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Codes P₃ and NTP₃ --- Two Versions of a P₃ Program
for Calculating Thermal Neutron Flux Distribution
in Cylindrical Cells

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SUMMARY

This report describes two versions of a machine code which solves the P₃ approximation to the single-energy Boltzmann transport equation in cylindrical geometry. The two versions differ only in the input-output routine with the P₃ calculation being the same in both. The code is an adaptation of a Hanford P₃ code, and was programmed in FORTRAN for the IBM-7090 electronic computer. It will handle up to 17 concentric cylindrical regions with a maximum of 237 spatial points. Running time for a problem with 2 points in each of 6 regions is about 3 seconds.

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INTRODUCTION

In reactor evaluation work extensive use is made of calculations in which the reactor core is subdivided into unit cells which are representative of the lattice arrangement. The nuclear calculations are then concerned with the neutron balance within this unit cell. If such calculations are rapidly performed on high-speed electronic computers, they are very useful in survey studies.

In these calculations it is desirable to know the spatial distribution of the thermal neutron flux within the cell in order to obtain an accurate neutron balance. One of the most widely used methods for obtaining this flux distribution is the P_3 approximate solution of the one-velocity Boltzmann transport equation in cylindrical geometry. This report describes one such calculation which has been found very useful.

The P_3 calculation described here was written by C. R. Richey of the Hanford Laboratory as a subroutine to the lattice parameter code, IDIOT.¹ An IDIOT Fortran deck was obtained from Mr. Richey, and the P_3 subroutine was simply lifted from this program and assembled with new input-output routines to make CODE P3 and NTP3.

The input-output routines were programmed by T. B. Fowler and C. D. Griffies.

DESCRIPTION OF CALCULATION

Since the P_3 calculation is described in References 2 and 3, no detailed description will be given here. The input-output options will be explained fully in order that the code may be easily utilized.

This calculation will treat up to 17 concentric cylindrical regions with a maximum of 237 spatial flux points. The calculation described here will not treat void regions, although the IDIOT code does make provisions to handle voids. The outermost region cannot be a fuel (heavy absorber) region; otherwise, the region assignment may be completely arbitrary.

Two different versions of the code are described in this report, CODE P3 in Part A and CODE NTP3 in Part B. CODE P3 requires the user to input macroscopic nuclear properties for each region, while CODE NTP3 contains a set of equations from which nuclear data is calculated as a function of moderator temperature and nuclide concentrations.

Part A --- CODE P3

Input

The items listed below are required as input to CODE P3. Most of the items must be input for each of the regions in the cell. These quantities are indicated under the title "ITEM" with argument 17 since there is a maximum of 17 regions. They are written in fields of ten with seven numbers per card. Each new item starts on a new card rather than utilizing any vacant fields on the last card of the preceding item.

Table 1. Input Format for CODE P3

<u>Item</u>	<u>Card No.</u>	<u>Format</u>	<u>Description</u>
TITLE	1	Columns 2-66	Any desired title
M	1	Cols. 67-72, I6	Number of regions
R(17)	2+	7E10.0	Radii of all regions, beginning at center, cm; as many cards as needed
ξ (17)	Begin on new card	7E10.0	Log mean energy decrement for each region
AMASS (17)	ditto	ditto	Effective atomic mass number for each region
POINTS (17)	ditto	ditto	Number of thermal flux points desired in each region in traverse
Σ_a (17)	ditto	ditto	Macroscopic absorption cross section in each region, cm^{-1}
Σ_s (17)	ditto	ditto	Macroscopic scattering cross section in each region, cm^{-1}
$\bar{\mu}_o$ (17)	ditto	ditto	Average cosine of scattering angle in each region

Output

The output listing from CODE P3 consists of the following:

1. A one-page summary listing the radius, average flux values, thermal utilization, cross sections, atomic mass number, and source term for each region.
2. One or more pages containing the thermal flux traverse.

The input and output for a sample problem are in Appendix C.

Part B --- CODE NTP3

One approach to obtaining average thermal cross sections to use in making a neutron balance is the concept of an effective temperature for thermal neutrons. This concept assumes that the thermal neutrons have an energy distribution corresponding to a Maxwellian distribution about some mean temperature. One then has the problem of trying to determine this mean temperature such that the reaction rate given by a Maxwell-Boltzmann energy distribution closely approximates the actual reaction rate of the thermal neutrons.

CODE NTP3 obtains the spatial distribution of the thermal flux in a unit lattice cell from the P_3 calculation and calculates thermal flux disadvantage factors. These disadvantage factors are then used to homogenize the cell and an effective neutron temperature is calculated using the neutron temperature model of Coveyou,⁴ et al.

This version of the P_3 calculation does not require nuclear data to be input by hand. All the necessary cross sections and other data have been programmed in equation form as a function of temperature (See Appendix A). The only input required are: moderator temperature, moderator mass number, number of regions and points per region, radii of all regions, and material specifications for each region. The input format for NTP3 is given below.

Table 2. Input Format for CODE NTP3

Card 1: Any Desired Title, columns 2-72

Card 2: $T_M(E10.0)$, $A_M(E10.0)$, M(I3), POINTS (I3)

Card 3+: R(17) (7E10.0), as many cards as needed to specify M regions

Card 4+: Element No. (I2); Mass (E8.0)

Blank card to signal end of region
Element No.; Mass

Blank card to signal end of region

Continue until all regions are described

If several cases are being run together, end the last region of each case with one blank card in the normal manner, then follow with the next case. The end of a series of cases is signalled by placing a total of three blank cards at the end of the last region of the last case.

Output

The output listing from NTP3 consists of the following:

1. A one-page summary listing the radius, average flux values, thermal utilization, cross sections, atomic mass number, and source term for each region.
2. One or more pages containing the thermal flux traverse.
3. A one-page listing of the thermal flux disadvantage factor for each region, the moderator temperature used, and the calculated neutron temperature.

The input and output for a sample problem are included in Appendix D.

Equations Used

The following set of equations are used in the calling program for NTP3 to prepare the average nuclear data needed by the P₃ subroutine.

$$(1) \quad V_c = \pi R_M^2$$

$$(2) \quad V_i = \pi (R_i^2 - R_{i-1}^2)$$

$$(3) \quad N_{ij} = \frac{M_{ij}}{V_i} \cdot \frac{0.6023}{(MW)_j}$$

$$(4) \quad \sigma_a^j = \text{function of } T_N; \text{ see Appendix A}$$

$$(5) \quad \sigma_s^j = \sigma_a^j \text{ from Table A-2}$$

$$(6) \quad \Sigma_a^i = \sum_{\text{all } j} N_{ij} \sigma_a^j (T_M)$$

$$(7) \quad \Sigma_s^i = \sum_{\text{all } j} N_{ij} \sigma_s^j$$

$$(8) \quad \bar{\mu}_o^i = \frac{1}{\Sigma_s^i} \sum_{\text{all } j} \bar{\mu}_o^j N^{ij} \sigma_s^j$$

$$(9) \quad \bar{\xi}^i = \frac{1}{\Sigma_s^i} \sum_{\text{all } j} \xi^j N^{ij} \sigma_s^j$$

$$(10) \quad \bar{A}^i = 2/3 \bar{\mu}_o^i$$

(11) Call P₃ Calculation; calculate $\bar{\phi}_i$, average thermal flux in each region

$$(12) \quad \xi_i = \frac{\bar{\phi}_i}{\bar{\phi}_1}, \text{ flux disadvantage factors}$$

$$(13) \quad T_N = T_M \left\{ 1 + 1.11 A_M \sqrt{\frac{2}{\pi}} \sqrt{\frac{2}{3}} \sqrt{\frac{293}{T_M}} \frac{\sum_{i=1}^M \frac{V_i}{V_c} \xi_i \Sigma_a^i (20^\circ C)}{\sum_{i=1}^M \frac{V_i}{V_c} \xi_i \Sigma_s^i} \right\}$$

Notation Used in NTP3

1. i Region identification, $i = 1 - M$
2. j Element identification, $j = 1 - 40$
3. M Number of regions in problem, $M = 1 - 17$
4. R_i Radius of region i , cm
5. V_c Volume of the cell per unit length, cc/cm
6. V_i Volume of region i per unit length, cc/cm
7. M_{ij} Mass of element j in region i per unit cell length, grams/cm
8. MW_j Molecular weight of element j
9. σ_a^j Microscopic absorption cross section for element j , barns
10. σ_s^j Scattering cross section, barns
11. $\bar{\mu}_o^j$ Average cosine of the scattering angle
12. ξ^j Average logarithmic energy decrement
13. \bar{A}^i Average mass number for region i
14. A_M Moderator mass number
15. T_M Moderator temperature, °K
16. T_N Average neutron temperature, °K
17. ξ_i Thermal flux disadvantage factor for region i .

