sec}^{-1}$
$^{242}\text{Cm}$	6.11	6.11	73.7	36.10	$0.755 \times 10^{12}$
	6.066	6.066	26.3	—	$0.270 \times 10^{12}$
Total power				36.10	

REFERENCE COLUMN

The amount of helium produced by alpha decay of  $^{242}\text{Cm}$  as a function of time is given in the following table.

Volume of Helium as a Function of Decay Time

$\text{cm}^3$ of He per g of $^{242}\text{Cm}$ (standard conditions)	Time Days	Time Half-lives
11.9	32.6	0.2
22.4	65.2	0.4
31.5	97.8	0.6
39.4	130.4	0.8
46.3	163	1.0
59.8	244	1.5
69.4	326	2.0
80.9	489	3.0
86.7	652	4.0
89.6	815	5.0
92.4	1630	10.0

b. Beta particles - none

c. Gamma

In addition to the gammas from the alpha decay, there are the prompt and fission-product gammas from the spontaneous fission of  $^{242}\text{Cm}$  ( $T_{1/2} = 7.2 \times 10^6$  y). The gamma-emission rates are given in the following table.

5

Gamma-emission rate,* photons sec <sup>-1</sup> g <sup>-1</sup>	Photon energy, Mev
<u><math>^{242}\text{Cm}</math> gammas</u>	
$0.27 \times 10^{14}$	0.044
$1.42 \times 10^{10}$	0.10
$2.83 \times 10^9$	0.158
<u>Prompt gammas</u>	
$2.44 \times 10^7$	1.0
$6.09 \times 10^6$	1.5
$6.45 \times 10^6$	2.3
$1.15 \times 10^6$	3.0
$1.52 \times 10^6$	5.0

REFERENCE COLUMN

Gamma-emission rate,* photons sec <sup>-1</sup> g <sup>-1</sup>	Photon energy, Mev
<u>Fission-product gammas</u>	
2.16 x 10 <sup>7</sup>	0.63
7.99 x 10 <sup>6</sup>	1.1
9.36 x 10 <sup>6</sup>	1.55
1.80 x 10 <sup>6</sup>	2.38
2.66 x 10 <sup>6</sup>	2.75

\*120-watt source.

d. Bremsstrahlung - none

e. Neutrons

2.30 x 10<sup>7</sup> neutrons sec<sup>-1</sup> g<sup>-1</sup> of <sup>242</sup>Cm from spontaneous fission (120-watt source) 5

2.0 x 10<sup>7</sup> neutrons sec<sup>-1</sup> g<sup>-1</sup> of <sup>242</sup>Cm from ( $\alpha$ ,n) reaction on oxygen in Cm<sub>2</sub>O<sub>3</sub> (120-watt source)

The energy distribution of spontaneous fission neutrons from <sup>242</sup>Cm is given in the following table. 3

#### Spontaneous Fission Neutrons From <sup>242</sup>Cm

Energy, Mev	Abundance,* neutrons sec <sup>-1</sup> g <sup>-1</sup> of <sup>242</sup> Cm
0.3-0.4	7.7 x 10 <sup>5</sup>
0.4-0.6	1.6 x 10 <sup>6</sup>
0.6-0.8	1.6 x 10 <sup>6</sup>
0.8-1.0	1.4 x 10 <sup>6</sup>
1.0-1.2	1.4 x 10 <sup>6</sup>
1.2-1.4	1.4 x 10 <sup>6</sup>
1.4-1.6	1.2 x 10 <sup>6</sup>
1.6-1.8	1.1 x 10 <sup>6</sup>
1.8-2.0	1.0 x 10 <sup>6</sup>
2.0-2.2	9.1 x 10 <sup>5</sup>
2.2-2.4	8.4 x 10 <sup>5</sup>
2.4-2.6	8.0 x 10 <sup>5</sup>
2.6-2.8	6.5 x 10 <sup>5</sup>
2.8-3.0	5.5 x 10 <sup>5</sup>
3.0-3.2	5.0 x 10 <sup>5</sup>
3.2-3.4	5.0 x 10 <sup>5</sup>
3.4-3.6	4.7 x 10 <sup>5</sup>
3.6-3.8	3.7 x 10 <sup>5</sup>
3.8-4.0	4.1 x 10 <sup>5</sup>

REFERENCE COLUMN

## Spontaneous (continued)

Energy, Mev	Abundance, neutrons sec <sup>-1</sup> g <sup>-1</sup> of <sup>242</sup> Cm
4.0-4.4	5.2 x 10 <sup>5</sup>
4.4-4.8	4.4 x 10 <sup>5</sup>
4.8-5.2	3.2 x 10 <sup>5</sup>
5.2-5.6	2.5 x 10 <sup>5</sup>
5.6-6.0	1.9 x 10 <sup>5</sup>
6.0-6.4	1.5 x 10 <sup>5</sup>
6.4-6.8	1.1 x 10 <sup>5</sup>
6.8-7.2	7.5 x 10 <sup>4</sup>
7.2-7.6	5.6 x 10 <sup>4</sup>
7.6-8.0	4.7 x 10 <sup>4</sup>
8.0-8.8	5.0 x 10 <sup>4</sup>
8.8-9.6	1.5 x 10 <sup>4</sup>
9.6-10.4	1.6 x 10 <sup>4</sup>
10.4-11.2	1.0 x 10 <sup>4</sup>
11.2-12.8	7.1 x 10 <sup>3</sup>

\* 120-watt source.

The energy distribution of neutrons occurring as a result of a collision of fast alpha particles from <sup>242</sup>Cm decay with oxygen atoms in Cm<sub>2</sub>O<sub>3</sub> is given in the following table.

3

Neutrons From ( $\alpha$ ,n) Reactions With Oxygen

Energy, Mev	Abundance, neutrons sec <sup>-1</sup> g <sup>-1</sup> of <sup>242</sup> Cm
0.2	5.0 x 10 <sup>3</sup>
0.4	1.0 x 10 <sup>4</sup>
0.6	2.0 x 10 <sup>4</sup>
0.8	2.5 x 10 <sup>4</sup>
1.0	7.6 x 10 <sup>4</sup>
1.2	1.5 x 10 <sup>5</sup>
1.4	2.8 x 10 <sup>5</sup>
1.6	4.5 x 10 <sup>5</sup>
1.8	7.6 x 10 <sup>5</sup>
2.0	1.0 x 10 <sup>6</sup>
2.2	1.3 x 10 <sup>6</sup>
2.4	1.7 x 10 <sup>6</sup>
2.6	2.0 x 10 <sup>6</sup>
2.8	2.1 x 10 <sup>6</sup>

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## Neutrons (continued)

Energy, Mev	Abundance,* neutrons sec <sup>-1</sup> g <sup>-1</sup> of <sup>242</sup> Cm
3.0	2.1 x 10 <sup>6</sup>
3.2	2.1 x 10 <sup>6</sup>
3.4	1.8 x 10 <sup>6</sup>
3.6	1.5 x 10 <sup>6</sup>
3.8	1.0 x 10 <sup>6</sup>
4.0	6.5 x 10 <sup>5</sup>
4.2	4.0 x 10 <sup>5</sup>
4.4	2.8 x 10 <sup>5</sup>
4.6	1.8 x 10 <sup>5</sup>
4.8	5.0 x 10 <sup>4</sup>

\*120-watt source.

4. Critical Mass5. Compatibility With Materials of Containment

Tests at 1100°C for 1000 hr and at 2000°C for 25 hr with an oxide mixture containing 29 wt %  $\text{Cm}_2\text{O}_3$ , 57 wt %  $\text{AmO}_2$ , and 14 wt %  $\text{PuO}_2$  showed that this oxide mixture was compatible with the alloy Mo-0.5% Ti-0.1% Zr (TZM). 28

With the use of iridium in a metal-metal oxide cermet, alloying of iridium with molybdenum was observed at 2000°C. Also the molten oxide mix appeared to react with iridium to form a lower melting alloy. At 1000°C the reaction between iridium and molybdenum was too slow to be observed, at least over a period of time of 1000 hr.

6. Thermophysical Properties

## a. Density

The density of oxide mixture is equal to 29  
11.67 g/cm<sup>3</sup>.

## b. Coefficient of thermal expansion

Linear coefficient of expansion, °C <sup>-1</sup>	Temperature, °C	30 ( $\text{Nd}_2\text{O}_3$ )
8.90 x 10 <sup>-6</sup>	300	
10.60 x 10 <sup>-6</sup>	500	
11.35 x 10 <sup>-6</sup>	800	
11.41 x 10 <sup>-6</sup>	1050	

The thermal coefficient of expansion of the cermet will depend markedly on the matrix material.

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- c. Specific heat and enthalpy
  - (1) Specific heat  
Values will depend on the matrix material.
  - (2) Enthalpy  
Values will depend on the matrix material.
- d. Temperatures of phase transformations
  - (1) Melting point - 2000-2200°C for  $\text{AmO}_2\text{-Cm}_2\text{O}_3$  mixture 32
  - (2) Boiling point - 3400°C for  $\text{AmO}_2\text{-Cm}_2\text{O}_3$  mixture 31 ( $\text{Am}_2\text{O}_3$ )
- e. Latent heats of phase transformations
  - $\Delta H$  fusion 17 kcal/mole 31 ( $\text{Am}_2\text{O}_3$ )
  - $\Delta H$  vaporization 85 kcal/mole 31 ( $\text{Am}_2\text{O}_3$ )
- f. Vapor pressure
  - % Will depend primarily on the matrix metal and on the temperature.
- g. Thermal conductivity 33 ( $\text{ThO}_2$ )
 

<u>cal cm<sup>-1</sup> sec<sup>-1</sup> °C<sup>-1</sup></u>	<u>Temperature, °C</u>
0.0245	100
0.0143	400
0.0081	800
0.0059	1400

With the selection of the proper matrix material for cermet, it should be possible to reach a  $0.06 \text{ cal cm}^{-1} \text{ sec}^{-1} \text{ °C}^{-1}$  thermal conductivity for the cermet.
- h. Thermal diffusivity  
Values will depend on the matrix material.
- i. Viscosity  
The viscosity will depend primarily on the properties of the matrix metal.
- j. Surface tension  
The surface tension will depend primarily on the properties of the matrix metal.