REFERENCES

1. C. R. Richey, "IDIOT -- A Lattice Parameter Code for the IBM-709," HW-63411, January 7, 1960.
2. D. D. Matsumoto and C. R. Richey, "Program on the 709 Digital Computer of the P_3 Approximation to the Boltzmann Transport Equation in Cylindrical Geometry," HW-60781, June 17, 1959.
3. C. R. Richey, "The Calculation of the Thermal Neutron Flux Distribution in a Unit Lattice Cell, Comparison of Experiment and Theory," Sept. 23, 1957.
4. R. R. Coveyou, R. R. Bate, and R. K. Osborn, "Effect of Moderator Temperature Upon Neutron Flux in Infinite, Capturing Medium," ORNL-1958, October 20, 1955.

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APPENDIX A

Nuclear Data Used in CODE NTP3

All the nuclear data needed in CODE NTP3 has been included as part of the program. The relationship between absorption cross section and neutron temperature has been approximated by simple functions for the isotopes of general interest in reactor evaluation work.

For most of the nuclides, the relationship between cross section and temperature was assumed to be of the form:

$$\sigma_a(T) \simeq aT^b, \quad (A-1)$$

where T is in degrees Kelvin

Table A-1 lists the appropriate value for a and b for the nuclides considered. Table A-2 lists additional nuclear data used in the code.

Table A-1. Values of a and b for the Isotopes

<u>Element No. (j)</u>	<u>Isotope*</u>	<u>a</u>	<u>b</u>
1	Thorium (232)	114.683	- 0.5
2	Uranium (234)	2240.0	- 0.5421
3	Uranium (236)	3317.0	- 1.0703
4	Uranium (238)	41.110	- 0.5
9	Protactinium (233)	773.657	- 0.5
10	Uranium (233)	7144.0	- 0.4635
11	Uranium (235)	13,250.0	- 0.5476
12	Neptunium (239)	1061.27	- 0.5
13	Plutonium (242)	455.092	- 0.5
14	Americum (243)	2396.41	- 0.5
15	Plutonium (239)	See Equation (A-2)	
16	Plutonium (240)	See Equation (A-3)	
17	Plutonium (241)	See Equation (A-4)	
18	Light water	10.06494	- 0.5
19	Heavy water	0.027901	- 0.5
20	Sodium	7.95952	- 0.5
21	Oxygen	0	0
22	Helium	0	0
23	Beryllium	0.15166	- 0.5
24	Boron	11,383.0	- 0.5
25	Carbon	0.056487	- 0.5
26	Magnesium	1.04758	- 0.5
27	Aluminum	3.66309	- 0.5
28	Stainless Steel	43.82013	- 0.5
29	Manganese	200.24	- 0.5
30	Copper	58.40	- 0.5
31	Nitrogen	28.519	- 0.5
32	Sulfur	7.888	- 0.5
33	Iron	39.745	- 0.5
34	Chromium	47.03	- 0.5
35	Zircalloy-2	2.80723	- 0.5
36	Zircalloy-4	2.76961	- 0.5

Table A-1 cont'd

<u>Element No. (j)</u>	<u>Isotope*</u>	<u>a</u>	<u>b</u>
37	Nickel	69.781	- 0.5
38	Fluorine	0.15170	- 0.5
39	(Blank)	0	0
40	(Blank)	0	0

* When the particular isotope is not indicated, the naturally occurring mixture is implied.

Table A-2. Other Nuclear Data for the Isotopes

<u>Element No. (j)</u>	<u>MW_j</u>	<u>σ_s^j</u>	<u>$\bar{\mu}_o^j$</u>	<u>ξ^j</u>
1	232	12.5	2.87×10^{-3}	8.59×10^{-3}
2	234	9.0	2.85	8.52
3	236	10.0	2.82	8.45
4	238	9.0	2.80	8.38
9	233	10.0	2.86	8.56
10	233	12.5	2.86	8.56
11	235	12.5	2.84	8.51
12	239	10.0	2.79	8.37
13	242	9.0	2.75	8.24
14	243	10.0	2.74	8.22
15	239	12.0	2.79	8.37
16	240	9.0	2.78	8.31
17	241	12.0	2.77×10^{-3}	8.28×10^{-3}
18	18	75.0	(Eq. A-5)	0.925
19	20	12.9	0.19	0.506
20	23	3.4	0.029	0.0845
21	16	4.0	0.0417	0.113
22	4	0.8	0.167	0.425
23	9	5.8	0.0741	0.209
24	10.82	4.4	0.0667	0.184
25	12	4.8	0.0556	0.158
26	24.32	3.6	0.0274	0.0822
27	27	1.5	0.0247	0.0724
28	54.87	9.67	0.01215	0.0364
29	54.93	2.3	0.0122	0.0363
30	63.54	7.5	0.0106	0.0314
31	14	11.0	0.048	0.1373
32	32.07	1.2	0.021	0.0616
33	55.85	11.8	0.012	0.0357
34	52.01	4.3	0.0129	0.0383
35	91.22	6.25	0.00731	0.0218

Table A-2. cont'd

<u>Element No. (j)</u>	<u>MW_j</u>	<u>σ_s^j</u>	<u>μ̄_o^j</u>	<u>ξ^j</u>
36	91.22	6.25	0.00731	0.0218
37	58.69	17.5	0.0115	0.034
38	19	4.0	0.0351	0.102
39	-	-	-	-
40	-	-	-	-

The nuclear properties not satisfied by Equation (A-1) or given in Tables A-1 and A-2 are given below.

$$\begin{aligned} \sigma_a^{15}(T) = & 1753.6 - 5.0936T + 1.0057 \times 10^{-2} T^2 \\ & - 6.8093 \times 10^{-6} T^3 + 1.5237 \times 10^{-9} T^4, \end{aligned} \quad (A-2)$$

$$\begin{aligned} \sigma_a^{16}(T) = & 505.22 - 0.74719 T + 6.7052 \times 10^{-4} T^2 \\ & - 2.07784 \times 10^{-7} T^3, \end{aligned} \quad (A-3)$$

$$\begin{aligned} \sigma_a^{17}(t) = & 2216.2 - 5.2166T + 9.362 \times 10^{-3} T^2 \\ & - 7.1727 \times 10^{-6} T^3 + 1.9745 \times 10^{-9} T^4, \end{aligned} \quad (A-4)$$

$$\bar{\mu}_o^{18}(T) = 0.58866 - 3.76744 T_M^{-0.5} - 20.8016 T_M^{-1}, \quad (A-5)$$

APPENDIX B

Lists of Fortran Programs

Table B-1. Calling Program for CØDE P3

Table B-2. Calling Program for CØDE NTP3

Table B-3. List of the P_3 Subroutine

Table B-1. Calling Program for CODE P3

C1805 CALLING PROGRAM FOR P3 SUBROUTINE	1805 CDG	18050103
DIMENSIONHOL(12),R(17),TSI(17),AMASS(17),POINTS(17),		18050105
1SIGA(17),SIGS(17),PE1(17),PHIBAR(17),THERMU(17)		18050107
1 READINPUTTAPE10,1000,(HOL(I),I=1,11),M		18050101
IF(M)777,777,2		18050103
2 READINPUTTAPE10,1001,(R(I),I=1,M)		18050105
READINPUTTAPE10,1001,(TSI(I),I=1,M)		18050117
READINPUTTAPE10,1001,(AMASS(I),I=1,M)		18050119
READINPUTTAPE10,1001,(POINTS(I),I=1,M)		18050121
READINPUTTAPE10,1001,(SIGA(I),I=1,M)		18050123
READINPUTTAPE10,1001,(SIGS(I),I=1,M)		18050125
READINPUTTAPE10,1001,(PE1(I),I=1,M)		18050201
CALLP3(HOL,M,R,TSI,AMASS,POINTS,SIGA,SIGS,PE1,		18050203
1PHIBAR,THERMU)		18050205
GOTO1		18050207
777 CALLEXIT		18050209
1000 FORMAT(11A6,I6)		18050109
1001 FORMAT(7E10.0)		18050213
END		18050217