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- k. Total hemispherical emittance
- l. Spectral emissivity  
0.20-0.57 19 ( $\text{ThO}_2$ )  
The matrix material will have a pronounced effect on the emissivity.
- m. Crystallography 29  
 $\text{Cm}_2\text{O}_3$ : Monoclinic, beta-type rare-earth oxide  
 $a = 14.28$   
 $b = 3.65$   
 $c = 8.92$   
 $\beta = 100^\circ 24'$   
 Space group  
 $C_2^3 h$   
 Six units per cell  
 $\text{Cm}_2\text{O}_3$ : Orthorhombic  
 $a = 7.993$   
 $b = 6.188$   
 $c = 3.368$
- n. Solubilities  
Insoluble in water 20 ( $\text{Cm}_2\text{O}_3$ )
- o. Diffusion rates

7. Mechanical Properties

The mechanical properties of the metal-oxide mixture will depend strongly on the properties of the matrix metal.

- a. Hardness  
b. Crush strength

8. Chemical Properties

- a. Heat and free energy of formation, entropy  
The thermodynamic properties of a metal-oxide mixture will depend strongly on the metal matrix.  
 (1) Heat of formation  
 $\Delta H_f^\circ = -440 \text{ kcal/mole}$  31  
 (estimated from  $\text{Am}_2\text{O}_3$  and  $\text{Pu}_2\text{O}_3$ )

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(2) Free energy of formation	
$\Delta F^\circ_f = -420 \text{ kcal/mole}$	31
(estimated from $\text{Am}_2\text{O}_3$ and $\text{Pu}_2\text{O}_3$ )	
(3) Entropy (estimated)	35
$\text{Cm}_2\text{O}_3: S^\circ_{298} = 38.4 \text{ eu}$	
$\text{CmO}_2: S^\circ_{298} = 20.9 \text{ eu}$	
b. Chemical reactions and reaction rates (oxygen, nitrogen, water, steam, hydrogen liquid metals, other)	
These properties will depend on the matrix material.	

9. Biological Tolerances

The  $^{242}\text{Cm}$  tolerances taken from Ref 24 are given in 24  
the table on the following page.

10. Shielding Data

Gamma dose rates with water, iron, lead, and uranium  
shielding are given in Figs. 8-12 for  $^{242}\text{Cm}$  power 5  
sources of 100, 200, 500, 1000, 2000, 5000, 10,000,  
and 20,000 watts. Neutron dose rates with water  
shielding are given in Fig. 13. Neutron dose rates on  
shielding with Be, CH,  $\text{CH}_2$ , or LiH can be estimated by  
using Fig. 13 in conjunction with Fig. 14.

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Maximum Permissible Body Burdens and Maximum Permissible Concentrations  
for Radionuclides in Air and in Water for Occupational Exposure<sup>24</sup>

Radionuclide and type of decay	Organ of reference (critical organ underscored)	Max. permissible burden in total body, g( $\mu$ c)	Maximum permissible concentrations, $\mu$ c/cm <sup>3</sup>			
			For 40-hr week		For 168-hr week	
			Water	Air	Water	Air
(Sol)	<u>GI (LLI)*</u>		<u><math>7 \times 10^{-4}</math></u>	<u><math>2 \times 10^{-7}</math></u>	<u><math>2 \times 10^{-4}</math></u>	<u><math>5 \times 10^{-8}</math></u>
	Liver	0.05	$3 \times 10^{-3}$	<u><math>10^{-10}</math></u>	$9 \times 10^{-4}$	<u><math>4 \times 10^{-11}</math></u>
	Bone	0.09	$5 \times 10^{-3}$	$2 \times 10^{-10}$	$2 \times 10^{-3}$	$8 \times 10^{-11}$
	Kidney	0.2	$9 \times 10^{-3}$	$4 \times 10^{-10}$	$3 \times 10^{-3}$	$10^{-10}$
	Total Body	0.2	0.01	$6 \times 10^{-10}$	$5 \times 10^{-3}$	$2 \times 10^{-10}$
(Insol)	<u>Lung</u>			<u><math>2 \times 10^{-10}</math></u>		<u><math>6 \times 10^{-11}</math></u>
	<u>GI (LLI)*</u>		<u><math>7 \times 10^{-4}</math></u>	$10^{-7}$	<u><math>3 \times 10^{-4}</math></u>	$4 \times 10^{-8}$

\* The abbreviations GI and LLI refer to the gastrointestinal tract and lower large intestine, respectively.