Table B-2. Calling Program for CODE NTP3

*	CALLING PROGRAM FOR NTP3	18050101
	DIMENSION R(17),TSI(17),AMASS(17),POINTS(17),	18050103
	1SIGA(17),SIGS(17),PEI(17),XMAS(17,40),	18050105
	2PHIBAR(17),THERMU(17),VOL(17),DEN(17,40),	18050107
	3SSIGA2(40),SSIGAT(40),SSIGS2(40),CONA(40),	18050109
	4CONEQ1(40),CONEQ2(40),CONSP(40),XMUBD(17,40),XSEE(17,40),	18050111
	5CONMU(40),CONSI(40),SIGA2D(17),HOL(12),PRATIO(17)	18050113
100	READ INPUT TAPE 10,1001,(HOL(I),I#1,12)	18050115
	READ INPUT TAPE 10,1003,TEMPM,XMODA,M,NPOIT	18050117
	IF(TEMPM)101,107,101	18050119
101	DO 102 I # 1,M	18050121
102	POINTS(I) # FLOATF(NPOIT)	18050123
	READ INPUT TAPE 10,1002,(R(I),I#1,M)	18050201
	DO 103 I # 1,M	18050203
	DO 103 J # 1,40	18050205
103	XMAS(I,J) # 0.0	18050207
	DO 106 I # 1,M	18050209
104	READ INPUT TAPE 10,1004,JJJ,XJJJ	18050211
	IF(JJJ)106,106,105	18050213
105	XMAS(I,JJJ) # XJJJ	18050215
	GO TO 104	18050217
106	CONTINUE	18050219
	CALL NTP3(HOL,M,POINTS,TEMPM,XMODA,XMAS,R,	18050103
	ITEMPN,PRATIO)	18050223
	WRITE OUTPUT TAPE 9,1000	18050301
	WRITE OUTPUT TAPE 9,1001,(HOL(I),I#1,12)	18050303
	WRITE OUTPUT TAPE 9,1005,TEMPM,ITEMPN	18050305
	WRITE OUTPUT TAPE 9,1006	18050307
	WRITE OUTPUT TAPE 9,1007,(PRATIO(I),I#1,M)	18050309
	WRITE OUTPUT TAPE 9,1000	18050311
	GO TO 100	18050313
1000	FORMAT(1H1)	18050401
1001	FORMAT(12A6)	18050403
1002	FORMAT(7E10.0)	18050405

1003 FORMAT(2E10.0,2I3)	18050407
1004 FORMAT(I2,E8.0)	18050409
1005 FORMAT(10HD MOD TEMP1PE13.6, 115H NEUT TEMPE13.6)	18050411
1006 FORMAT(30HD FLUX DISADVANTAGE FACTORS(I))	18050415
1007 FORMAT(IH 1P8E15.6)	18050417
107 CALL EXIT	18050419
END	18050421
*TYPE(FORTRAN)	
* SUBROUTINE NTP3 TBF 9204-1	18050101
SUBROUTINE NTP3(HOL,M,POINTS,TEMPPM,XMODA,XMAS,R, ITEMPN,PRATIO)	18050105
DIMENSION R(17),TSI(17),AMASS(17),POINTS(17), !SIGA(17),SIGS(17),PE1(17),XMAS(17,40), 2PHIBAR(17),THERMU(17),VOL(17),DEN(17,40), 3SSIGA2(40),SSIGAT(40),SSIGS2(40),CONA(40), 4CONEQ1(40),CONEQ2(40),CONSP(20),XMUB0(17,40),XSEE(17,40), 5CONMU(40),CONSI(40),SIGA20(17),HOL(12),PRATIO(17) IF(TEMPPM)900,901,901	18050109 18050111 18050113 18050115 18050117 18050119 18051517
900 III#1 TEMPPM#ABSF(TEMPPM)	18051519 18051520
GO TO 100	
901 III#0	18051523
100 CONA(1) # 232.0	18050201
CONA(2) # 234.0	18050203
CONA(3) # 236.0	18050205
CONA(4) # 238.0	18050207
CONA(5) # 1.0	18050209
CONA(6) # 1.0	18050211
CONA(7) # 1.0	18050213
CONA(8) # 1.0	18050215
CONA(9) # 233.0	18050217
CONA(10) # 233.0	18050219
CONA(11) # 235.0	18050221
CONA(12) # 239.0	18050223
CONA(13) # 242.0	18050225
CONA(14) # 243.0	18050301
CONA(15) # 239.0	18050303

CONA(16) # 240.0	18050305
CONA(17) # 241.0	18050307
CONA(18) # 18.0	18059901
CONA(19) # 20.0	18059903
CONA(20) # 23.0	18050313
CONA(21) # 16.0	18050315
CONA(22) # 4.0	18050317
CONA(23) # 9.0	18050319
CONA(24) # 10.82	18050321
CONA(25) # 12.0	18050323
CONA(26) # 24.32	18050325
CONA(27) # 27.0	18050401
CONA(28) # 54.87	18050403
CONA(29) # 54.93	18050405
CONA(30) # 63.54	18050407
CONA(31) # 14.0	18050409
CONA(32) # 32.07	18050411
CONA(33) # 55.85	18050413
CONA(34) # 52.01	18050415
CONA(35) # 91.22	18050417
CONA(36) # 91.22	18050419
CONA(37) # 58.69	18050421
CONA(38) # 19.0	
CONA(39) # 7.0	
CONA(40) # 1.0	18050425
CONEQ1(2) # 2240.0	18050502
CONEQ1(3) # 3317.0	18050503
CONEQ1(5) # 0.0	18050505
CONEQ1(6) # 0.0	18050506
CONEQ1(7) # 0.0	18050507
CONEQ1(8) # 0.0	18050508
CONEQ1(10) # 7144.0	18050510
CONEQ1(11) # 13250.0	18050511
CONEQ1(15) # 0.0	18050515
CONEQ1(16) # 0.0	18050516
CONEQ1(17) # 0.0	18050517
CONEQ1(21) # 0.0	18050521
CONEQ1(22) # 0.0	18050522

CONEQ1(38) # 0.1517	
CONEQ1(39) # 1.4335	
CONEQ1(40) # 0.0	18050615
CONEQ1(1) # 114.683	CORR0001
CONEQ1(4) # 41.110	CORR0002
CONEQ1(9) # 773.657	CORR0003
CONEQ1(12) # 1061.2689	CORR0004
CONEQ1(13) # 455.092	CORR0005
CONEQ1(14) # 2396.41	CORR0006
CONEQ1(18) # 10.06494	CORR0007
CONEQ1(19) # 0.027901	CORR0008
CONEQ1(20) # 7.95952	CORR0009
CONEQ1(23) # 0.15166	CORR0010
CONEQ1(24) # 11383.0	CORR0011
CONEQ1(25) # 0.056487	CORR0012
CONEQ1(26) # 1.04758	CORR0013
CONEQ1(27) # 3.66309	CORR0014
CONEQ1(28) # 43.82013	CORR0015
CONEQ1(29) # 200.24	CORR0016
CONEQ1(30) # 58.40	CORR0017
CONEQ1(31) # 28.519	CORR0018
CONEQ1(32) # 7.888	CORR0019
CONEQ1(33) # 39.745	CORR0020
CONEQ1(34) # 47.03	CORR0021
CONEQ1(35) # 2.80723	CORR0022
CONEQ1(36) # 2.76961	CORR0023
CONEQ1(37) # 69.781	CORR0024
CONEQ2(1) # -0.5	18050701
CONEQ2(2) # -0.5421	18050703
CONEQ2(3) # -1.0703	18050705
CONEQ2(4) # -0.5	18050707
CONEQ2(5) # 0.0	18050709
CONEQ2(6) # 0.0	18050711
CONEQ2(7) # 0.0	18050713
CONEQ2(8) # 0.0	18050715
CONEQ2(9) # -0.5	18050717
CONEQ2(10) # -0.4635	18050719
CONEQ2(11) # -0.5476	18050721

CONEQ2(12) # -0.5	18050723
CONEQ2(13) # -0.5	18050725
CONEQ2(14) # -0.5	18050801
CONEQ2(15) # 0.0	18050803
CONEQ2(16) # 0.0	18050805
CONEQ2(17) # 0.0	18050807
CONEQ2(18) # -0.5	18050809
CONEQ2(19) # -0.5	18050811
CONEQ2(20) # -0.5	18050813
CONEQ2(21) # 0.0	18050815
CONEQ2(22) # 0.0	18050817
DO 101 I # 23,37	18050819
101 CONEQ2(I) # -0.5	18050821
CONEQ2(38) # -0.5	18050825
CONEQ2(39) # -0.5	18050901
CONEQ2(40) # 0.0	18050902
CONSP(1) # 1753.6	18050903
CONSP(2) # 5.0936	18050904
CONSP(3) # 1.0057E-2	18050905
CONSP(4) # 6.8093E-6	18050906
CONSP(5) # 1.5237E-9	18050907
CONSP(6) # 505.22	18050908
CONSP(7) # 0.74719	18050909
CONSP(8) # 6.7052E-4	18050910
CONSP(9) # 2.07784E-7	18050911
CONSP(10) # 2216.2	18050912
CONSP(11) # 5.2166	18050913
CONSP(12) # 9.362E-3	18050914
CONSP(13) # 7.1727E-6	18050915
CONSP(14) # 1.9745E-9	18050916
CONSP(15) # 222.84	18050917
CONSP(16) # 1.1807	18050918
CONSP(17) # 0.0	18050919
CONSP(18) # 0.0	18050920
CONSP(19) # 0.0	18051001
CONSP(20) # 0.0	18051002
SSIQS2(1) # 12.5	
SSIQS2(2) # 9.0	