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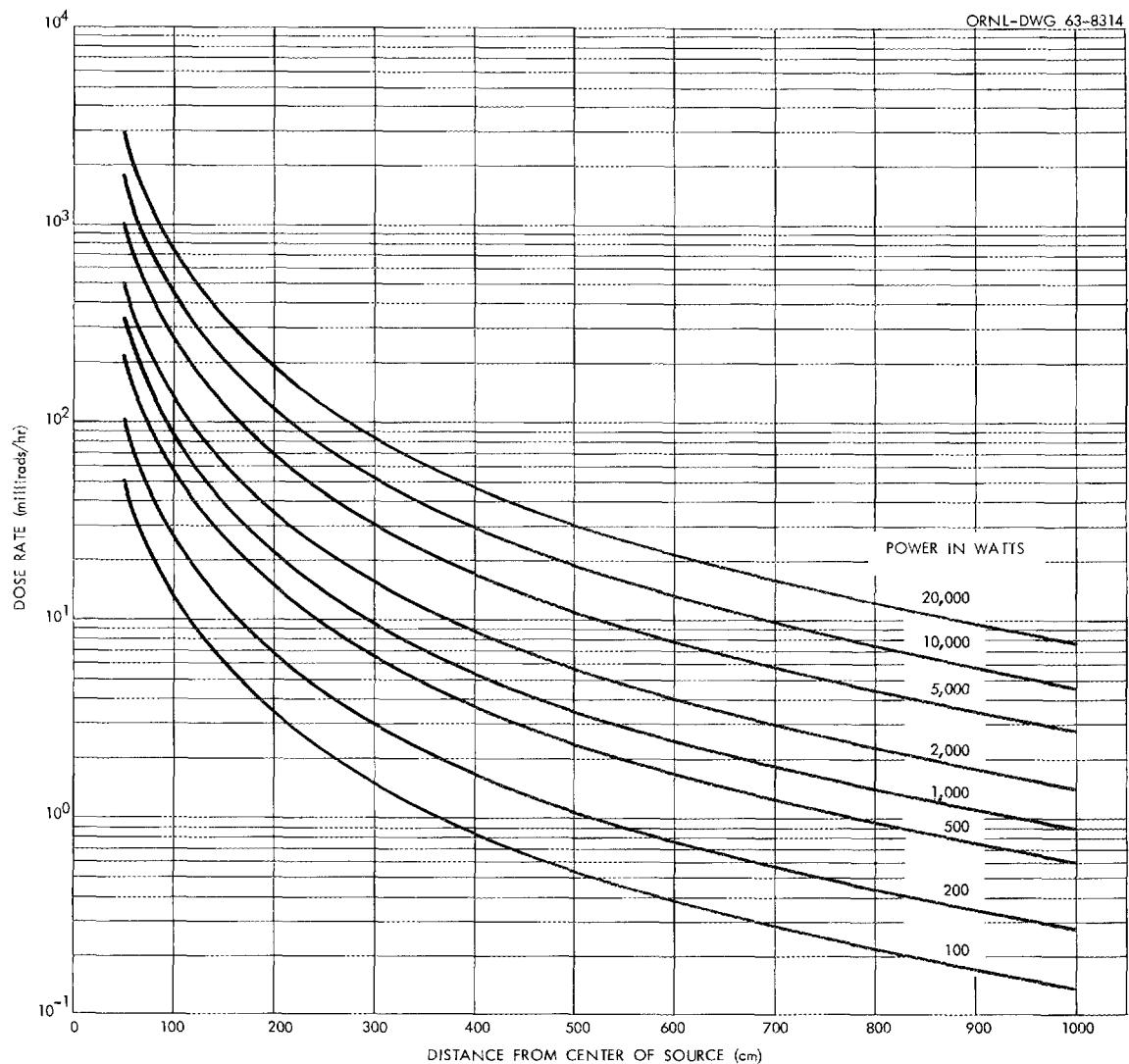


Fig. 8. Gamma Dose Rates From Unshielded Isotopic Power Sources of Curium-242 as a Function of Distance From Center of Source.

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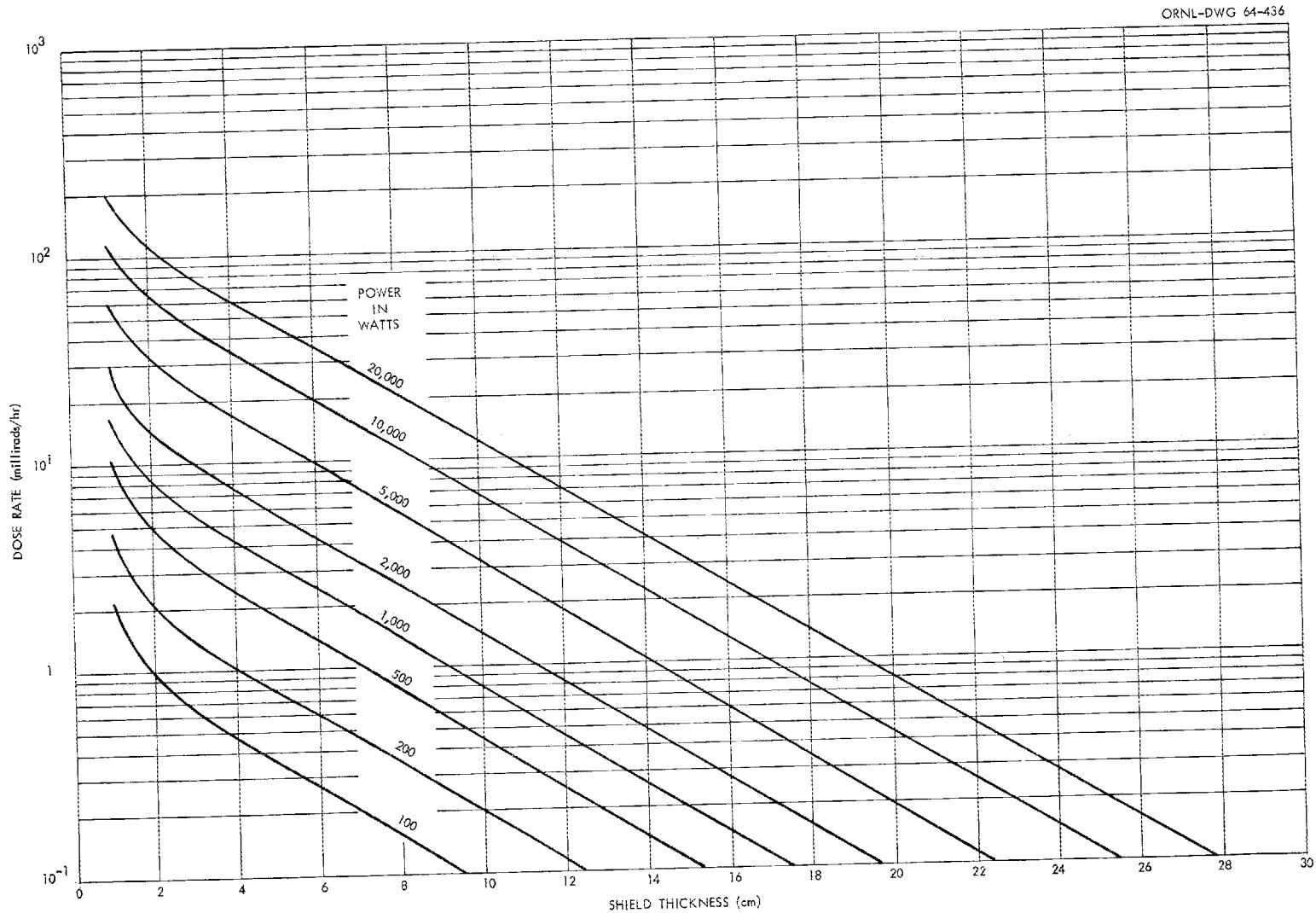


Fig. 9. Gamma Dose Rates From Iron-Shielded Isotopic Power Sources of Curium-242. Center of source to dose point separation distance = 100 cm.

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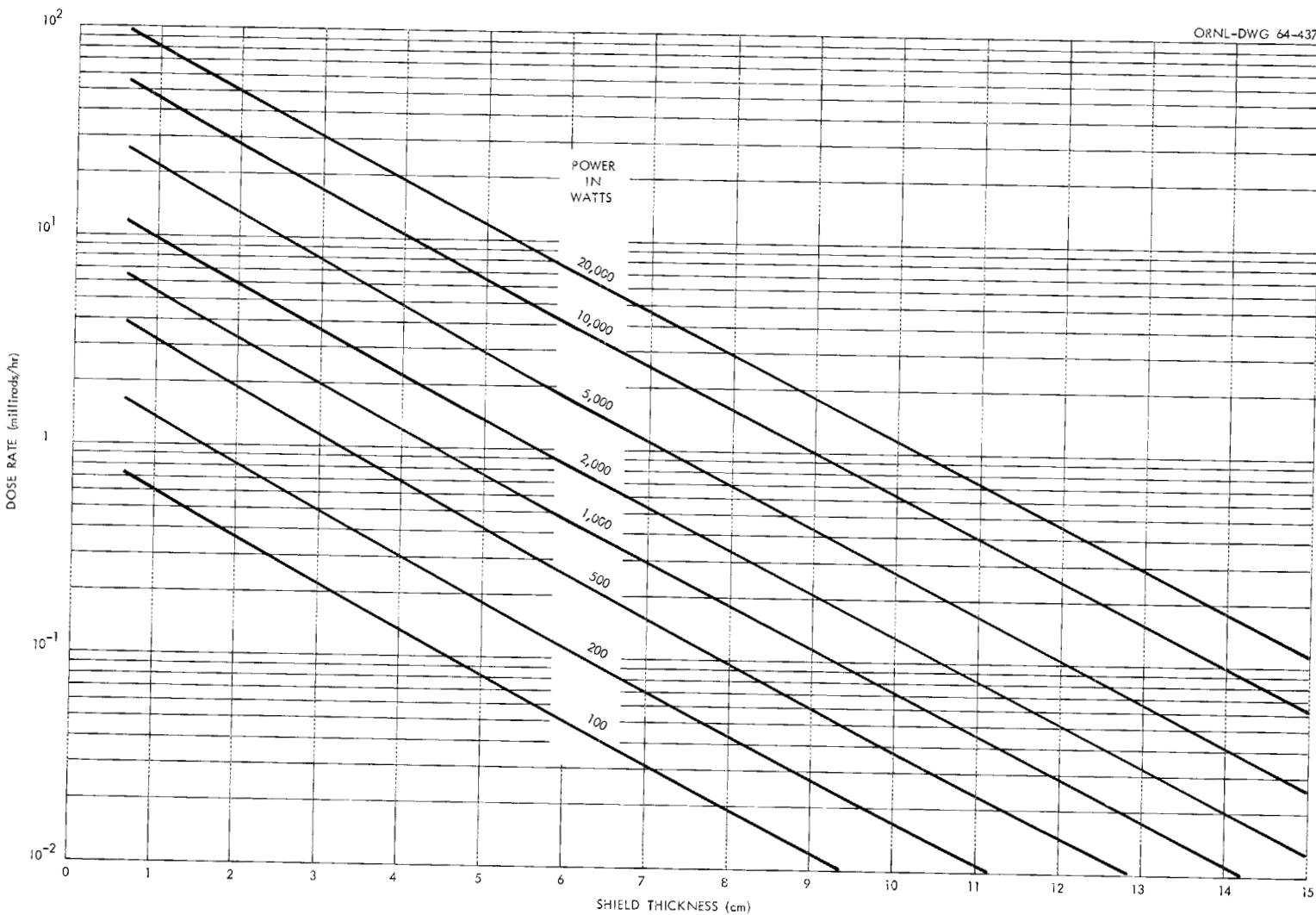


Fig. 10. Gamma Dose Rates From Lead-Shielded Isotopic Power Sources of Curium-242. Center of source to dose point separation distance = 100 cm.