SSIGS2(3) # 10.0	18051003
SSIGS2(4) # 9.0	18051004
SSIGS2(5) # 0.0	18051005
SSIGS2(6) # 0.0	18051006
SSIGS2(7) # 0.0	18051007
SSIGS2(8) # 0.0	18051008
SSIGS2(9) # 10.0	18051009
SSIGS2(10) # 12.5	18051010
SSIGS2(11) # 12.5	18051011
SSIGS2(12) # 10.0	18051012
SSIGS2(13) # 9.0	18051013
SSIGS2(14) # 10.0	18051014
SSIGS2(15) # 12.0	18051015
SSIGS2(16) # 9.0	18051016
SSIGS2(17) # 12.0	18051017
SSIGS2(18) # 75.0	18051018
SSIGS2(19) # 12.9	18051019
SSIGS2(20) # 3.4	18051020
SSIGS2(21) # 4.0	18051021
SSIGS2(22) # 0.8	18051022
SSIGS2(23) # 5.8	18051023
SSIGS2(24) # 4.4	18051024
SSIGS2(25) # 4.8	18051025
SSIGS2(26) # 3.6	18051101
SSIGS2(27) # 1.5	18051102
SSIGS2(28) # 9.67	18051103
SSIGS2(29) # 2.3	18051104
SSIGS2(30) # 7.5	18051105
SSIGS2(31) # 11.0	18051106
SSIGS2(32) # 1.2	18051107
SSIGS2(33) # 11.8	18051108
SSIGS2(34) # 4.3	18051109
SSIGS2(35) # 6.25	18051110
SSIGS2(36) # 6.25	18051111
SSIGS2(37) # 17.5	18051112
SSIGS2(38) # 4.0	
SSIGS2(39) # 1.5	
SSIGS2(40) # 0.0	18051115

CONMU(1) # 2.87E-3	18051201
CONMU(2) # 2.85E-3	18051202
CONMU(3) # 2.82E-3	18051203
CONMU(4) # 2.80E-3	18051204
CONMU(5) # 0.0	18051205
CONMU(6) # 0.0	18051206
CONMU(7) # 0.0	18051207
CONMU(8) # 0.0	18051208
CONMU(9) # 2.86E-3	18051209
CONMU(10) # 2.86E-3	18051210
CONMU(11) # 2.84E-3	18051211
CONMU(12) # 2.79E-3	18051212
CONMU(13) # 2.75E-3	18051213
CONMU(14) # 2.74E-3	18051214
CONMU(15) # 2.79E-3	18051215
CONMU(16) # 2.78E-3	18051216
CONMU(17) # 2.77E-3	18051217
CONMU(18) # 0.58866-3.76744*/{SQRTF(TEMPPM)}- 120.8016/TEMPPM	18059905
CONMU(19) # 0.19	18059907
CONMU(20) # 2.9E-2	18051219
CONMU(21) # 0.0417	18051220
CONMU(22) # 0.167	18051221
CONMU(23) # 0.0741	18051222
CONMU(24) # 0.0667	18051223
CONMU(25) # 0.0556	18051224
CONMU(26) # 2.74E-2	18051225
CONMU(27) # 2.47E-2	18051301
CONMU(28) # 1.215E-2	18051302
CONMU(29) # 0.0122	18051303
CONMU(30) # 0.0106	18051304
CONMU(31) # 0.048	18051305
CONMU(32) # 0.021	18051306
CONMU(33) # 0.012	18051307
CONMU(34) # 0.0129	18051308
CONMU(35) # 7.31E-3	18051309
CONMU(36) # 7.31E-3	18051310
CONMU(37) # 0.0115	18051311
	18051312

CONMU(38) # 0.0351	
CONMU(39) # 0.0953	
CONMU(40) # 0.0	18051315
CONSI(1) # 8.59E-3	18051401
CONSI(2) # 8.52E-3	18051402
CONSI(3) # 8.45E-3	18051403
CONSI(4) # 8.38E-3	18051404
CONSI(5) # 0.0	18051405
CONSI(6) # 0.0	18051406
CONSI(7) # 0.0	18051407
CONSI(8) # 0.0	18051408
CONSI(9) # 8.56E-3	18051409
CONSI(10) # 8.56E-3	18051410
CONSI(11) # 8.51E-3	18051411
CONSI(12) # 8.37E-3	18051412
CONSI(13) # 8.24E-3	18051413
CONSI(14) # 8.22E-3	18051414
CONSI(15) # 8.37E-3	18051415
CONSI(16) # 8.31E-3	18051416
CONSI(17) # 8.28E-3	18051417
CONSI(18) # 0.925	18051418
CONSI(19) # 0.506	18051419
CONSI(20) # 8.45E-2	18051420
CONSI(21) # 0.113	18051421
CONSI(22) # 0.425	18051422
CONSI(23) # 0.209	18051423
CONSI(24) # 0.184	18051424
CONSI(25) # 0.158	18051425
CONSI(26) # 8.22E-2	18051501
CONSI(27) # 7.24E-2	18051502
CONSI(28) # 3.64E-2	18051503
CONSI(29) # 0.0363	18051504
CONSI(30) # 0.0314	18051505
CONSI(31) # 0.1373	18051506
CONSI(32) # 0.0616	18051507
CONSI(33) # 0.0357	18051508
CONSI(34) # 0.0383	18051509
CONSI(35) # 2.18E-2	18051510

CONSI(36) # 2.18E-2	18051511
CONSI(37) # 0.034	18051512
CONSI(38) # 0.102	
CONSI(39) # 0.268	
CONSI(40) # 0.0	18051515
I02 VOLC # 3.141593*R(M)**2	18051601
VOL(I) # 3.141593*R(I)**2	18051603
DO I03 I # 2,M	18051605
I03 VOL(I) # 3.141593*(R(I)**2-R(I-1)**2)	18051607
DO I04 I # 1,17	18051609
DO I04 J # 1,40	18051611
I04 DEN(I,J) # 0.0	18051613
DO I05 I # 1,M	18051615
DO I05 J # 1,40	18051617
I05 DEN(I,J) # XMAS(I,J)*0.6023/(VOL(I)*CONA(J))	18059901
DO I06 J # 1,14	18051701
SSIGAT(J) # CONEQ1(J)*(TEMPM**CONEQ2(J))	18051703
I06 SSIGA2(J) # CONEQ1(J)*(293.0**CONEQ2(J))	18051705
HEC1 # TEMPM**2	18051707
HEC2 # TEMPM**3	18051709
HEC3 # TEMPM**4	18051711
HEC4 # 293.0**2	18051713
HEC5 # 293.0**3	18051715
HEC6 # 293.0**4	18051717
SSIGAT(15) # CONSP(1)-CONSP(2)*TEMPM+	18051719
I CONSP(3)*HEC1-CONSP(4)*HEC2+CONSP(5)*HEC3	18051721
SSIGA2(15) # CONSP(1)-CONSP(2)*293.0+	18051723
I CONSP(3)*HEC4-CONSP(4)*HEC5+CONSP(5)*HEC6	18051725
SSIGAT(16) # CONSP(6)-CONSP(7)*TEMPM+	18051801
I CONSP(8)*HEC1-CONSP(9)*HEC2	18051803
SSIGA2(16) # CONSP(6)-CONSP(7)*293.0+	18051805
I CONSP(8)*HEC4-CONSP(9)*HEC5	18051807
SSIGAT(17) # CONSP(10)-CONSP(11)*TEMPM+	18051809
I CONSP(12)*HEC1-CONSP(13)*HEC2+CONSP(14)*HEC3	18051811
SSIGA2(17) # CONSP(10)-CONSP(11)*293.0+	18051813
I CONSP(12)*HEC4-CONSP(13)*HEC5+CONSP(14)*HEC6	18051815
DO I07 J # 18,40	18051817
SSIGAT(J) # CONEQ1(J)*(TEMPM**CONEQ2(J))	18051819