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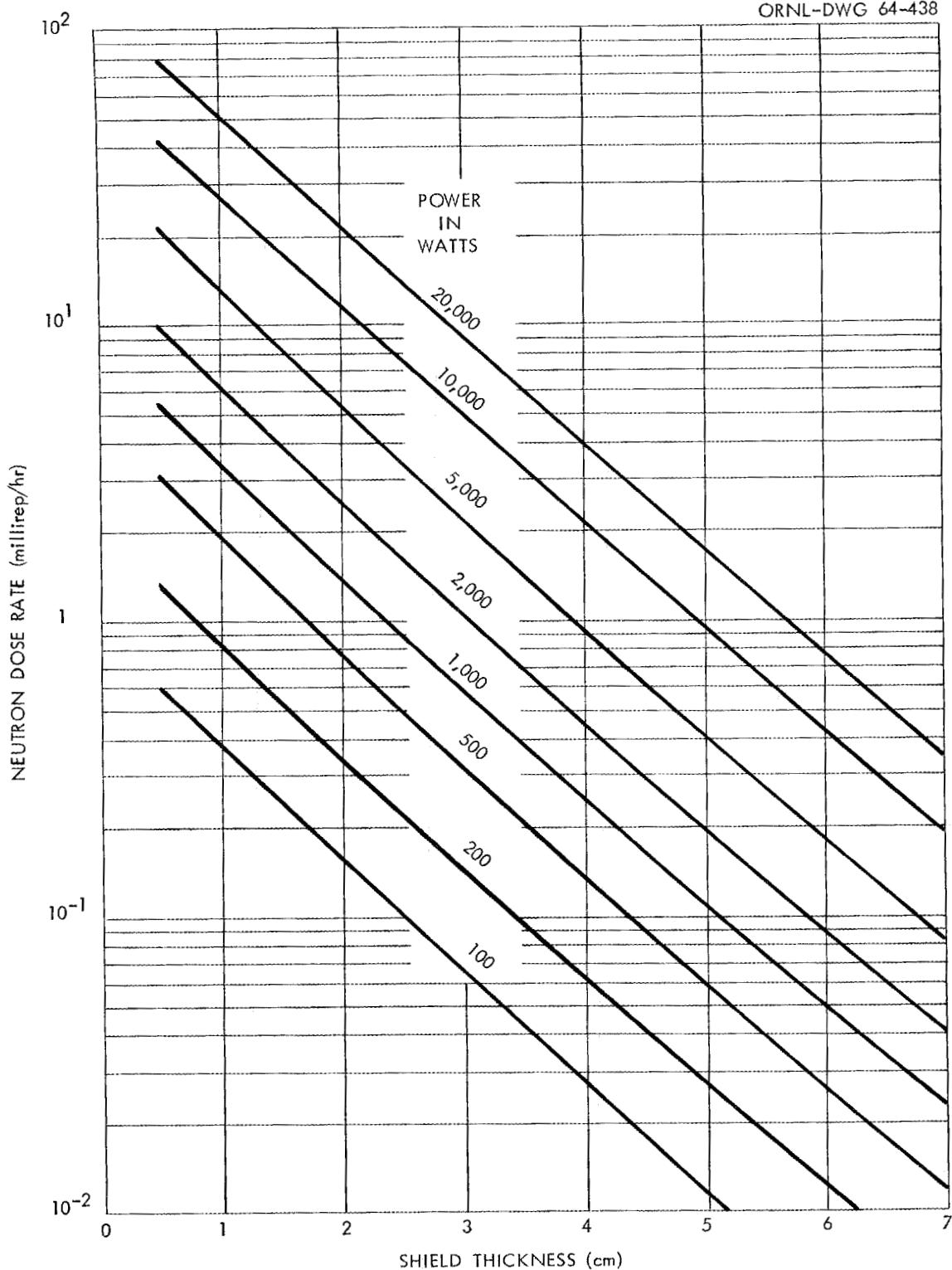


Fig. 11. Gamma Dose Rates From Uranium-Shielded Isotopic Power Sources of Curium-242. Center of source to dose point separation distance = 100 cm.

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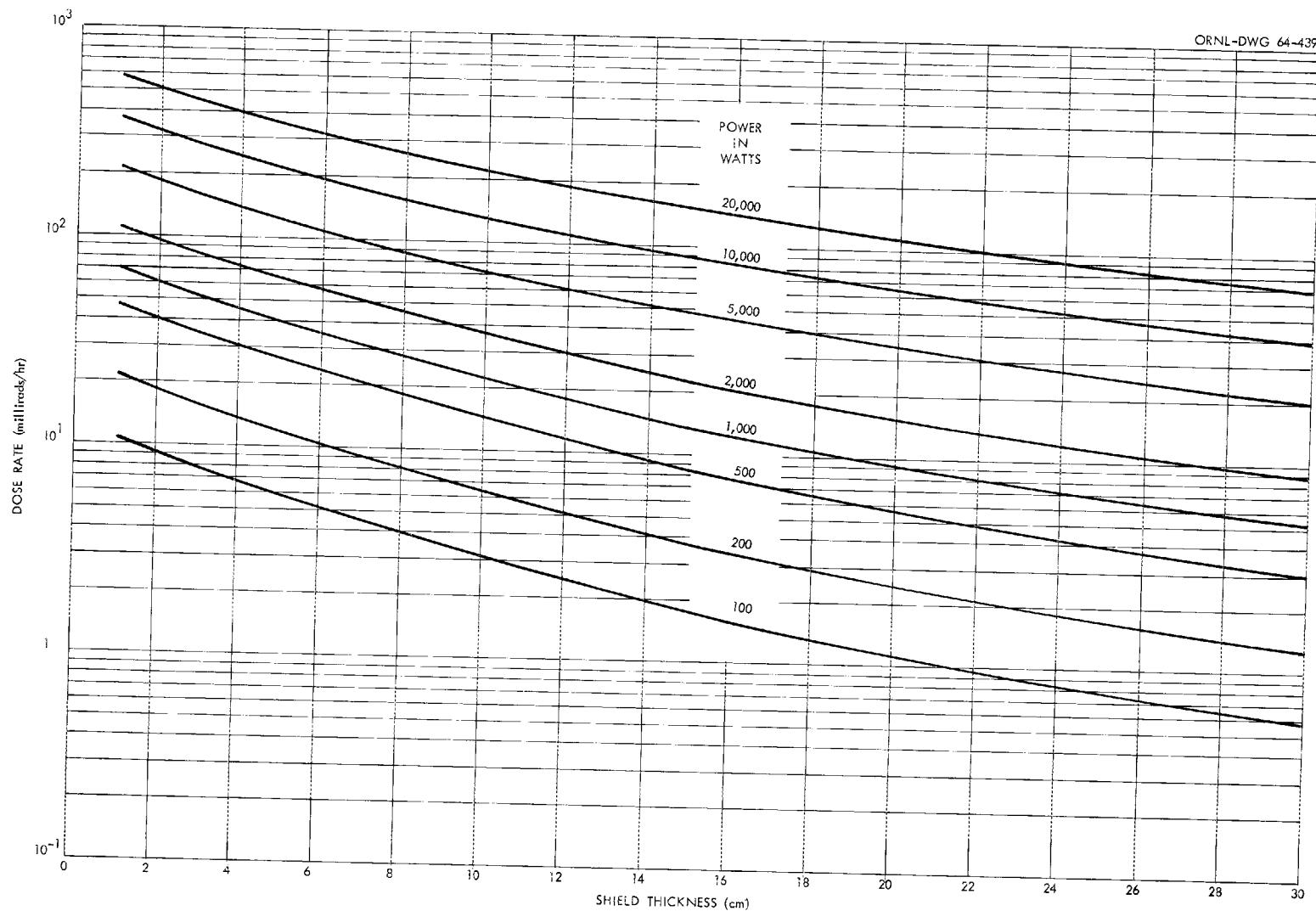


Fig. 12. Gamma Dose Rates From Water-Shielded Isotopic Power Sources of Curium-242. Center of source to dose point separation distance = 100 cm.

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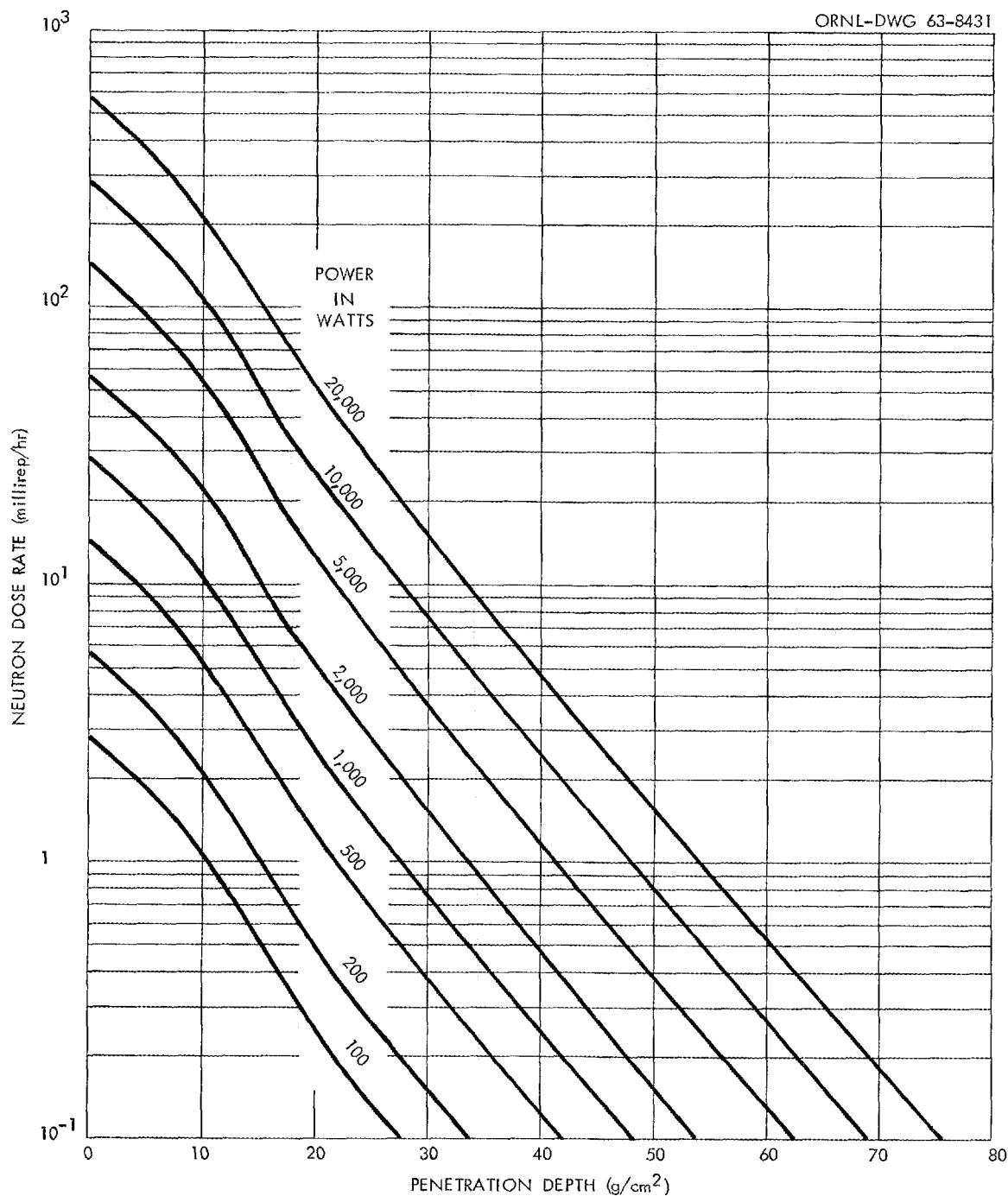