107	SSIGA2(J) # CONEQ1(J)*(293.0**CONEQ2(J))	18051821
	DO 108 I # 1,M	18051901
	SIGA(I) # 0.0	18051903
	SIGS(I) # 0.0	18051905
	SIGA2D(I) # 0.0	18051906
	DO 108 J # 1,40	18051907
	SIGA(I) # SIGA(I)+DEN(I,J)*SSIGAT(J)	18051909
	SIGS(I) # SIGS(I)+DEN(I,J)*SSIGS2(J)	18051911
	SIGA2D(I) # SIGA2D(I)+DEN(I,J)*SSIGA2(J)	18051913
108	CONTINUE	18051915
	DO 109 I # 1,M	18051917
	DO 109 J # 1,40	18051919
	XMUBD(I,J) # CONMU(J)	18051921
109	XSEE(I,J) # CONSI(J)	18051923
	DO 111 I # 1,M	18052001
	PEI(I) # 0.0	18052003
	TSI(I) # 0.0	18052005
	DO 110 J # 1,40	18052007
	HEC # DEN(I,J)*SSIGS2(J)	18052009
	PEI(I) # PEI(I)+XMUBD(I,J)*HEC	18052011
110	TSI(I) # TSI(I)+XSEE(I,J)*HEC	18052013
	PEI(I) # PEI(I)/SIGS(I)	18052015
	TSI(I) # TSI(I)/SIGS(I)	18052017
111	AMASS(I) # 2.0/(3.0*PEI(I))	18052019
	CALLP3(HOL,M,R,TSI,AMASS,POINTS,	18052021
	SIGA,SIGS,PEI,PHIBAR,THERMU)	18052023
	HEC1 # 0.0	18052101
	HEC2 # 0.0	18052103
	DO 112 I # 1,M	18052105
	PRATIO(I) # PHIBAR(I)/PHIBAR(I)	18052107
	HEC1 # HEC1+(VOL(I)/VOLC)*PRATIO(I)*SIGA2D(I)	18052109
112	HEC2 # HEC2+(VOL(I)/VOLC)*PRATIO(I)*SIGS(I)	18052111
	TEMPPN # TEMPM*(1.0+17.50517*XMODA*HEC1/(HEC2*SQRTF(TEMPPM)))	
	IF(III)114,114,113	18052115
113	WRITE OUTPUT TAPE 9,1000	18052117
	WRITE OUTPUT TAPE 9,1001,(HOL(I),I#1,12)	18052119
	WRITE OUTPUT TAPE 9,1002	18052121
	WRITE OUTPUT TAPE 9,1008,VOLC,(VOL(I),I#1,M)	18052123

WRITE OUTPUT TAPE 9,1003	18052125
WRITE OUTPUT TAPE 9,1008,(AMASS(I),I#1,M)	18052201
WRITE OUTPUT TAPE 9,1004	18052203
WRITE OUTPUT TAPE 9,1008,((DEN(I,J),I#1,M),J#1,40)	18052205
WRITE OUTPUT TAPE 9,1005	18052207
WRITE OUTPUT TAPE 9,1008,(TSI(I),I#1,M)	18052209
WRITE OUTPUT TAPE 9,1006	18052211
WRITE OUTPUT TAPE 9,1008,(PEI(I),I#1,M)	18052213
WRITE OUTPUT TAPE 9,1007	18052215
WRITE OUTPUT TAPE 9,1008,(SIGA2D(I),I#1,M)	18052217
1000 FORMAT(1H1)	18052301
1001 FORMAT(12A6)	18052303
1002 FORMAT(15HO VOLC - VOL(I))	18052305
1003 FORMAT(6HO A(I))	18052307
1004 FORMAT(8HO N(I,J))	18052309
1005 FORMAT(9HO XSEE(I))	18052311
1006 FORMAT(11HO MUOBAR(I))	18052313
1007 FORMAT(11HO SIGA2D(I))	18052315
1008 FORMAT(1H 1P8E15.6)	18052317
114 RETURN	18052401
END	18052403

Table B-3. List of the P₃ Subroutine

*TYPE(FORTRAN)

SUBROUTINE P3(HOL,M,R,TSI,AMASS,POINTS,	18059903
1SIGAA,SIGSS,PE111,PHIBAR,THERMU)	18059901
DIMENSION R(17),TSI(17),AMASS(17),POINTS(17),	18050107
1SIGAA(17),SIGSS(17),PE111(17),PHIBAR(17),THERMU(17),	18059903
2SIGT(17),QSA(17),RADI(17),PE2(17),A(237,12),	18050111
3D(237),C(237),BOX(4,17),B(24,2),CAP1(17),	18050113
4CAP2(17),VOL(17),SIGA(17),SIGS(17),PE1(17),HOL(12)	18059905
DO 1000 I=1,M	068-0356
L=M+1-I	068-0357
SIGA(L)=SIGAA(I)	18059907
SIGS(L)=SIGSS(I)	18059909
PE1(L)=PE111(I)	18059911
SIGT(L)=SIGA(L)+SIGS(L)	068-0360
RADI(L)=R(I)	068-0361
1005 QSA(L)=TSI(I)*SIGS(L)/SIGA(L)	068-0368
ZA=1./AMASS(I)**2	068-0370
PE2(L)=1.E-3*ZA*(200.+ZA*(28.57+ZA*(9.523+ZA*(4.329+ZA*(2.331+ZA*1068-0371	068-0371
1.399))))	068-0372
1007 IF(I-1)1008,1008,1009	068-0373
1008 VOL(L)=3.14159*R(I)**2	068-0374
GO TO 1000	068-0375
1009 VOL(L)=3.14159*(R(I)**2-R(I-1)**2)	068-0376
1000 CONTINUE	068-0377
MATSIZ=6*M-3	068-0378
I2=7	068-0379
AB=-1	068-0380
J=1	068-0381
IR=1	068-0382
I=1	068-0383
K=2	068-0384
L=3	068-0385
I1=1	068-0386
1 IF(SIGT(I))20,20,2	068-0387

2 BUZZ=SIGS(I)/SIGT(I)	068-0388
AL0=1.-BUZZ	068-0389
AL1=(1.-BUZZ*PE1(I))*AL0	068-0390
AL2=1.-BUZZ*PE2(I)	068-0391
BETA=SQRTF(7.*AL2)	068-0392
BUZZ=35.*AL2+28.*AL0+27.*AL1	068-0393
FUZZ=3780.*AL1*AL2	068-0394
CUZZ=SQRTF(BUZZ*BUZZ-FUZZ)	068-0395
CAP1(I)=SQRTF((BUZZ+CUZZ)/18.)	068-0396
CAP2(I)=SQRTF((BUZZ-CUZZ)/18.)	068-0397
G11=-AL0/CAP1(I)	068-0398
G12=-AL0/CAP2(I)	068-0399
G21=-.5+1.5*AL1/CAP1(I)**2	068-0400
G22=-.5+1.5*AL1/CAP2(I)**2	068-0401
G31=.21428*CAP1(I)-.64285*AL1/CAP1(I)	068-0402
G32=.21428*CAP2(I)-.64285*AL1/CAP2(I)	068-0403
JSW=1	068-0404
3 RADIUS=RADI(IR)	068-0405
4 BUZZ=SIGT(I)*RADIUS	068-0406
ARG1=CAP1(I)*BUZZ	068-0407
ARG2=CAP2(I)*BUZZ	068-0408
ARG3=BETA*BUZZ	068-0409
CALL BESS(ARG1,ARG2,ARG3,JSW,I,M,B)	068-0410
GO TO (6,8),JSW	068-0411
6 BOX(1,I)=RADIUS/CAP1(I)*B(8,JSW)	068-0412
BOX(2,I)=RADIUS/CAP2(I)*B(10,JSW)	068-0413
IF(I-M)7,9,9	068-0414
7 BOX(3,I)=RADIUS/CAP1(I)*B(20,JSW)	068-0415
BOX(4,I)=RADIUS/CAP2(I)*B(22,JSW)	068-0416
JSW=2	068-0417
RADIUS=RADI(IR+1)	068-0418
GO TO 4	068-0419
8 BOX(1,I)=BOX(1,I)-RADIUS/CAP1(I)*B(8,JSW)	068-0420
BOX(2,I)=BOX(2,I)-RADIUS/CAP2(I)*B(10,JSW)	068-0421
BOX(3,I)=BOX(3,I)-RADIUS/CAP1(I)*B(20,JSW)	068-0422
BOX(4,I)=BOX(4,I)-RADIUS/CAP2(I)*B(22,JSW)	068-0423
9 JSW=1	068-0424
15 A(J,I2)=-.5*G31*AB*B(8,JSW)	068-0425
A(J,I2+1)=-.5*AB*G32*B(10,JSW)	068-0426
A(J,I2+2)=-1.66667*AB*AL2/BETA*B(11,JSW)	068-0427
A(K,I2)=AB*G11*B(8,JSW)	068-0428
A(K,I2+1)=AB*G12*B(10,JSW)	068-0429

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A(K,I2+2)=0.0                                068-0430
A(L,I2)=2.5*AB*G31*B(7,JSW)                  068-0431
A(L,I2+1)=2.5*AB*G32*B(9,JSW)                  068-0432
A(L,I2+2)=-5.*AL2*AB*B(12,JSW)/BETA        068-0433
IF(I-M)10,11,11                               068-0434
10 A(J,I2+3)=-5*AB*G31*B(20,JSW)             068-0435
A(J,I2+4)=-5*AB*G32*B(22,JSW)                068-0436
A(J,I2+5)=1.66667*AB*AL2/BETA*B(24,JSW)      068-0437
A(K,I2+3)=-AB*G11*B(20,JSW)                  068-0438
A(K,I2+4)=-AB*G12*B(22,JSW)                  068-0439
A(K,I2+5)=0.0                                  068-0440
A(L,I2+3)=-2.5*AB*G31*B(19,JSW)              068-0441
A(L,I2+4)=-2.5*AB*G32*B(21,JSW)              068-0442
A(L,I2+5)=5.*AB*AL2*B(23,JSW)/BETA          068-0443
IF(IR-1)17,17,11                               068-0444
11 A(I1+6,I2)=AB*B(2,JSW)                    068-0445
A(I1+6,I2+1)=AB*B(4,JSW)                    068-0446
A(I1+6,I2+2)=0.0                            068-0447
A(I1+8,I2)=-5*AB*G21*B(2,JSW)              068-0448
A(I1+8,I2+1)=-5*AB*G22*B(4,JSW)            068-0449
A(I1+8,I2+2)=AB*B(6,JSW)                    068-0450
A(I1+7,I2)=1.5*AB*G21*B(1,JSW)              068-0451
A(I1+7,I2+1)=1.5*AB*G22*B(3,JSW)            068-0452
A(I1+7,I2+2)=AB*B(5,JSW)                    068-0453
IF(I-M)12,18,18                               068-0454
12 A(I1+6,I2+3)=AB*B(14,JSW)                 068-0455
A(I1+6,I2+4)=AB*B(16,JSW)                  068-0456
A(I1+6,I2+5)=0.0                            068-0457
A(I1+8,I2+3)=-5*AB*G21*B(14,JSW)           068-0458
A(I1+8,I2+4)=-5*AB*G22*B(16,JSW)           068-0459
A(I1+8,I2+5)=AB*B(18,JSW)                   068-0460
A(I1+7,I2+3)=1.5*AB*G21*B(13,JSW)           068-0461
A(I1+7,I2+4)=1.5*AB*G22*B(15,JSW)           068-0462
A(I1+7,I2+5)=AB*B(17,JSW)                   068-0463
GO TO (13,16),JSW                           068-0464
13 DO 14 JJ=1,6                                068-0465
JK=I1+JJ+2                                 068-0466
14 D(JK)=0.0                                  068-0467
D(I1+6)=QSA(I)-QSA(I-1)                    068-0468
AB=-AB                                     068-0469
I2=1                                       068-0470
IR=IR+1                                    068-0471

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	JSW=2	068-0472
	I1=I1+6	068-0473
	J=I1+4	068-0474
	K=I1+3	068-0475
	L=I1+5	068-0476
	GO TO 15	068-0477
16	I=I+1	068-0478
	I2=7	068-0479
	AB=-AB	068-0480
	GO TO 1	068-0481
17	D(1)=0.0	068-0482
	D(2)=0.0	068-0483
	D(3)=0.0	068-0484
	I2=1	068-0485
	J=5	068-0486
	K=4	068-0487
	L=6	068-0488
	AB=-AB	068-0489
	IR=IR+1	068-0490
	JSW=2	068-0491
	GO TO 15	068-0492
18	DO 19 JJ=1,6	068-0493
	JK=I1+JJ+2	068-0494
19	D(JK)=0.0	068-0495
	D(I1+6)=QSA(I)-QSA(I-1)	068-0496
	GO TO 26	068-0497
20	RADIUS=RADI(IR)	068-0498
	JSW=1	068-0499
21	DO 22 JJ=1,6	068-0500
	JK=I1+2+JJ	068-0501
	D(JK)=0.0	068-0502
	DO 22 KJ=1,6	068-0503
	LM=I2-1+KJ	068-0504
22	A(JK,LM)=0.0	068-0505
	A(I1+6,I2)=AB	068-0506
	A(I1+6,I2+1)=-2.5*AB*RADIUS*RADIUS	068-0507
	A(I1+7,I2+1)= AB*RADIUS*RADIUS	068-0508
	A(I1+8,I2+1)= .33333*AB*RADIUS*RADIUS	068-0509
	A(I1+8,I2+2)=AB	068-0510
	IF(I-M) 23,2026,2026	068-0511
23	A(I1+3,I2+3)=AB/RADIUS	068-0512
	A(I1+4,I2+4)=AB/RADIUS	068-0513

A(I1+5,I2+3)=2.*AB/RADIUS	068-0514
A(I1+5,I2+4)=-AB/RADIUS	068-0515
A(I1+5,I2+5)= AB/(RADIUS*RADIUS*RADIUS)	068-0516
GO TO (24,25),JSW	068-0517
24 D(I1+6)= -QSA(I-1)	068-0518
I1=I1+6	068-0519
J=I1+4	068-0520
K=I1+3	068-0521
L=I1+5	068-0522
AB=-AB	068-0523
I2=1	068-0524
IR=IR+1	068-0525
RADIUS=RADI(IR)	068-0526
JSW=2	068-0527
GO TO 21	068-0528
25 I=I+1	068-0529
I2=7	068-0530
AB=-AB	068-0531
GO TO 1	068-0532
2026 D(I1+6)= -QSA(I-1)	068-0533
26 KEY=0	068-0534
CALL SOL (KEY,A,D,MATSIZ,C)	068-0535
BOX(3,M)=0.0	068-0536
BOX(4,M)=0.0	068-0537
DENOM=0.0	068-0538
DO 105 I=1,M	068-0539
L=M+1-I	068-0540
IF(SIGT(I))100,100,104	068-0541
100 AL0=RADI(I)**2	068-0542
IF(I-M)101,102,102	068-0543
101 AL1=RADI(I+1)**2	068-0544
GO TO 103	068-0545
102 AL1=0.0	068-0546
103 PHIBAR(L)=C(6*I-5)-1.25*C(6*I-4)*(AL0+AL1)	068-0547
GO TO 105	068-0548
104 PHIBAR(L)=QSA(I)+6.28318/(VOL(I)*SIGT(I))*(C(6*I-5)*BOX(1,I)+C(6*I-4)*BOX(2,I)-C(6*I-2)*BOX(3,I)-C(6*I-1)*BOX(4,I))	068-0549
105 DENOM=DENOM+VOL(I)*SIGA(I)*PHIBAR(L)	068-0550
WRITE OUTPUT TAPE 9,796	18059907
WRITE OUTPUT TAPE 9,797,(HOL(IJJ),IIJJ=1,12)	18059909
796 FORMAT(1H1)	18059911
797 FORMAT(12A6)	18059913