Fig. 13. Neutron Dose Rates From Water-Shielded Isotopic Power Sources of Curium-242 as a Function of Penetration Depth of Shielding Material. Center of source to dose point separation distance = 100 cm. Refer to Fig. 9 to obtain dose rates through other materials.

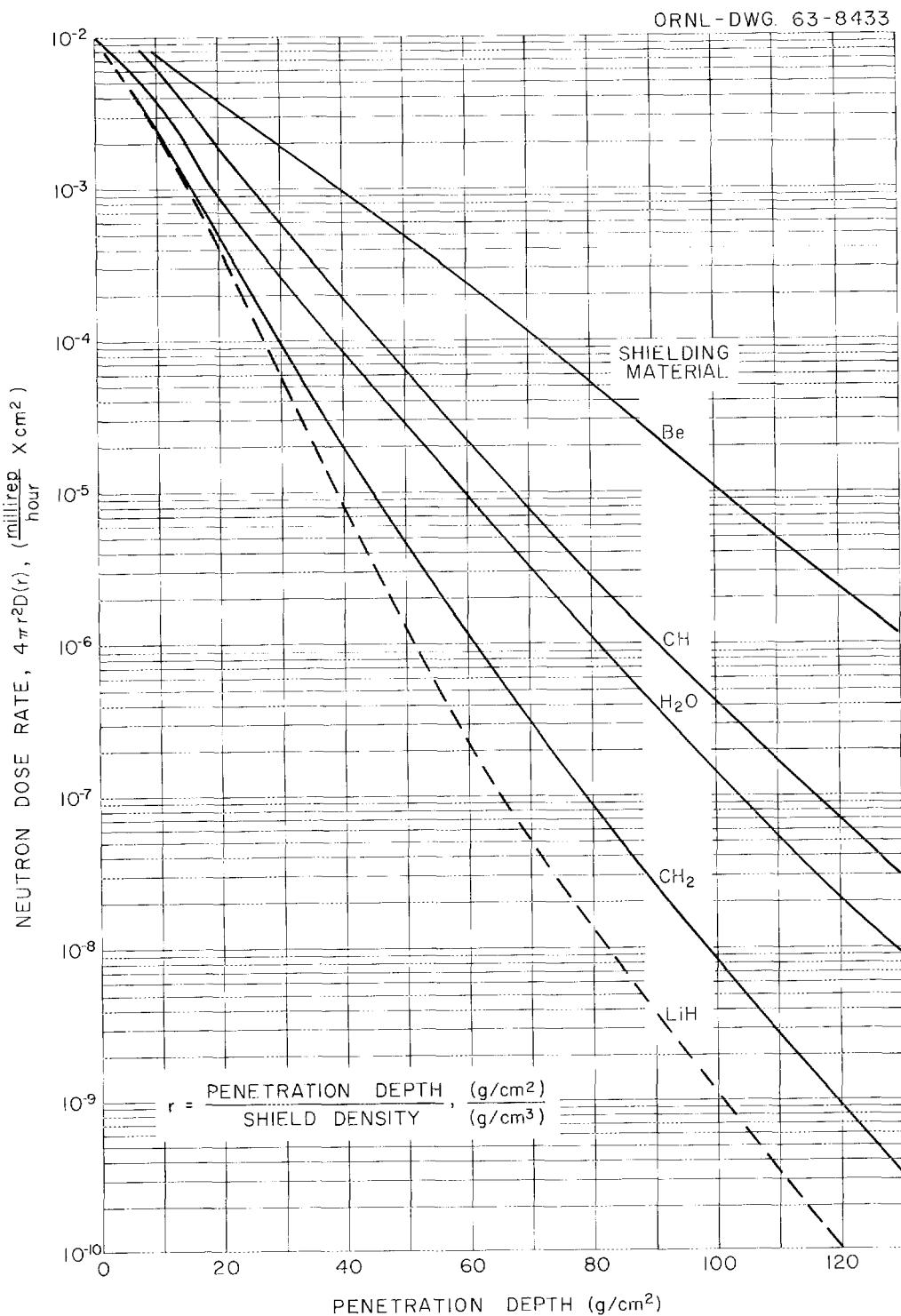


Fig. 14. Fast Neutron Dose Rate (Multiplied by  $4\pi r^2$ ) in Various Materials as a Function of Penetration Depth From a Unit Point Isotropic Fission Source.

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