WRITE OUTPUT TAPE 9,904	18059915
904 FORMAT(1HNU P3 OUTPUT/4HUREG5X,6HRADIUS8X,	18059901
112HAVERAGE FLUX4X,13HTHERMAL UTIL.7X,	18059903
27HSIGMA-A10X,7HSIGMA-S7X,	18059905
311HMASS NUMBER7X,11HSOURCE TERM)	18059907
TOTQ=0.0	068-0556
DO 106 I=1,M	068-0557
L=M+1-I	068-0558
TOTQ=TOTQ+QSA(I)*SIGA(I)*VOL(I)	068-0561
THERMU(I)=VOL(L)*SIGA(L)*PHIBAR(I)/DENOM	068-0562
106 WRITE OUTPUT TAPE 9,905,I,R(I),PHIBAR(I),THERMU(I),SIGA(L),SIGS(L)	18059919
1,AMASS(I),QSA(L)	068-0564
905 FORMAT(1H 12,F12.4,F10.4,F16.8,E19.5,E17.5,F15.3,F18.3)	068-0565
WRITE OUTPUT TAPE 9,906,1OTQ,DENOM	18059921
906 FORMAT(1HU15X,24H TOTAL NEUTRON PRODUCTIONF11.4,5A,34H SHOULD EQUAL	068-0567
1TOTAL NEUTRON CAPTUREF11.4)	068-0568
LINL=40-M	068-0569
DO 107 I=1,M	068-0570
L=POINTS(I)	068-0571
IF(L)107,107,108	068-0572
108 IF(LINL-4-L)109,110,110	068-0573
109 WRITE OUTPUT TAPE 9,907	18059923
WRITE OUTPUT TAPE 9,797,(HOL(IJJ),IJJ=1,12)	18059925
907 FORMAT(1H1)	068-0575
LINL=45	068-0576
110 LINL=LINL-4-L	068-0577
WRITE OUTPUT TAPE 9,908,I	18059901
908 FORMAT(24HUEFLUX TRAVERSE IN REGIONI3/1H08X,6HRADIUS14X,	18059909
14HFLUX)	18059911
K=M+1-I	068-0581
IF(I-1) 115,115,116	068-0582
115 DELR=R(1)/POINTS(I)	068-0583
RSTAR=0.0	068-0584
GO TO 117	068-0585
116 DELR=(R(I)-R(I-1))/POINTS(I)	068-0586
RSTAR=R(I-1)	068-0587
117 DO 111 J=1,L	068-0588
DELA1=DELR*SIGHT(K)*CAP1(K)	068-0589
DELA2=DELR*SIGHT(K)*CAP2(K)	068-0590
ARG1=RSTAR*SIGHT(K)*CAP1(K)	068-0591
ARG2=RSTAR*SIGHT(K)*CAP2(K)	068-0592
RSTAR=RSTAR+DELR	068-0593

```

      IF(SIGT(K))112,112,113          068-0594
112 BUZZ=C(6*K-5)-2.25*RSTAR**2*C(6*K-4) 068-0595
      GO TO 111                      068-0596
113 ARG1=ARG1+DELA1                 068-0597
      ARG2=ARG2+DELA2                 068-0598
      BUZZ=QSA(K)+C(6*K-5)*BIO(ARG1)+C(6*K-4)*BIO(ARG2)+C(6*K-2)*BK0(ARG068-0599
      11)+C(6*K-1)*BK0(ARG2)          068-0600
111 WRITE OUTPUT TAPE 9,909,RSTAR,BUZZ    18059905
909 FORMAT(1H F14.4,F18.3)              068-0602
107 CONTINUE                         068-0603
143 RETURN                           068-0604
      END                             068-0605
*
*      TYPE(FORTRAN)                  06
*      SUBROUTINE SOL (KEY,AA,DD,MATSIZ,C) 068-0606
*      DIMENSION AA(237,12),DD(237),C(237) 068-0607
*      IF(KEY)100,100,103                068-0608
100 KEY=6                            068-0609
      J1=1                            068-0610
      K1=7                            068-0611
      DO 101 L=1,2                   068-0612
      J1=J1+1                         068-0613
      KEY=KEY+1                       068-0614
      K1=K1+1                         068-0615
      DO 101 J=J1,3                   068-0616
      AL0=AA(J,KEY)/AA(L,KEY)         068-0617
      DD(J)=DD(J)-AL0*DD(L)          068-0618
      DO 101 K=K1,12                 068-0619
101 AA(J,K)=AA(J,K)-AL0*AA(L,K)       068-0620
      KEY=KEY-1                       068-0621
      K1=8                            068-0622
      J2=0                            068-0623
      DO 102 L=2,3                   068-0624
      KEY=KEY+1                       068-0625
      J2=J2+1                         068-0626
      K1=K1+1                         068-0627
      DO 102 J=1,J2                  068-0628
      AL0=AA(J,KEY)/AA(L,KEY)         068-0629
      DD(J)=DD(J)-AL0*DD(L)          068-0630
      DO 102 K=K1,12                 068-0631
102 AA(J,K)=AA(J,K)-AL0*AA(L,K)       068-0632
      KEY=1                           068-0633
103 L=KEY*6-6                      068-0634

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104 I=6          068-0635
J1=L+4          068-0636
J2=L+9          068-0637
DO 105 II=1,3   068-0638
L=L+1          068-0639
I=I+1          068-0640
DO 105 J=J1,J2  068-0641
AL0=AA(J,I-6)/AA(L,I) 068-0642
DD(J)=DD(J)-AL0*DD(L) 068-0643
DO 105 K=4,6   068-0644
105 AA(J,K)=AA(J,K)-AL0*AA(L,K+6) 068-0645
IF(L+6-MAT>IZ)106,107,107
106 K2=12        068-0646
GO TO 108      068-0647
107 K2=10        068-0648
108 K1=3         068-0649
I=I-6          068-0650
J2=L+6          068-0651
DO 109 II=1,5   068-0652
L=L+1          068-0653
I=I+1          068-0654
J1=L+1          068-0655
K1=I+1          068-0656
DO 109 J=J1,J2  068-0657
AL0=AA(J,I)/AA(L,I) 068-0658
DD(J)=DD(J)-AL0*DD(L) 068-0659
DO 109 K=K1,K2  068-0660
109 AA(J,K)=AA(J,K)-AL0*AA(L,K) 068-0661
L=L-4          068-0662
I=4            068-0663
K1=5            068-0664
J1=L            068-0665
J2=L-1          068-0666
DO 110 II=1,5   068-0667
L=L+1          068-0668
I=I+1          068-0669
K1=K1+1          068-0670
J2=J2+1          068-0671
DO 110 J=J1,J2  068-0672
AL0=AA(J,I)/AA(L,I) 068-0673
DD(J)=DD(J)-AL0*DD(L) 068-0674
DO 110 K=K1,K2  068-0675
                                         068-0676

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110 AA(J,K)=AA(J,K)-AL0*AA(L,K) 068-0677
    IF(L-MATSI<111,112,112 068-0678
111 KEY=KEY+1 068-0679
    GO TO 103 068-0680
112 DO 113 I=1,6 068-0681
    J=MATSI<+1-I 068-0682
    K=10-I 068-0683
113 C(J)=DD(J)/AA(J,K) 068-0684
    L=MATSI<+3 068-0685
    MNO=MATSI<-8 068-0686
    DO 114 II=7,MNO,6 068-0687
    L=L-6 068-0688
    K=10 068-0689
    DO 114 JJ=1,6 068-0690
    K=K-1 068-0691
    J=L-JJ-2 068-0692
114 C(J)=(DD(J)-C(L)*AA(J,12)-C(L-1)*AA(J,11)-C(L-2)*AA(J,10))/AA(J,K) 068-0693
    DO 115 I=1,3 068-0694
115 C(I)=(DD(I)-C(4)*AA(I,10)-C(5)*AA(I,11)-C(6)*AA(I,12))/AA(I,I+6) 068-0695
    RETURN 068-0696
    END 068-0697
*
* TYPE(FORTRAN) 05
SUBROUTINE BESS (ARG1,ARG2,ARG3,JSW,I,M,B) 068+0285
DIMENSION B(24,2) 068+0286
B(2,JSW)=BI0(ARG1) 068+0287
B(8,JSW)=BI1(ARG1) 068+0288
B(1,JSW)=B(2,JSW)-2./ARG1*B(8,JSW) 068+0289
B(7,JSW)=B(8,JSW)-4./ARG1*B(1,JSW) 068+0290
B(4,JSW)=BI0(ARG2) 068+0291
B(10,JSW)=BI1(ARG2) 068+0292
B(3,JSW)=B(4,JSW)-2./ARG2*B(10,JSW) 068+0293
B(9,JSW)=B(10,JSW)-4./ARG2*B(3,JSW) 068+0294
B(6,JSW)=BI0(ARG3) 068+0295
B(11,JSW)=BI1(ARG3) 068+0296
B(5,JSW)=B(6,JSW)-2./ARG3*B(11,JSW) 068+0297
B(12,JSW)=B(11,JSW)-4./ARG3*B(5,JSW) 068+0298
IF(I-M)5,6,6 068+0299
5 B(14,JSW)=BK0(ARG1) 068+0300
B(20,JSW)=BK1(ARG1) 068+0301
B(13,JSW)=2./ARG1*B(20,JSW)+B(14,JSW) 068+0302
B(19,JSW)=4./ARG1*B(13,JSW)+B(20,JSW) 068+0303
B(16,JSW)=BK0(ARG2) 068+0304

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B(22,JSW)=BK1(ARG2)          068+0305
B(15,JSW)=2./ARG2*B(22,JSW)+B(16,JSW) 068+0306
B(21,JSW)=4./ARG2*B(15,JSW)+B(22,JSW) 068+0307
B(18,JSW)=BK0(ARG3)          068+0308
B(24,JSW)=BK1(ARG3)          068+0309
B(17,JSW)=2./ARG3*B(24,JSW)+B(18,JSW) 068+0310
B(23,JSW)=4./ARG3*B(17,JSW)+B(24,JSW) 068+0311
6 RETURN                      068+0312
END                          068+0313
*
TYPE(FORTRAN)
FUNCTION B10 (X)              04
IF (X-3.75)2,2,3
2 Z=(X/3.75)**2
B10=1.0+Z*(3.5156229+Z*(3.0899424+Z*(1.2067492+
1Z*(.2659732+Z*(.0360768+Z*.0045813)))) )
GO TO 4
3 Z=3.75/X
B10=(EXP(X)/SQRTF(X))*(.39894228+Z*(.013285917+
1Z*(.002253187+Z*(-.001575649+Z*(.009162808+Z*
2(-.020577063+Z*(.026355372+Z*(-.016476329+Z*
3.003923767)))))))
4 RETURN                      068+0314
END                          068+0315
*
TYPE(FORTRAN)
FUNCTION B11 (X)              068+0316
IF (X-3.75)2,2,3
2 Z=(X/3.75)**2
B11=(.5+Z*1.87890594+Z*(.51498869+Z*(.15084934+
1Z*(.02658733+Z*(.00301532+Z*.00032411)))))*X
GO TO 4
3 Z=3.75/X
B11=(EXP(X)/SQRTF(X))*(.39894228+Z*(-.039880242+Z*(-.003620183+
1Z*(.00163014+Z*(-.01031555+Z*(.022829673+Z*(-.028953121+
2Z*(.017676235-Z*.004200587)))))))
4 RETURN                      068+0317
END                          068+0318
*
TYPE(FORTRAN)
FUNCTION BK0 (X)              068+0319
IF (X-2.0)2,2,3
2 Z=(X/2.0)**2
SERIES=-.57721566+Z*(.4227842+Z*(.23069756+
1Z*(.0348859+Z*(.00262698+Z*(.0001075+Z* 068+0320
068+0321
068+0322
068+0323
068+0324
068+0325
068+0326
068+0327
068+0328
068+0329
068+0330
068+0331
068+0332
068+0333
068+0334
068+0335
068+0336
068+0337
068+0338
068+0339
068+0340
068+0341
068+0342
068+0343

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2.0000074)))))) 068+0344
BK0=SERIES-LOGF(X/2.0)*B10(X) 068+0345
GO TO 4 068+0346
3 Z=2.0/X 068+0347
BK0=(1.25331414+Z*(-.07832358+
1Z*(.02189568+Z*(-.01062446+Z*(.00587872+Z*
2(-.0025154+Z*.00053208)))))/(SQRTF(X)*EXP(X)) 068+0348
068+0349
068+0350
4 RETURN 068+0351
END 068+0352
* TYPE(FORTRAN) 01
FUNCTION BK1(X) 068+0353
IF(X>2.0)2,2,3 068+0354
2 Z=(X/2.0)**2 068+0355
SERIES=1.0+Z*(.15443144+Z*(-.67278579+Z*(-.18156897
1+Z*(-.01919402+Z*(-.00110404-Z*.00004686)))) 068+0356
BK1=SERIES/X +LOGF(X/2.0)*B11(X) 068+0358
GO TO 4 068+0359
3 Z=2.0/X 068+0360
BK1=(1.25331414+Z*(.23498619+Z*(-.0365562+Z*(
1.01504268+Z*(-.00780353+Z*(.00325614-Z*.00068245)))))/(SQRTF(X)*
2EXP(X)) 068+0361
068+0362
068+0363
4 RETURN 068+0364
END 068+0365

```

APPENDIX C

Sample Problem for CODE P3

650 DATA SHEET

REQUEST

JOB TITLE CODE P-3

—WRITTEN BY—

— DATE

TEST CASE FOR CODE P3

000000

P3 OUTPUT

REG	RADIUS	AVERAGE FLUX	THERMAL UTIL.	SIGMA-A	SIGMA-S	MASS NUMBER	SOURCE TERM
1	4.1280	10.1095	0.96336868	0.40710E-01	0.14400E-00	34.962	0.187
2	5.6000	11.7105	0.00402565	0.17580E-03	0.39800E-00	12.000	357.702
3	7.0000	12.7699	0.00540772	0.17580E-03	0.39800E-00	12.000	357.702
4	8.5000	13.4007	0.00747964	0.17580E-03	0.39800E-00	12.000	357.702
5	10.0000	13.7792	0.00917948	0.17580E-03	0.39800E-00	12.000	357.702
6	11.4645	13.9694	0.01053882	0.17580E-03	0.39800E-00	12.000	357.702

TOTAL NEUTRON PRODUCTION 23.0062

SHOULD EQUAL TOTAL NEUTRON CAPTURE 23.0059

FLUX TRAVERSE IN REGION 1

RADIUS	FLUX
2.0640	9.830
4.1280	10.865

FLUX TRAVERSE IN REGION 2

RADIUS	FLUX
4.8640	11.712
5.6000	12.328

FLUX TRAVERSE IN REGION 3

RADIUS	FLUX
6.3000	12.772
7.0000	13.117

FLUX TRAVERSE IN REGION 4

RADIUS	FLUX
7.7500	13.404
8.5000	13.622

FLUX TRAVERSE IN REGION 5

RADIUS	FLUX
9.2500	13.783
10.0000	13.897

FLUX TRAVERSE IN REGION 6

RADIUS	FLUX
10.7322	13.969
11.4645	14.011

- 41 -

APPENDIX D

Sample Problem for CODE NTF3

650 DATA SHEET

REQUEST	JOB TITLE	CODE NTP 3	WRITTEN BY	DATE			
1 - 10	11 - 20	21 - 30	31 - 40	41 - 50	51 - 60	61 - 70	71 - 80
TEST CASE	FOR CODE NTP3 -- GAS COOLED GRAPHITE REACTOR						
660.0	12.0	6.2					
4.128	5.60	7.00	8.50	10.0	11.4645		
111.3624							
4134.877							
2118.322							
2817.2244							
22.05017							
00							
2574.2277							
00							
2591.4394							
00							
25120.5196							
00							
25143.846							
00							
25162.9464							
00							
00							

CITI

TEST CASE FOR CODE NTP3---GAS COOLED GRAPHITE REACTOR

P3 OUTPUT

REG	RADIUS	AVERAGE FLUX	THERMAL UTIL.	SIGMA-A	SIGMA-S	MASS NUMBER	SOURCE TERM
1	4.1280	10.0930	0.96227772	0.40925E-01	0.14400E-00	34.962	0.186
2	5.6000	11.6252	0.00414421	0.18209E-03	0.39752E-00	11.990	344.923
3	7.0000	12.6793	0.00556806	0.18209E-03	0.39752E-00	11.990	344.923
4	8.5000	13.3076	0.00770248	0.18209E-03	0.39752E-00	11.990	344.923
5	10.0000	13.6645	0.00945365	0.18209E-03	0.39752E-00	11.990	344.923
6	11.4645	13.8696	0.01085386	0.18209E-03	0.39752E-00	11.990	344.923

TOTAL NEUTRON PRODUCTION 22.9789 SHOULD EQUAL TOTAL NEUTRON CAPTURE 22.9791

FLUX TRAVERSE IN REGION 1

RADIUS	FLUX
2.0640	9.755
4.1280	10.785

FLUX TRAVERSE IN REGION 2

RADIUS	FLUX
4.8640	11.627
5.6000	12.239

FLUX TRAVERSE IN REGION 3

RADIUS	FLUX
6.3000	12.681
7.0000	13.025

FLUX TRAVERSE IN REGION 4

RADIUS	FLUX
7.7500	13.311
8.5000	13.528

FLUX TRAVERSE IN REGION 5

RADIUS	FLUX
9.2500	13.689
10.0000	13.802

FLUX TRAVERSE IN REGION 6

RADIUS	FLUX
10.7322	13.873
11.4645	13.915

TEST CASE FOR CODE NTP3---GAS COOLED GRAPHITE REACTOR

MOD TEMP 6.600000E 02 NEUT TEMP 7.566326E 02

FLUX DISADVANTAGE FACTORS(I)

1.000000E 00 1.151808E 00 1.256247E 00 1.318492E 00 1.355833E 00 1.374180E 00

-45-

Distribution

1. DTIE, AEC
2. M. J. Skinner
- 3-23. L. L. Bennett

